

Teston Road Area Transportation Improvements Individual Environmental Assessment

Transportation System Technical Report # 1

Presented to:

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1. INTRODUCTION

1.1 Study Overview

In 2020 the Regional Municipality of York (York Region) retained Morrison Hershfield (MH) to conduct an Individual Environmental Assessment (IEA) Study for transportation improvements in the Teston Road area. MH will examine alternative solutions that will improve transportation throughout the study area through a comprehensive IEA process.

The road network in northern Vaughan has a number of 'missing links'. The most notable of these is Teston Road between Keele Street and Dufferin Street. York Region has previously tried to secure approval to construct this link. Though York Region presented strong transportation arguments for this link in the previous (2003) Municipal Class Environmental Assessment (EA), and the current and updated Transportation Master Plan (2009 and 2016), given the sensitive land uses in the area, obtaining project approval has been extremely challenging. Consequently, the Ministry of the Environment, Conservation and Parks (MECP) required that the transportation problems and opportunities in the area be examined through an IEA Study to determine the most appropriate solution to address future transportation requirements in the area.

In 2016 York Region initiated the IEA process and completed the Teston Road Area Transportation IEA Terms of Reference (ToR) in 2018. Consultation with interested and/or affected parties is an essential part of this planning process and provides a mechanism for the proponent (York Region) to identify and respond to issues before decisions are made and documentation is filed with the MECP.

1.2 Study Area

The study area for this project was determined during the ToR stage completed in 2018. The study area is bounded by Kirby Road to the north, Bathurst Street to the east, Major Mackenzie Drive West to the south, and Highway 400 to the west.

The IEA study area is situated within the City of Vaughan. The City of Vaughan is one of nine local municipalities within York Region, with local government organized in a two-tier structure.

For the purposes of the traffic analysis, the study area is extended to include Yonge Street, Pine Valley Drive, King Vaughan Road and Rutherford Road. The IEA and Traffic Analysis study areas are outlined in **Figure 1**.



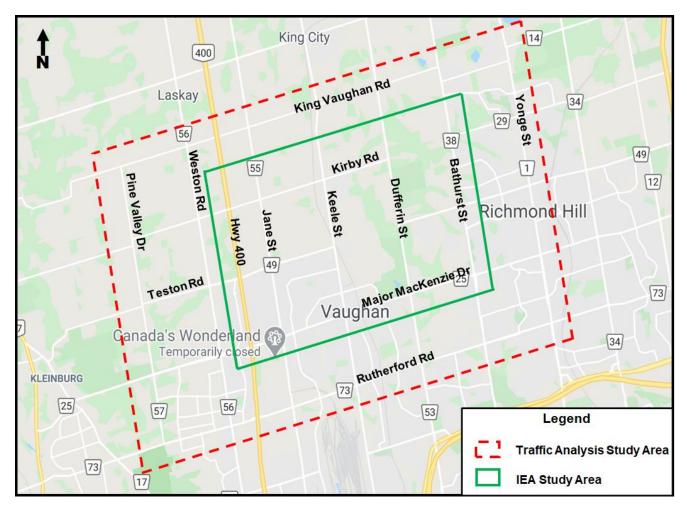


Figure 1: Study Area

1.3 Background

According to the Statistic Canada's population census from 2016, York Region has a population of 1.14 million residents and is anticipated to grow to 1.5 million residents by 2031 (the time or planning horizon for the Official Plan). York Region is currently undertaking the Municipal Comprehensive Review process to review the Region's population and employment forecasts, land budget and Regional Official Plan policies. Through this review process York Region is forecast to reach 2.02 million residents and 990 thousand jobs by 2051. Along with this growth comes the need for additional infrastructure to meet the demands of the growing communities, including the City of Vaughan.

The City of Vaughan is forecast to experience significant population and employment growth by 2031. With a population of more than 330,000 residents, Provincial and Regional forecasts predict Vaughan will reach a population of 416,600 people and 266,100 jobs by 2031. As such, Vaughan will require a significant investment in infrastructure to support this growth.



Although improvements to Teston Road have been identified in the Region's TMP (2016) and various other studies, the IEA is not starting off with a 'predetermined outcome'. The problem and opportunity components of this task will be based on the Transportation Analysis outlined in this report.

1.4 Purpose of Transportation System Technical Report #1

This Report documents regional and municipal planning context, existing transportation facilities and their conditions, existing and future operational performance analysis, a 5-year collision history review and any existing road deficiencies which could affect and have an influence on this study.

The information presented within this Transportation System Technical Report will be used during subsequent stages of this study to support the generation and evaluation of the appropriate alternative solutions as well as the evaluation of those alternatives.



2. REGIONAL AND MUNICIPAL PLANNING CONTEXT

In addition to provincial policies, various municipal policy documents exist and will be taken into consideration in relation to this Project. At the municipal level, Official Plans provide the context and boundaries within which a municipality operates with regards to land use, development and growth. The *Planning Act* requires that an Official Plan conforms to, or does not conflict with provincial plans, has regard for matters of provincial interest, and "shall be consistent with" policy statements issued under the Act. Municipalities must incorporate provincial policy initiatives into their Official Plans and other planning policy documents. Relevant municipal planning policies and how they affect land uses within the study area are presented below for York Region and the City of Vaughan.

2.1 York Region Plans/Policies

2.1.1 York Region Official Plan

The Modified 2010 York Region Official Plan – 2019 Office Consolidation (2019) describes how the Region plans to accommodate future growth and development while meeting the needs of existing residents and businesses in the Region. It provides directions and policies that outline how the community is designed, serviced and supported; and, guides economic, environmental and community building decisions to manage growth (York Region Official Plan – 2019 Office Consolidation, 2019).

The Plan includes policies to help co-ordinate and provide the framework for the nine local municipalities within York Region to undertake more detailed planning. The Region is responsible for regulating land use and establishing policies for physical, economic and social development within its jurisdiction. However, this responsibility is conducted within a provincial framework. Accordingly, during the planning horizon of its Plan, the Province and the Region will work together to ensure successful implementation of the governing Provincial Plans and legislation. Thus, all planning decisions under the York Region Official Plan shall conform with provincial plans such as the Oak Ridges Moraine Conservation Plan (ORMCP), Growth Plan (A Place to Grow, 2020), and Greenbelt Plan and be consistent with the Provincial Policy Statement (PPS).

According to the Statistic Canada's population census from 2016, York Region has a population of 1.14 million residents and is anticipated to grow to 1.5 million residents by 2031 (the time or planning horizon for the Official Plan). Along with this growth comes the need to add infrastructure to meet the demands of the growing communities, including the City of Vaughan.

York Region is currently undertaking the Municipal Comprehensive Review process to review the Region's population and employment forecasts, land budget and Regional Official Plan policies. Through this Review process York Region is forecast to reach 2.02 million residents and 990 thousand jobs by 2051.



The decisions documented within the Official Plan will act as a base scenario for the IEA study and it is assumed that all improvements identified within the Official Plan for the study area will be approved and built. The extension of Teston Road between Keele Street and Dufferin Street, while included in the Official Plan, will be considered as just one alternative through the IEA study.

Section 7.2 of the Official Plan documents York Region's policies for the provision of infrastructure and servicing for the movement of people and goods through transit, active transportation and streets. The objectives that dictate the policies as well as the most relevant policies for this study are included in **Table 1.**

Table 1: Official Plan Objectives for the Movement of People and Goods

| OBJECTIVE FOR EACH TRANSPORTATION MODE | RELEVANT POLICIES |
|--|---|
| Active Transportation Objective: To create an active transportation system and programs that encourage walking, cycling and the use of public transit. | Implement the cycling network. Apply the planning and design guidelines for these facilities in the implementation of the network. To develop an integrated Regional cycling network connecting people to places of recreation, services and employment and transit. |
| Transit Objective: To provide transit service that is convenient and accessible to all residents and workers of York Region. | To develop transit corridors and related infrastructure necessary to establish the York Region Transit and Viva network. To provide preferential treatment for transit vehicles on designated Regional streets, including the construction of high-occupancy vehicle lanes, dedicated transit lanes, transit signal priority and other transit priority measures within the right-of-way. To achieve higher transit usage by supporting improvements in service, convenient access and good urban design To manage the movement of traffic in the Regional Rapid Transit Corridors to improve the safety and efficiency of all movements including that of pedestrians, cyclists and transit vehicles |
| Streets Objectives: To ensure streets support all modes of transportation including walking, cycling, transit, automobile use, and the efficient movement of goods. To plan and protect future urban and rural streets to accommodate transportation demands | That an Individual Environmental Assessment will be undertaken for the unopened road allowance of Teston Road between Dufferin Street and Keele Street which will include a comprehensive network analysis and environmental impact assessment to determine a preferred transportation strategy in the corridor. To improve the street network as identified in the Official Plan, including the completion of the necessary Environmental Assessments. Corridors are to accommodate all modes of transportation including walking, cycling, transit, automobile use and the movement of goods, as well as public and private utilities. To investigate establishing a continuous alternative east-west corridor(s) in the central part of the Region. |



| OBJECTIVE FOR EACH TRANSPORTATION MODE | RELEVANT POLICIES | |
|---|--|--|
| | That within the Oak Ridges Moraine, all improvements to the Regional Transit and Street Networks shall conform with the policies of the Oak Ridges Moraine Conservation Plan | |
| Goods Movement Objective: To promote a linked and efficient network for goods movement | To promote an interconnected goods movement network that links local municipalities and surrounding areas, utilizing Provincial highways, Regional streets and rail corridors. | |
| that supports economic vitality and minimizes conflicts with sensitive land uses. | To support the optimization of the existing transportation network for goods movement, through methods such as access management and intelligent transportation systems. | |

2.1.2 York Region Transportation Master Plan

The York Region Transportation Master Plan (TMP 2016) builds upon the direction given in the Official Plan but focusses on the transportation network and the various modes of transportation provided or planned throughout York Region. The TMP sets five objectives for planning and implementing the transportation network. The objectives focus on transit, active transportation, the road network, and employment areas. **Table 2** identifies the various objectives and the initiatives within those objectives that apply to the Teston Road Area Transportation Improvements Project.

Table 2: TMP Objectives and Applicable Major Initiatives

| OBJECTIVE | MAJOR INITIATIVES | |
|--|--|--|
| Objective 1: Create a world class transit system | Improve transit frequency and coverage. | |
| Objective 2: Develop a road network fit for the future | Build missing links and new roads Utilize technology to improve efficiency of the road network Expand high occupancy vehicle/transit network Develop the finer grid road network Build context sensitive multi-modal corridors Incorporate flexibility in corridors Maximize the person carrying capacity through corridor evolution | |
| Objective 3: Integrate active transportation in urban areas | Accelerate active transportation infrastructure that connects communities to transit spines, major destinations and Regional Centres Support the last mile Complete gaps in sidewalks | |
| Objective 4: Maximize the potential of employment areas | Improve connectivity to 400-series highways | |
| Objective 5: Make the last mile work | Provide safe and convenient walking/cycling opportunities to mobility hubs | |



Section 9.3.5 of the TMP addresses the need to complete several missing links within the Regional road network, including Teston Road between Keele Street and Dufferin Street. The TMP ensures that any future crossing of natural heritage systems in the Teston Road area, would be subject to an environmental assessment that demonstrates the need and justification for the project through an analysis of alternative solutions and consideration of potential environmental effects. The completion of missing links is also supported by active transportation policies throughout the TMP as these would provide additional connections for active transportation users.

The TMP also identifies existing and future road network conditions, transit network and pedestrian and cyclist facilities. These conditions will play a crucial role in identifying the problems and opportunities, generating reasonable alternatives, and comparatively evaluating those alternatives during the IEA study.

2.1.3 York Region Pedestrian and Cycling Planning & Design Guidelines

Building upon York Region's original Pedestrian & Cycling Master Plan, the latest Pedestrian and Cycling Planning & Design Guidelines (PCPDG, 2018) provide designers with a design reference to support the development of active transportation facilities from the Region's perspective. The guideline, in addition to the Region's Designing Great Streets, reflects the Region's vision to develop high quality active transportation facilities to balance the needs of all road users (comfort, safety and efficiency). The guideline highlights the importance of implementing consistent facility types and design treatments which are in accordance with the Region's planning and design initiatives to further increase active mode shares. The PCPDG expands on the objectives of the TMP that pertain to pedestrians and cyclists, such as Objective 3 as shown in **Table 2**.

The PCPDG will be examined for opportunities to provide active transportation facilities within the study area.

2.1.4 York Region Designing Great Streets: Building Roads that Build Community - Design Guideline

The Designing Great Streets (DGS, 2019) design guideline is an update to York Region's roadway design process using a context sensitive approach, which emphasizes greater mobility for all road users while supporting the development of adjacent land uses. The latest guideline contains six roadway typologies (City Centre Street, Avenue, Main Street, Connector, Rural Road and Rural Hamlet Road) that the Region has developed to reflect their road network aspirations. Additionally, the guideline includes design best practices for cross sectional elements and intersection design, with a nine-step decision-making process to guide the development of roadway corridors (retrofit, reconstruction or new construction). The concerted effort between the various features of the latest design guideline support the Region's vision of "creat[ing] vibrant streets for York Region that provide a range of safe and reliable transportation options, while being sensitive to adjacent land uses and needs of the community."



The DGS will be reviewed for opportunities to incorporate the Region's recommended road typologies and design best practices.

2.1.5 Other Pertinent Regional Policies

There are a number of important Regional policies that will play a role in the evaluation of alternatives and/or the development of the Preliminary Design. These policies include, but are not limited to:

- Vision 2051 (n.d.): Vision 2051 is a policy document providing long term strategies for York Region. Vision 2051 includes eight goal areas ranging from being a place people can thrive to creating a resilient natural environment and agricultural system. There are several goals within Vision 2051 that support the creation of new infrastructure to support growing communities and increasing connectivity, which is the aim of the IEA study.
- Sustainability Strategy (2007): The strategy is a framework for growth
 management decision making that integrates the economy, environment,
 and community. The strategy is intended to ensure that each decision made
 by York Region produces value and a net gain within the economy,
 environment, and the community.
- Regional Streetscape Policy (n.d): The streetscape policy provides an
 approach to ensure a unified vision for the design of regional streets and the
 policy will be used during the generation of alternatives to determine
 appropriate roadway corridor widths. Moreover, the specific roadway design
 details will be addressed during the Preliminary Design stage of the IEA
 process.
- Standard Operating Procedures for Traffic Noise Mitigation (2010): A noise assessment will be completed to assist in the evaluation of the alternative methods. The guidelines in this standard operating procedure will be followed and provide the framework to complete the noise assessment.

2.2 City of Vaughan Plans/Policies

2.2.1 City of Vaughan Official Plan

The study area lies within the City of Vaughan, which is a municipality in York Region. Centrally located within the Greater Golden Horseshoe (GGH) area, the City enjoys strong rail and road transportation links to its neighbouring municipalities and others across the GGH and beyond. The City is also home to the headwaters of both the Humber and Don Rivers, with their significant valley systems being a prominent feature on the landscape.

Similar to York Region, Vaughan is forecast to experience significant population and employment growth by 2031. With a population of more than 330,000 residents, Provincial and Regional forecasts predict Vaughan will reach a population of 416,600 people and 266,100 jobs by 2031. As such, Vaughan will require significant investment in the infrastructure necessary to support this growth.



The City of Vaughan Official Plan 2010 (June 2019 Office Consolidation) is part of an overall Growth Management Strategy, initiated by City Council that is intended to shape the future of the City and guide its continued transformation into a vibrant, beautiful and sustainable City. The Official Plan – A Plan for Transformation, was prepared as part of a comprehensive three-year exercise, involving a number of concurrent studies and Master Plans to address the City's long-term planning requirements to the year 2031. The June 2019 Office Consolidation of the Vaughan Official Plan 2010 was updated to include Local Planning Appeal Tribunal (LPAT) decisions and City Council approved Official Plan Amendments as of May 29, 2019. In addition to consolidating all former land use policy into one document, the June 2019 Office Consolidation brings the City into conformity with recent Provincial and Regional land use policy direction.

Where the York Region Official Plan sets priorities at the regional level, the City of Vaughan's Official Plan provides the structure for planning decisions made within the City and at the local level. This includes land use planning and the local road network. The study area features a number of different land uses which are described in **Table 3**.

The City's Official Plan also discusses the importance of a safe and efficient street network that accommodates transit, active transportation and other vehicles. The City's local network is dependent on the planning and implementation of the provincial and regional road networks.

During the IEA study, potential impacts to mapped land uses will be examined during the evaluation of alternatives. Where applicable, sensitive land uses will be avoided, and pertinent mitigation measures explored and prescribed during the Preliminary Design phase, to minimize potential impacts to land uses and features that cannot be avoided.

Table 3: City of Vaughan Land Use Descriptions and Areas

| LAND USE | DESCRIPTION FROM THE OFFICIAL PLAN | LOCATIONS WITHIN THE STUDY AREA |
|-------------------------------------|--|--|
| Natural Areas and Countryside | Natural Areas and Countryside generally follow the valleys of the Humber and Don River systems and their associated tablelands but also feature areas of agricultural lands in the north parts of Vaughan. | Similar to areas identified as Natural Core or Countryside Areas in the ORMCP. The areas east of Dufferin Street and North of Teston Road. Throughout the study area generally following watercourses such as the east and west branches of the Don River. |
| Employment Area | Employment Areas are intended for the use of economic activities that require separation from other uses in order to achieve their maximum potential. Employment areas offer areas for economic activity related to | On the east side of the GO Barrie Line, north and south of Teston Road abutting the former landfills. Between Jane Street and Highway 400, north of Teston Road. |



| LAND USE | DESCRIPTION FROM THE OFFICIAL PLAN | LOCATIONS WITHIN THE STUDY AREA |
|--|--|---|
| | industrial, manufacturing, warehousing and some offices. | |
| Primary Intensification Corridor | Intensification corridors link various centres and are linear places of activity in their own right. They may accommodate mixed-use intensification or employment intensification. | Along Major Mackenzie Drive West. |
| Local Centres | Local centres act as the focus for communities, are lower in scale and offer a more limited range of uses. | Surrounding the intersection of Major Mackenzie Drive West and Keele Street and encompasses much of Historic Maple Village. |
| Primary Centres | Primary Centres accommodate a wide range of uses and will have tall buildings, as well as lower ones, to facilitate an appropriate transition to neighbouring areas. | North of Major Mackenzie Drive West, west of Jane Street and east of Highway 400, includes the Mackenzie Vaughan Hospital (currently under construction). |
| Community Areas | Characterized by predominately Low-Rise Residential housing stock, with local amenities including local retail, community facilities, schools and parks, and they provide access to the City's natural heritage and open spaces. | The remainder of the study area not identified above. A new community area is planned for the block bound by Kirby Road, Keele Street, Teston Road, and Jane Street. |

2.2.2 City of Vaughan Transportation Master Plan

Similar to York Region's TMP, the City's TMP (2012) builds upon the direction given in the Official Plan but focusses on the transportation network and the various modes of transportation provided or planned throughout the City of Vaughan. The City's TMP focusses on solutions to several transportation issues including: affordability of supplying sufficient capacity for rapid growth; the dependency on the automobile; heavy orientation for travel to the City of Toronto; providing more efficient movement of goods; the threat of air quality posed by the rise in auto and truck travel; and if development density is high enough to support efficient public transit. The TMP attempts to address these issues through the planning of the City's road network, active transportation and transit initiatives.

The future conditions provided within the TMP will be incorporated into the IEA study as part of the generation and evaluation of alternatives. In this regard, every effort will be made to conform to the City's TMP during the IEA study.

2.2.3 City of Vaughan Pedestrian and Bicycle Master Plan (2019 Update)

The City of Vaughan Pedestrian and Bicycle Master Plan (PBMP) reflects the direction from the City's Official Plan and Transportation Master Plan with a dedicated focus towards pedestrian and cycling infrastructure. Originally completed



in 2012, the City of Vaughan commenced an update to the Pedestrian and Bicycle Master Plan in 2017 to guide the planning, design, construction, and maintenance of pedestrian and cycling infrastructure. The key areas of opportunity identified in the update include safety for all ages and abilities, supporting pedestrian and cycling infrastructure, addressing gaps and connectivity, and creating awareness and culture. The process of the following IEA study shall address and support the key opportunity areas identified within the PBMP update.

2.2.4 North Vaughan and New Communities Transportation Master Plan

The North Vaughan and New Communities Transportation Master Plan (NVNCTMP) is a long-range plan that recommends policies, programs and the infrastructure required to meeting the existing and future mobility needs for the North Vaughan area (City of Vaughan, 2019a). The area covered by the NVNCTMP is shown in **Figure 2**. The Teston Road IEA study area has been added to the map.

The TMP recommended both the Transportation network layout and Active Transportation networks for the area.

The study was conducted in parallel with Secondary Plan studies for both Block 27 and Block 41 (see **Figure 2**) that are reviewing the transportation network and land uses within each block.

A portion of the NVNCTMP study area and all of Block 27 falls within the Teston Road Area Improvements study area. The decisions made within these studies will be further examined and integrated into the Teston Road Area study as required.

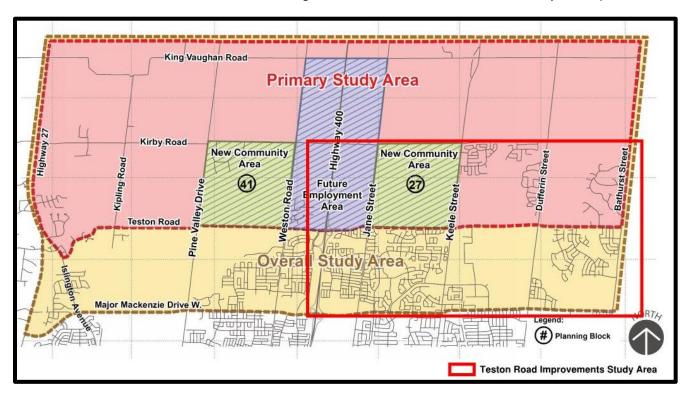


Figure 2: North Vaughan and New Communities TMP Study Area (City of Vaughan, 2019)



2.3 Other Relevant Plans/Policies

2.3.1 Metrolinx 2041 Regional Transportation Plan (2018)

The 2041 Regional Transportation Plan (RTP) represents Metrolinx's dedication to developing a complete multi-modal transportation system that connects the greater Toronto and Hamilton area. The groundwork of the RTP plan is in support of the planning policies of the Growth Plan for the Greater Golden Horseshoe to provide safe, convenient and reliable connections. The goals of the RTP are to provide strong multi-modal connections to transit, address a complete trip and to support the development of sustainable and healthy communities. To achieve the vision and goals of the RTP, Metrolinx's primary strategies include expanding the transit network to serve a greater proportion of the region, optimizing the transportation system to support transit use and integrating transit in the planning of transportation systems and land use.

2.3.2 Provincial Policy Statement (2020)

The PPS is a policy planning document prepared in accordance with the Planning Act, providing underlying direction for land use planning and developments within Ontario. The policies of the PPS are aimed at protecting provincial interests to ensure efficient land use planning and enhancing the quality of life for Ontarians addressing a breadth of matters related to community development, resource management, and public health and safety. The PPS supports the development of a reliable, cost effective multi-modal transportation systems that promotes the use of a mix of active transportation modes and transit to facilitate the safe movement of people. In addition, the policies are in support of improving connections between various transportation modes and expanding the greater transportation network beyond regional boundaries. Teston Road is a key east-west corridor through the City of Vaughan that has the potential to serve as an important multi-modal transportation corridor to support the City's future growth and development outlook.

2.3.3 A Place to Grow (2020)

Building upon the PPS, the Growth Plan for the Greater Golden Horseshoe (GPGGH) is a regional specific land use planning policy for the Greater Golden Horseshoe in conjunction with other plans, such as the Oak Ridges Moraine Conservation Plan and Niagara Escarpment Plan, which focus on establishing a framework for developing a thriving economy, clean and healthy environment, and social equity. The vision of the GPGGH is to support the development of complete communities which include access to affordable transit and active transportation facilities, employment zones, and a range of housing options. These policies support the development of active transportation and transit supportive networks to offer residents with a balance of transportation choices by providing continuous links and multi-modal connections which align with the York Region's proposed plans for Teston Road.



2.3.4 Nearby Ongoing/Approved EAs

There are several ongoing EAs within and in proximity to the study area. Though these EAs involve assessments of planned improvements identified within the Official Plans of either York Region or the City of Vaughan for the most part, it is recognized that they may affect the future conditions within the study area.

The IEA study will ensure the recommendations for these EAs are incorporated should they be available. Otherwise reasonable assumptions will be made based on available information. A preliminary list of other EAs within and in proximity to the study area includes:

- York Region's EA for Teston Road Pine Valley Drive to Weston Road (approved November 2016 – construction anticipated in 2021).
- York Region's EA for Major Mackenzie Drive McNaughton Road/Avro Road to Keele Street (approved December 2018 – construction anticipated in 2024).
- City of Vaughan's EA for the Kirby Road Widening between Jane Street and Dufferin Street and the Grade Separation of the Barrie GO Line at Kirby Road (ongoing).
- City of Vaughan's EA for Kirby Road Extension between Bathurst Street and Dufferin Street (approved October 2019 – construction anticipated in 2022).
- City of Vaughan's EA for North Maple Community Bridge (approved December 2013).
- Ministry of Transportation's (MTO) EA for the GTA West Corridor (expected to be complete by the end of 2022).
- Metrolinx Barrie Rail Corridor Expansion Project, Transit Project Assessment Process, Environmental Project Report (approved August 2017).
- Metrolinx Transportation and Traffic Impact Analysis for Kirby GO Station (approved August 2018).

Additional information on any anticipated EAs within the study area will be requested from York Region and the City of Vaughan, and the list updated as the IEA study progresses.



3. EXISTING CONDITIONS

3.1 Road Network

As mentioned in **Section 1.2**, the IEA study area is bounded by Kirby Road to the north, Bathurst Street to the east, Major Mackenzie Drive West to the south, and Highway 400 to the west. This section provides a glimpse of traffic characteristics at each of the north/south and east/west arterial roads within the study area.

3.1.1 Teston Road (York Region Road 49)

Teston Road (York Region Road 49) is an east-west arterial road with a 4-lane cross section (between Highway 400 and Keele Street) and 2-lanes (from Keele Street to Rodinea Road and from Dufferin Street to Bathurst Street) and a posted speed limit of 60 km/h. The posted speed limit is reduced to 50 km/h, east of Bathurst Street. There is a discontinuity along Teston Road between Keele Street and Dufferin Street.

The land uses abutting the Teston Road corridor between Highway 400 and the eastern boundary for the City of Vaughan (Bathurst Street) includes a mix of open space, agricultural, residential, and commercial / industrial. Portions of the open space and agricultural land near Teston Road are part of the Oak Ridges Moraine and Greenbelt natural heritages systems. The land east of Keele Street adjacent to Teston Road includes environmentally significant areas and areas of natural and scientific interest subject to the policies of the Oak Ridges Moraine Conservation Plan. Other Greenbelt areas would be subject to the policies of the Greenbelt Plan. The majority of the residential land use abutting Teston Road is comprised of lowrise residential and mixed-use properties with new community areas planned for the land on the north side of Teston Road bounded by Jane Street and Keele Street subject to the New Communities Secondary Plan. The commercial and industrial lands along Teston Road are concentrated on the east of Keele Street, adjacent to the existing Go Transit rail line, comprised of general and prestige employment areas. The missing segment of Teston Road between Keele Street and Dufferin Street currently provide access to landfill sites formerly used by the City of Toronto and regional municipalities of York and Durham.

With regards to the existing road geometrics, the existing Teston Road horizontal alignment from west to east begins with a reverse curve with approximate radii of 350m to 475m between Highway 400 and Jane Street. It is then on a tangent between Jane Street and Keele Street. East of Keele Street, the alignment crosses the Barrie GO Line rail at-grade with an approximate 375m radius reverse curve which terminates as a tangent at Rodinea Road. Between Dufferin Street and Bathurst Street, a 400m reverse curve is present at the Dufferin Street intersection with the remaining segment being on a tangent until Bathurst Street. The existing profile follows a rolling topography with approximate grades ranging from 0.30% and 12.50% (which exceeds the Region's maximum desirable vertical grade of 8%) with crest curve K values ranging from 1 to 21 (which certain areas do not meet the minimum 17 K_{crest} value for a 70 km/h Design Speed) and sag curve K values



ranging from 1 to 7 which do not meet the minimum 10 K_{sag} value for a 70 km/h Design Speed).

As shown in **Table 4**, the Annual Average Daily Traffic (AADT) volume in this section of Teston Road (between Highway 400 and Bathurst Street) was in the range of 2,222 to 16,285 veh/day. The field measured 85th percentile speed was in the order of 72-83 km/h. The typical vehicle carrying capacity of a single arterial traffic lane on Teston Road is in the order of 800 to 900 veh/h.

Table 4: Traffic Characteristics along Teston Road

| Location Description | AADT (vpd) | 85 th Percentile Speed (kph) |
|----------------------------|---------------|---|
| Hwy 400 to Jane St | 5,309 (2019) | 83 |
| Jane St to Keele St | 6,476 (2018) | 75 |
| Keele St to Rodinea Rd | 2,222 (2019) | 72 |
| Dufferin St to Bathurst St | 16,285 (2018) | 74 |

3.1.2 Kirby Road (City of Vaughan)

Kirby Road (from Highway 400 to Dufferin Street) is an east-west minor arterial road with a 2-lane cross-section and a posted speed limit of 60 km/h. There is a discontinuity along Kirby Road between Dufferin Street and Bathurst Street. Currently, there is minimal development along the westerly section of Kirby Road between Keele Street and Jane Street. The easterly section from Jane Street to Dufferin Street includes substantial residential development to the south.

With regards to the existing road geometrics, the existing horizontal alignment from east to west is generally tangent with an offset intersection at Jane Street and an approximate 1,250m radius reverse curve to the east of the Keele Street intersection. The existing profile follows a rolling topography with approximate grades ranging from 0.30% and 11.50% (which exceeds the Region's maximum desirable vertical grade of 8%) with crest curve K values ranging from 4 to 28 (which does not meet the minimum 26 K_{crest} value for an 80 km/h Design Speed) and sag curve K values ranging from 2 to 15 (which does not meet the minimum 12 K_{sag} value for a 80 km/h Design Speed).

As shown in **Table 5**, the 2016 two-way AADT volume in this section of Kirby Road (between Highway 400 and Jane Street) was 2,878 veh/day. The typical vehicle carrying capacity of a single lane on Kirby Road is approximately 700 veh/h.

Table 5: Traffic Characteristics along Kirby Road

| Location Description | AADT (vpd) |
|----------------------|--------------|
| Hwy 400 to Jane St | 2,878 (2016) |
| Jane St to Keele St | 3,787 (2011) |



3.1.3 Major Mackenzie Drive (York Regional Road 25)

Major Mackenzie Drive (York Regional Road 25) is an east-west arterial road with an interchange at Highway 400. Currently, Major Mackenzie Drive has a 4-lane cross-section and a posted speed limit of 60 km/h and is identified in the York Region TMP as a future Rapid Transit corridor. Currently, Major Mackenzie Drive is fully urbanized and generally surrounded by residential and commercial lands on both sides between Highway 400 and Bathurst Street.

With regards to the existing road geometrics, the existing horizontal alignment from east to west begins with a reverse curve with approximate radii of 1250m between Highway 400 to the east of Jane Street. It is then tangent between Jane Street and Keele Street where a tight 175m reverse curve shifts the road to the north. The alignment then generally follows a tangent until the west of Dufferin Street where a 1350m curve shifts the road to the south. The road continues on a tangent until ending in a 1250m curve at the Bathurst Street intersection. The existing profile follows a rolling topography with approximate grades ranging from 0.30% and 10.50% (which exceeds the Region's maximum desirable vertical grade of 8%) with crest curve K values ranging from 1 to 16 (which does not meet the minimum 26 K_{crest} value for an 80 km/h Design Speed) and sag curve K values ranging from 1 to 14 (which does not meet the minimum 12 K_{sag} value for a 80 km/h Design Speed).

As shown in **Table 6**, the AADT volume in this section of Major Mackenzie Drive (between Highway 400 and Bathurst Street) was in the range of 34,336 to 63,533 veh/day. The field measured 85th percentile speed was in the order of 62-86 km/h. The typical vehicle carrying capacity of a single arterial traffic lane on Major Mackenzie Drive is in the order of 800 to 900 veh/h.

Table 6: Traffic Characteristics along Major Mackenzie Drive

| Location Description | AADT (vpd) | 85 th Percentile Speed (kph) |
|----------------------------|---------------|---|
| Hwy 400 to Jane St | 63,533 (2019) | 70 |
| Jane St to Keele St | 58,053 (2018) | 70 |
| Keele St and Dufferin St | 34,336 (2019) | 62 |
| Dufferin St to Bathurst St | 35,176 (2018) | 86 |

3.1.4 Bathurst Street (York Regional Road 38)

Bathurst Street (York Regional Road 38) is a north-south major urban arterial road with a 4-lane cross section and a posted speed limit of 60 km/h. Currently, Bathurst Street is fully urbanized and generally surrounded by residential and natural heritage lands on both sides between Major Mackenzie Drive and Kirby Road.

With regards to the existing road geometrics, the existing horizontal alignment from south to north is generally tangent throughout from Major Mackenzie Drive to Kirby Road. The existing profile follows a rolling topography with approximate grades ranging from 0.30% and 8% with crest curve K values ranging from 1 to 15 (which does not meet the minimum $26 \text{ K}_{\text{crest}}$ value for an 80 km/h Design Speed) and sag



curve K values ranging from 1 to 27 (which does not meet the minimum 12 K_{sag} value for a 80 km/h Design Speed).

As shown in **Table 7**, the AADT in this section of Bathurst Street (between Rutherford Road and King Vaughan Road) was in the range of 24,518 to 38,877 veh/day. The field measured 85th percentile speed was 74 km/h. The typical vehicle carrying capacity of a single arterial traffic lane on Bathurst Street is in the order of 900 to 1,200 veh/h.

Table 7: Traffic Characteristics along Bathurst Street

| Location Description | AADT (vpd) | 85 th Percentile Speed (kph) |
|---|---------------|---|
| Rutherford Rd IC to Major Mackenzie Dr | 37,672 (2019) | 74 |
| Major Mackenzie Dr to Mill St/Queen Filomena Ave | 38,877 (2018) | 74 |
| Oxford St/Lady Dolores Ave and Elgin Mills Rd/Teston Rd | 34,478 (2019) | 74 |
| Teston Rd to Kirby Road | 33,838 (2018) | 74 |
| Kirby Road to King Vaughan Rd | 24,518 (2019) | n/a |

3.1.5 Dufferin Street (York Regional Road 53)

Dufferin Street (York Regional Road 53) is a north-south minor arterial road with a 2-lane cross section and a posted speed limit of 60 km/h. Currently, Dufferin Street is generally surrounded by residential and natural heritage lands including golf courses on both sides between Major Mackenzie Drive and Kirby Road.

With regards to the existing road geometrics, the existing horizontal alignment from south to north is generally tangent throughout from Major Mackenzie Drive to Kirby Road. The existing profile follows a rolling topography with approximate grades ranging from 0.30% and 12.50% (which exceeds the Region's maximum desirable vertical grade of 8%) with crest curve K values ranging from 1 to 15 (which does not meet the minimum 26 K_{crest} value for an 80 km/h Design Speed) and sag curve K values ranging from 1 to 18 (which does not meet the minimum 12 K_{sag} value for a 80 km/h Design Speed).

As shown in **Table 8**, the AADT in this section of Dufferin Street (between Rutherford Road and King Vaughan Road) was in the range of 9,491 to 29,671 veh/day. The field measured 85th percentile speed was in the order of 79-94 km/h. The typical vehicle carrying capacity of a single arterial traffic lane on Dufferin Street is in the order of 900 to 1,000 veh/h.

Table 8: Traffic Characteristics along Dufferin Street

| Location Description | AADT (vpd) | 85 th Percentile Speed (kph) |
|--|---------------|---|
| Rutherford Rd IC to Major Mackenzie Dr | 29,671 (2019) | 79 |
| Major Mackenzie Dr to Teston Rd | 18,553 (2018) | 79 |
| Hunterwood Chase to Beakes Cres | 14,430 (2019) | 84 |



| Location Description | AADT (vpd) | 85 th Percentile Speed (kph) |
|-----------------------------|---------------|---|
| Athabasca Dr and Kirby Rd | 12,051 (2018) | 84 |
| Kirby Rd to King Vaughan Rd | 9,491 (2019) | 94 |

3.1.6 Keele Street (York Regional Road 6)

Keele Street (York Regional Road 6) is a north-south urban arterial road with a 4-lane cross section and a posted speed limit of 50 km/h. Currently, Keele Street is generally surrounded by residential and agricultural lands as well as industrial lands to the north-east and south-east of the Teston Road intersection.

With regards to the existing road geometrics, the existing horizontal alignment from south to north is generally tangent throughout from Major Mackenzie Drive to Kirby Road. The existing profile follows a rolling topography with approximate grades ranging from 0.30% and 7.10% with crest curve K values ranging from 1 to 24 (which certain areas do not meet the minimum 17 K_{crest} value for a 70 km/h Design Speed) and sag curve K values ranging from 1 to 24 which do not meet the minimum 10 K_{sag} value for a 70 km/h Design Speed).

As shown in **Table 9**, the AADT in this section of Keele Street (between Rutherford Road and King Vaughan Road) was in the range of 14,032 to 21,957 veh/day. The field measured 85th percentile speed was in the order of 69-80 km/h. The typical vehicle carrying capacity of a single arterial traffic lane on Keele Street is in the order of 800 to 1,000 veh/h.

 Table 9: Traffic Characteristics along Keele Street

| Location Description | AADT (vpd) | 85 th Percentile Speed (kph) |
|--|---------------|--|
| Dina Rd and Cromwell Rd/Fieldgate Dr | 19,151 (2018) | 69 |
| Naylon St and Church St. Mid-Block Pedestrian Crossing | 20,095 (2018) | 80 |
| Major Mackenzie Dr W and Railway St/Killian Rd | 21,957 (2019) | 80 |
| Maple Health Centre and Drummond Dr | 19,357 (2018) | 76 |
| Teston Rd to Kirby Rd | 15,234 (2019) | 78 |
| Kirby Rd to King Vaughan Rd | 14,032 (2018) | 78 |

3.1.7 Jane Street (York Regional Road 55)

Jane Street (York Regional Road 55) is a north-south urban arterial road with a 4-lane cross section and a posted speed limit of 60 km/h. Currently, Jane Street is generally surrounded by residential and commercial lands between Major Mackenzie Drive and Teston Road and undeveloped agricultural lands between Teston Road and Kirby Road.

With regards to the existing road geometrics, the existing horizontal alignment from south to north is generally tangent throughout from Major Mackenzie Drive to Kirby



Road. The existing profile is fairly flat and follows a rolling topography with approximate grades ranging from 0.30% and 3.90% with crest curve K values ranging from 1 to 37 (which does not meet the minimum 26 K_{crest} value for an 80 km/h Design Speed) and sag curve K values ranging from 1 to 25 (which does not meet the minimum 12 K_{sag} value for a 80 km/h Design Speed).

As shown in **Table 10**, the AADT in this section of Jane Street (between Rutherford Road and King Vaughan Road) was in the range of 6,837 to 36,093 veh/day. The field measured 85th percentile speed was in the order of 73-97 km/h. The typical vehicle carrying capacity of a single arterial traffic lane on Jane Street is in the order of 900 to 1,000 veh/h.

85th Percentile Speed **Location Description** AADT (vpd) (kph) Rutherford Rd and Auto Vaughan Dr 27,619 (2019) 84 Avro Rd and Major Mackenzie Dr W 27,493 (2018) 80 Major Mackenzie Dr and Roseheath Dr/Grand Valley Blvd 36,093 (2019) 80 Ahmadiyya Ave and Teston Rd 12,374 (2018) 73 Teston Rd and Kirby Rd 6,837 (2019) 98 Kirby Rd and King Vaughan Rd 6,888 (2018) 97

Table 10: Traffic Characteristics along Jane Street

3.1.8 Highway 400

Highway 400 is a Controlled Access Highway under the jurisdiction of MTO, which traverses through the study area in a north/south direction. Highway 400 is considered regionally and provincially significant, serving as an important link between the GGH area and Simcoe County to the north. It also connects Highway 401 in southern Ontario to central and northern Ontario/western Canada via Highway 69 and Highway 11, respectively. Highway 400 has a 6-lane cross section and includes two interchanges within the study area at Major Mackenzie Drive West and Teston Road.

Table 11 illustrates pertinent traffic information along Highway 400 which provides a glimpse of traffic characteristics at each section. Summer traffic (2016 SADT) was approximately 22% higher than the two-way Annual Average Daily Traffic (2016 AADT) volume in this section of Highway 400. In the Pattern Type column: "CTR" refers to "Commuter Tourist Recreation".

Table 11: Traffic Characteristics along Highway 400

| Location Description | Pattern Type | 2016 AADT | 2016 SADT |
|---|--------------|-----------|-----------|
| Rutherford Rd IC to Major Mackenzie Dr IC | CTR | 158,900 | 193,800 |
| Major Mackenzie Dr IC to Teston Rd IC | CTR | 132,400 | 161,500 |
| Teston Rd IC to York Rd 11 IC | CTR | 119,200 | 145,400 |



3.2 Existing Signalized Intersections

As shown in **Figure 3**, there are currently 18 key signalized intersections within the study area summarized below:

- Kirby Road and Jane Street Intersection;
- Kirby Road and Keele Street Intersection;
- Kirby Road and Dufferin Street Intersection;
- Kirby Road and Bathurst Street Intersection;
- Teston Road and Cityview Boulevard Intersection;
- Teston Road and Highway 400 S-E/W Ramp Terminal;
- Teston Road and Jane Street Intersection:
- Teston Road and Cranston Park Avenue Intersection;
- Teston Road and Keele Street Intersection;
- Teston Road and Dufferin Street Intersection;
- Teston Road and Via Romano Boulevard;
- Teston Road and Bathurst Street Intersection;
- Major Mackenzie Drive and Highway 400 N-E/W Ramp Terminal;
- Major Mackenzie Drive and Highway 400 S-E/W Ramp Terminal;
- Major Mackenzie Drive and Jane Street Intersection;
- Major Mackenzie Drive and Keele Street Intersection;
- Major Mackenzie Drive and Dufferin Street Intersection; and
- Major Mackenzie Drive and Bathurst Street Intersection.

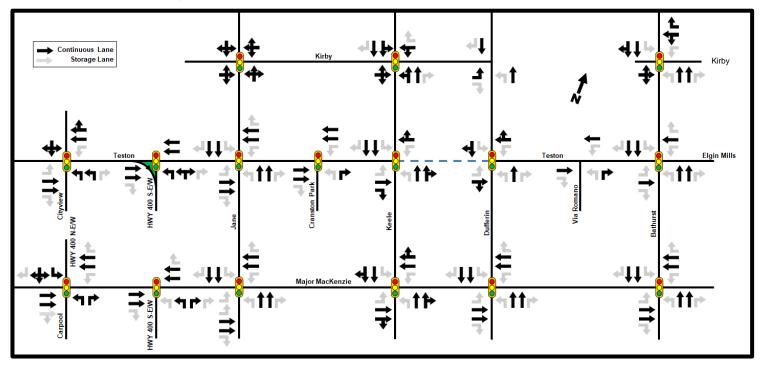


Figure 3: Existing Intersections within Traffic Analysis Study Area



3.3 Transit

Figure 4 illustrates existing York Region transit network. The existing GO, Viva, and YRT network within the study area is described below.

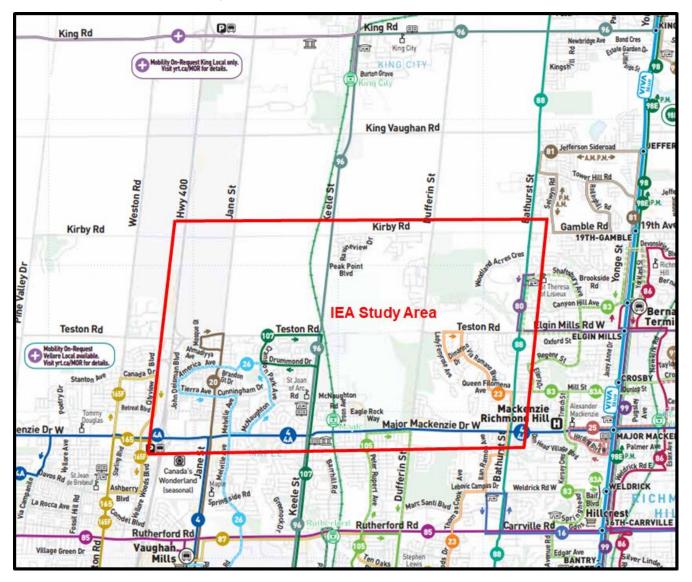


Figure 4: Existing York Region Transit Network (June 2020)

3.3.1 GO Transit

The Barrie GO rail corridor is one of the seven train lines of the GO Transit system in the Greater Toronto Area. It extends from Union Station in Toronto in a generally northward direction to Barrie, and includes ten stations along its 101.4 km route. Within the study area the GO Barrie rail corridor services the City of Vaughan with stops at King City, Maple (just north of Major MacKenzie Drive) and Rutherford (Refer to **Figure 4**).



King City GO Station is situated south of the intersection of Keele Street and King Vaughan Road. The existing 12-car accessible platform, station building and parking lot are located along the west side of the rail corridor. The existing parking lot includes accessible parking and can accommodate 468 vehicles. There is currently no Passenger Pick-up and Drop-off (PPUDO) facility at this location and the bus access is adjacent to the station's main parking lot on Keele Street. The existing King City GO Station has one mainline track that is accessed from the east side platform.

Maple GO Station is situated east of the intersection of Keele Street and Major Mackenzie Drive. The existing 12-car accessible platform, station building and parking lot are located along the east side of the rail corridor. The existing parking lot can accommodate 1,239 vehicles and includes a PPUDO area as well as a bus loop and accessible parking. The existing Maple GO Station has one mainline track that is accessible from the east side platform.

Rutherford GO Station is situated east of the Rutherford Road and Keele Street intersection. The existing 12-car accessible platform, station building and parking lot are located along the west side of the rail corridor. The existing parking lot can accommodate 978 vehicles and includes a PPUDO area as well as a bus loop and accessible parking. The existing Rutherford GO Station has one mainline track that is accessible from the west side platform.

The current train departure schedule from King City, Maple and Rutherford stations is shown in **Table 12**.

| King (| City | Ma | aple | Ruthe | erford |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| AM Trains (SB) | PM Trains (NB) | AM Trains (SB) | PM Trains (NB) | AM Trains (SB) | PM Trains (NB) |
| 5:52 AM | 5:19 PM | 5:59 AM | 5:11 PM | 6:03 AM | 5:07 PM |
| 6:37 AM | 5:49 PM | 6:44 AM | 5:41 PM | 6:48 AM | 5:37 PM |
| 7:22 AM | 6:34 PM | 7:29 AM | 6:26 PM | 7:33 AM | 6:22 PM |
| 8:07 AM | 7:34 PM | 8:14 AM | 7:26 PM | 8:18 AM | 7:22 PM |
| 9:07 AM | 8:34 PM | 9:14 AM | 8:26 PM | 9:18 AM | 8:22 PM |

Table 12: GO Train Departure Times (Monday to Friday)

The Barrie GO corridor, which sees more than 9,000 passenger trips each day, is preparing for future expansion. For expanded service, all existing platforms will be maintained and improvements will include an additional side platform and second track at all three above mentioned stations.

Based on the Barrie Rail Corridor Expansion Project, Transit Project Assessment Process, Environmental Project Report (approved in August 2017), Metrolinx announced five new GO Stations for the Barrie rail corridor in June 2016. These stations were endorsed by each municipality and received Municipal Council resolution approvals in November 2016. The new GO Stations include:

- Spadina (at Front Street) in the City of Toronto;
- Bloor-Davenport (Bloor Street near Lansdowne Avenue) in the City of Toronto;



- Kirby (near Keele Street) in the City of Vaughan;
- Mulock (near Bayview Avenue) in the Town of Newmarket; and
- Innisfil (at 6th Line) in the Town of Innisfil.

Kirby GO Station will be located south of Kirby Road approximately 300 metres west of Keele Street, with access from both sides of the Barrie GO rail corridor in the City of Vaughan. The Kirby GO Station will provide a stop between the Maple GO Station and the King City GO Station. Based on the Kirby GO Station Transpiration and Traffic Impact Analysis (completed in 2018), proposed components of the Kirby GO Station are:

- Three station access structures including a main station building to the east of the rail corridor and secondary station entrances east and west of the rail corridor;
- Two side platforms;
- Three rail tracks through the station, including a centre express track and two gauntlet tracks;
- Two pedestrian tunnels providing access across the corridor;
- Three bicycle parking areas;
- A bus loop;
- A passenger PPUDO area;
- A 1,000-space surface parking lot;
- Three non-signalized vehicular access points (two off of Keele Street and one off of Kirby Road). The north Keele Street access point will include dedicated bus lanes, vehicular lanes and pedestrian and cyclist access; and
- Multi-Use Path (MUP) connection to the planned TransCanada MUP trail south of the station.

3.3.2 VIVA Service

The following Viva Bus Service currently operates within the Traffic Analysis Study Area:

 Viva Blue runs along Yonge Street between Finch Go Bus Terminal and Newmarket Terminal, further described in **Table 13**.

Table 13: Existing VIVA Service within the Traffic Study Area

| Route No. | Service Corridor | Service Direction | From | То | Service Type | Peak/Off-Peak Frequency |
|--------------|---------------------|----------------------|--------------------------|-----------------------|-----------------|---|
| Viva Blue | Yonge Street | North-South | Finch Go Bus Terminal | Newmarket Terminal | Arterial | Finch Go Bus Terminal to Newmarket Terminal: |



3.3.3 York Region Transit (YRT) Service

Table 14 presents the existing and future transit routes within the study areas. The transit data provided below reflects October 2019 conditions, pre-COVID-19 pandemic.

Overall, there are 17 transit routes within the study area. Viva Blue, which operates within dedicated transit lanes along the Yonge Street BRT corridor, provides the shortest headway and most frequent service. There is a total average of 50,314 passenger boardings during a typical weekday for all routes shown below. Approximately 9% of all passengers are using Route 20 along Jane Street and 8% are using Route 4/4A along Major Mackenzie Drive. The predominant route is the Viva Blue along Yonge Street with 33% of all passenger-boardings on it.

Table 14: Existing and Future Transit Routes (October 2019)

| Route | 2019 Average Weekday Daily | 2 | g (October 019) | | Planned 041) | |
|------------------------|-------------------------------|--------|--------------------|-------|-----------------|--|
| Noute | Passenger | Weekda | Weekday Headway | | Weekday Headway | |
| | Boarding | Peak | Off-Peak | Peak | Off-Peak | |
| 4/4A - Major Mackenzie | 4,120 | 14 | 19 | 14 | 15 | |
| 16 - 16th Avenue | 1,645 | 30 | 30 | 15 | 15 | |
| 20 - Jane | 4,632 | 12 | 19 | 12 | 15 | |
| 23 - Thornhill Woods | 610 | 33 | 60 | 20 | - | |
| 26 - Maple | 1,311 | 16-20 | 46 | 16-20 | 46 | |
| 80 - Elgin Mills | 515 | 29 | 50 | 15 | 15 | |
| 81 - Inspiration | 193 | 29 | - | 29 | - | |
| 83/83A - Trench | 1,045 | 35 | 37 | 20 | 20 | |
| 85/85C - Rutherford | 3,486 | 15 | 30 | 15 | 15 | |
| 88 - Bathurst | 4,064 | 15 | 15 | 12 | 12 | |
| 96 - Keele-Yonge | 2,413 | 25-32 | 33 | 15 | 15 | |
| 98 - Yonge | 768 | 38 | 52 | 15 | 15 | |
| 99 - Yonge | 1,798^ | 32 | 51 | 15 | 15 | |
| 105 - Dufferin | 2,467 | 16 | 28 | 15 | 15 | |
| 107 - Keele | 2,720^ | 19 | 41 | 15 | 15 | |
| 165/165F - Weston | 2,111 | 15-19 | 44 | 15 | 15 | |
| Viva blue | 16,416 | 8 | 9 | 4 | 4 | |

^{*} Note: Ridership data based on the entire length of the route.

The existing and proposed transit routes along all major arterial roads within the study area is described below:

3.3.3.1 Teston Road (York Region Road 49)

Based on York Region Transit (YRT) Map (Refer to **Figure 4**), YRT local Route is only available on Teston Road in four short sections at Jane Street (Route 20), Keele Street (Route 107), Thornhill Woods (Route 23) and Elgin Mills (Route 80).

Figure 5 illustrates the proposed transit network in the 2016 TMP for the year 2041. Teston Road will be served by frequent transit service.



[^] Note: Ridership data includes associated branch routes (i.e. Route 98/99 - Yonge (Late Night) & Route 107B - Keele).

3.3.3.2 Kirby Road (City of Vaughan)

Currently transit is available on Kirby Road in a short section at Keele Street (Route 96) and along Bathurst Street (Route 88). Based on Figure 6, Kirby Road will be served by frequent transit service.

The GO Transit rail corridor crosses through Kirby Road west of Keele Street, with King City Station being the closest terminal. The City of Vaughan is supporting Metrolinx's GO Expansion program along the Barrie GO Rail Corridor to increase train frequency to provide all-day, two-way services and the future Kirby GO Station at Kirby Road/Keele Street.

3.3.3.3 Major Mackenzie Drive (York Regional Road 25)

Major Mackenzie Drive within the study area is primarily serviced along the whole corridor by YRT local Route 4/4A beginning at the Vaughan Mills Terminal. Short segments of other YRT routes travel along Major Mackenzie Drive including, Route 26 (Melville Avenue to McNaughton Road) and Route 105 (Peter Rupert Avenue to Dufferin Street).

The GO Transit rail corridor crosses through Major Mackenzie Drive east of Keele Street, with Maple Station being the closest terminal. The forthcoming plan for Major Mackenzie Drive is to provide VIVA curbside service until around 2026 before being transformed to a dedicated rapidway beyond 2027.

3.3.3.4 Bathurst Street (York Regional Road 38)

Bathurst Street is primarily serviced by YRT local Route 88 which travels between GO Transit's Finch terminal and Seneca College's King Campus. Other transit routes that intersect along short segments of Bathurst Street include Route 23 (Queen Filomena Avenue to Valley Vista Drive), and Route 80 and 83 (Elgin Mills Road to Shaftsbury Avenue).

Based on **Figure 5**, Bathurst Street will be served by frequent transit service.

3.3.3.5 Dufferin Street (York Regional Road 53)

There are no transit routes which travel along Dufferin Street within the study area between Major Mackenzie Drive and Kirby Road. Based on **Figure 5**, Dufferin Street will be served by frequent transit service.

3.3.3.6 Keele Street (York Regional Road 6)

Keele Street is primarily serviced by YRT local Route 96 which travels between TTC's Pioneer Village Station, Go Transit's King City Station,



and YRT's Newmarket terminal. Other transit routes that travel along Keele Street include YRT's local Route 107 which primarily travels along Keele Street, originating from TTC's Pioneer Village Station and loops through the residential community in the southwest corner of the Teston Road intersection. Based on **Figure 5**, Keele Street will be served by frequent transit service.

3.3.3.7 Jane Street (York Regional Road 55)

Transit on Keele Street is limited to YRT Route 20 which travels between TTC's Pioneer Village Station to the south and loops through the residential community in the southwest corner of the Teston Road intersection. Based on **Figure 5**, Jane Street will be served by frequent transit service.

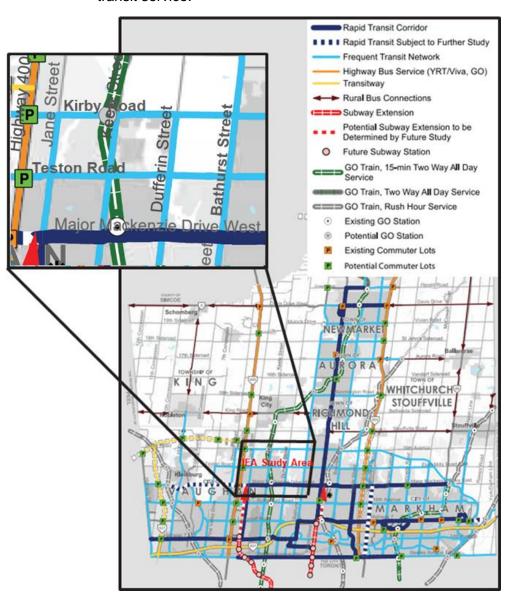


Figure 5: York Region Recommended Transit Network for 2041 (2016 TMP)



3.4 Modal Share by Ward / Zone

3.4.1 2016 Transportation Tomorrow Survey

As shown in **Figure 6**, the Traffic Analysis study area is within Wards 1, 3 and 4 of City of Vaughan.

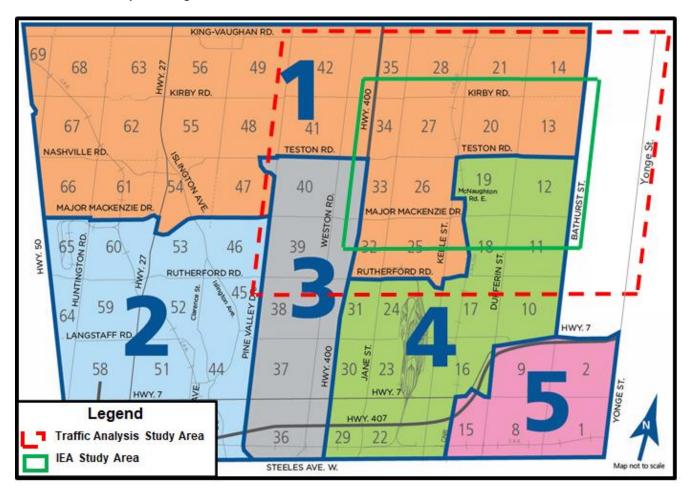


Figure 6: City of Vaughan Ward Area Map

To better identify the opportunities for modal shift, mode share data from the 2016 Transportation Tomorrow Survey (TTS) was extracted for trips made by residents of City of Vaughan within Wards 1, 3 and 4 (Refer to **Appendix A**).

As shown in **Table 15** the current combined Transit and GO Train ridership during the AM peak period is in the order of ten (10) percent of all trips (97,400) made by residents of City of Vaughan within Wards 1, 3 and 4.

Six (6) percent of trips are walking and/or cycle trips. Also, thirteen (13) percent of trips are made by passengers in vehicles driven by someone else.



Table 15: Trips Made by Residents of City of Vaughan (6:00 – 9:00 AM)

| | | | Mode of Travel | | | | | |
|--------|---------|--------|----------------|---------|----------|-----------------|-------|--|
| Trips | % 24 hr | Driver | Pass | Transit | GO Train | Walk & Cycle | Other | |
| Ward 1 | | | | | | · | | |
| 34,900 | 27.0% | 66% | 13% | 4% | 4% | 5% | 8% | |
| Ward 3 | | | | | | | | |
| 32,700 | 28.2% | 69% | 13% | 6% | 2% | 7% | 2% | |
| Ward 4 | | | | | | | | |
| 29,800 | 29.2% | 65% | 12% | 8% | 5% | 7% | 3% | |
| Total | | | | | | | | |
| 97,400 | - | 67% | 13% | 6% | 4% | 6% | 5% | |

As shown in **Table 16**, mode share data from the 2016 TTS was extracted for trips made by residents of the TTS area to City of Vaughan (Wards 1, 3 and 4). It is evident that approximately four (4) percent of all trips (112,300) by residents of the TTS area are using Transit and GO Train during the AM peak period to get into City of Vaughan (Wards 1, 3 and 4).

Five (5) percent of trips are walking and/or cycle trips. Also, eleven (11) percent of trips are made by passengers in vehicles driven by someone else.

Table 16: Trips Made to City of Vaughan by Residents of the TTS Area (6:00 – 9:00 AM)

| | | Mode of Travel | | | | | |
|---------|---------|----------------|------|---------|----------|-----------------|-------|
| Trips | % 24 hr | Driver | Pass | Transit | GO Train | Walk & Cycle | Other |
| Ward 1 | | | | | | Ĭ | |
| 17,200 | 18.60% | 67% | 17% | 2% | 1% | 9% | 4% |
| Ward 3 | | | | | | | |
| 33,100 | 26.10% | 74% | 12% | 3% | 1% | 7% | 3% |
| Ward 4 | | | | | | | |
| 62,000 | 35.50% | 83% | 9% | 4% | 1% | 3% | 1% |
| Total | | | | | | | |
| 112,300 | - | 78% | 11% | 3% | 1% | 5% | 2% |

3.4.2 York Region Travel Demand Forecasting Models (EMME)

The Region's current 2016 Travel Demand Forecasting Model (TDFM) is an a.m. peak period model, predicting both auto and transit demands between 6:00 a.m. and 8:59 a.m. This 3-hour a.m. peak period is considered to be most representative of morning peak period travel and has been adopted as a GTA standard for travel demand forecasting¹. The Region's current 2016 TDFM was calibrated at the Regional screenline level using data from the 2011 TTS.

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¹ For auto trips, conversion factors are required to transform the a.m. peak period demand to the a.m. peak hour demand for assignment purpose.

The 2031 and 2041 road networks were developed based on the 2006 network with the addition of road widenings and extensions across the Greater Toronto and Hamilton Area (GTHA) that have been committed to by both the provincial and municipal governments to address transportation needs and support future growth in the study area.

For the purpose of this study, York Region provided Subarea EMME Models for years 2016, 2031 and 2041. As mentioned in **Section 1.2**, the limits of subarea models were extended to include Yonge Street, Pine Valley Drive, King Vaughan Road and Rutherford Road (Refer to **Figure 1**).

Table 17 illustrates the 3-hour a.m. peak period demand for all internal traffic zones within 2016, 2031 and 2041Subarea Models (EMME).

For the origin trips produced within the subarea model, auto trips and transit trips are expected to increase by approximately 53% and 99%, respectively, from 2016 to 2041. Transit mode share is projected to increase from 11% to 14% over this period.

For the destination trips produced within the subarea model, auto trips and transit trips are expected to increase by approximately 75% and 126%, respectively from 2016 to 2041. Transit mode share is projected to remain at 4% over this period.

Table 17: AM 3-hour Peak Period Travel Demand Forecasts for Study Area

| Trips | Year | 20 | 16 | 2031 | | 1 2041 | |
|--------------|--------------------|--------|---------|--------|---------|---------|---------|
| TTIPS | Mode | Auto | Transit | Auto | Transit | Auto | Transit |
| Origins | Total | 75,843 | 9,492 | 97,316 | 16,135 | 115,649 | 18,853 |
| Origins | Transit Mode Share | | 11% | | 14% | | 14% |
| Destinations | Total | 43,227 | 1,591 | 62,551 | 2,950 | 79,596 | 3,591 |
| Destinations | Transit Mode Share | | 4% | | 5% | | 4% |

Figures 7 and **8** illustrate the origin and destination trips at the traffic zone level from the York Region TDFM for the years 2016 and 2041, respectively, during the AM peak hour. Green bars depict the trip production; red bars depict trip attractions. As shown in both figures, the majority of trips originate from east and south of the study area.



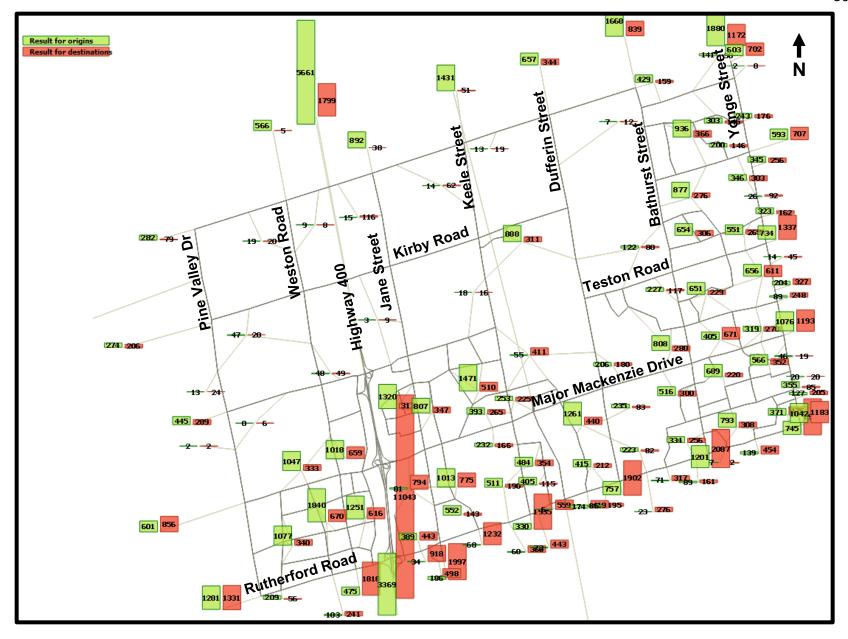


Figure 7: Origin and Destination Trips at Traffic Zone Level (2016 Subarea EMME Model)



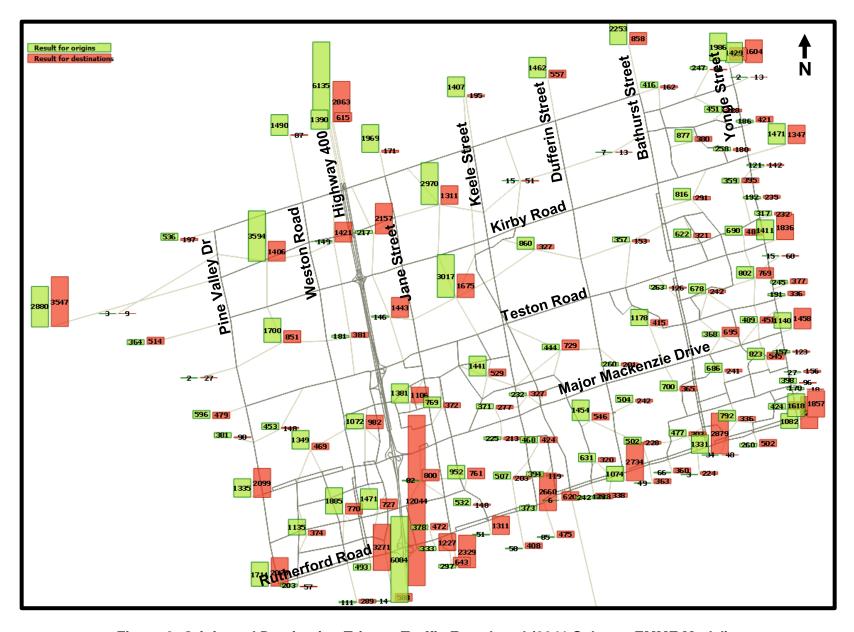


Figure 8: Origin and Destination Trips at Traffic Zone Level (2041 Subarea EMME Model)



3.5 Goods Movement

Based on York Region proposed strategic good movement network, Highway 400 and Kirby Road are designated as highway and primary arterial corridors to accommodate goods movement demands, respectively. However, Teston Road, Major Mackenzie Drive, Jane Street, Keele Street, Dufferin Street and Bathurst Street are identified as secondary arterial good movement corridors (Refer to **Figure 9)**.

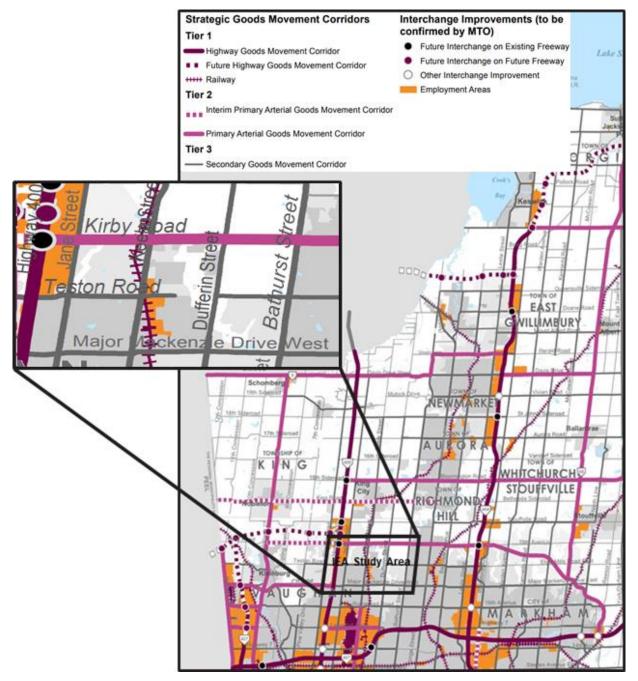


Figure 9: York Region Proposed Strategic Good Movement Network for 2041 (2016 TMP)



3.6 Active Transportation

3.6.1 Teston Road (York Region Road 49)

Teston Road is currently urban with curbs without any cycling facilities along Teston Road between Highway 400 and Keele Street. Pedestrian facilities are only provided on the south side of Teston Road with a 1.5m concrete sidewalk with a landscaping boulevard west of Jane Street and a 3.0m multiuse pathway with a grassed boulevard east of Jane Street to Keele Street. Between Keele Street and Rodinea Drive, Teston Road has a rural cross-section with wide shoulders and barely defined ditches. Between Dufferin Street and Bathurst Street, a semi-urban cross-section is present with a curb and gutter, boulevard and sidewalk on the south side and a shoulder and ditch on the north side.

Currently there are no cycling facilities on Teston Road and cyclists share the travel lanes with vehicular traffic. **Figure 10** illustrate the proposed cycling network in 2016 TMP for the year 2041. Separate facilities will be provided along Teston Road between Weston Road and Jane Street and between Keele Street and Dufferin Street to protect cyclists from vehicular traffic.

A detailed breakdown for the evaluation of the active transportation facilities on Teston Road is provided in **Section 3.10**.

3.6.2 Kirby Road (City of Vaughan)

The road cross-section is currently rural without any cycling facilities along Kirby Road. Narrow shoulders offer limited space for users and disabled vehicles. A concrete sidewalk, path, trail (Multi Use Path) of approximately 2.0 meters in width is available on the south side beyond the ditch from Keele Street to Dufferin Street. Utility poles and some vegetation are located relatively close to the edge of pavement. There is also a gated at-grade crossing of the Barrie GO Rail line approximately 300 m west of Keele Street.

Exclusive bike lanes are available on both sides of the roadway on Kirby Road.

As shown in **Figure 10** Kirby Road (between Highway 27 and Dufferin Street) will be a component of the overall bicycle network for York Region.

3.6.3 Major Mackenzie Drive (York Regional Road 25)

The road is currently urban with curbs without any cycling facilities along Major Mackenzie Drive between Highway 400 and Peter Rupert Avenue. The road becomes a rural cross-section with shoulders between Peter Rupert Avenue and Bathurst Street. A concrete sidewalk is present on both the north and south side from Highway 400 to Dufferin Street. The north sidewalk continues until Sir Benson Drive. The sidewalks resume from the west of Ilan Ramon Boulevard to Bathurst Street.



As shown in **Figure 10** separate facilities will be provided along Major Mackenzie Drive from west of Highway 27 to Woodbine Avenue to protect cyclists from vehicular traffic.

3.6.4 Bathurst Street (York Regional Road 38)

The road is currently urban with curbs without any bicycle facilities along Bathurst Street between Major Mackenzie Drive and the north of Teston Road. At this point, the road becomes semi-urban with shoulder on the west side and curb and boulevard on the east side. Bathurst Street becomes fully rural at the intersection of Shaftsbury Avenue. A concrete sidewalk is present on the east side from Major Mackenzie Drive to Mill Street at which point a sidewalk on both sides is present until Teston Road. The eastern sidewalk continues until it terminates at Shaftsbury Avenue.

As shown in **Figure 10** separate facilities will be provided along Bathurst Street between Steeles Avenue and Kirby Road to protect cyclists from vehicular traffic.

3.6.5 Dufferin Street (York Regional Road 53)

The road is currently rural with wide paved shoulders which double as bicycle facilities along Dufferin Street between Major Mackenzie Drive and Kirby Road. A concrete sidewalk is only present on the east side for the segment between Major Mackenzie Drive and Eagles Landing Road. There are no plans to improve bicycle facilities along Dufferin Street within the study area by 2041.

3.6.6 Keele Street (York Regional Road 6)

The road is generally urban with sidewalks on both sides from Major Mackenzie Drive to McNaughton Road. The west side sidewalk continues to Teston Road. Keele Street then becomes a rural road with gravel shoulders to the north of Teston Road beyond the Barrie GO Line grade separation structure. Dedicated on-street bike lanes are present on Keele Street between Masters Avenue to the north of McNaughton Road.

As shown in **Figure 10** dedicated facilities will be provided along Keele Street between Rutherford Road and Kirby Road to protect cyclists from vehicular traffic.

3.6.7 Jane Street (York Regional Road 55)

The road is fully urban with sidewalks on both sides from Major Mackenzie Drive to Teston Road. The east sidewalk continues for approximately 500m north of Teston Road where it terminates. North of Teston Road, Jane Street then becomes a rural road with gravel shoulders until Kirby Road.



As shown in **Figure 10** separate facilities will be provided along Jane Street from Major Mackenzie Drive to Teston Road to protect cyclists from vehicular traffic.

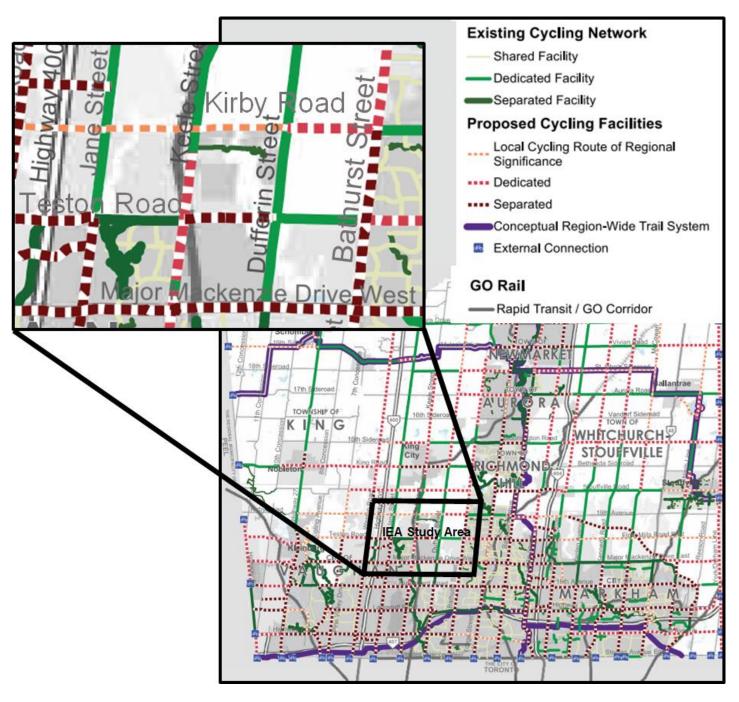


Figure 10: York Region Recommended Cycling Network for 2041 (2016 TMP)



3.7 Existing Traffic Data

A variety of traffic data was obtained from York Region in order to complete the traffic analysis provided herein. Detailed copies of the traffic data are provided in **Appendix B**.

- Traffic Volume Information System (TVIS-2010 to 2019) Data: The TVIS data spreadsheet included historical AADT for all midblock segments within the Traffic Analysis Study Area.
- Advance Traffic Management Systems (ATMS) Data: Automatic Traffic Recorder (ATR) Counts for all midblock segments from the designated ATMS traffic counting stations.
- Turning Movement Counts (TMC): The most recent TMCs at all ramp terminals/intersections along Teston Road between Highway 400 and Bathurst Street.
- Signal Timing Plans: The most recent signal timing plans at all ramp terminals/intersections along Teston Road between Highway 400 and Bathurst Street.
- **2018 2019 Speed Data**: The most recent field measured speed data for all arterial roads within the study area.
- 2015 2019 Automatic Identification System (AIS): The collision summary at all intersections and midblocks within the Traffic Analysis Study Area.
- 2016, 2031 and 2041 Subarea EMME Models: 2016, 2031 and 2041 (with and without GTA West) subarea Travel Demand Forecasting models (EMME).

3.8 Existing Traffic Volumes

The most recent turning movement count (2011 - 2019) volumes at all ramp terminals/intersections along Teston Road between Highway 400 and Bathurst Street were balanced and used for turning distributions.

The development of existing volumes for the year 2020 included a review of travel demand forecasts from the EMME sub-area models provided by York Region. The EMME model data provided was for the 2016 year and 2041 base year and includes various stages of planned development (i.e. new roadways, trip generators, etc.) within a 25-year window. Based on the review of the travel demand forecasts, an annual growth rate of 1% was selected for the development of the 2020 volume condition (i.e. existing conditions). The morning peak hour traffic volumes for this horizon year are illustrated in **Figure 11**.



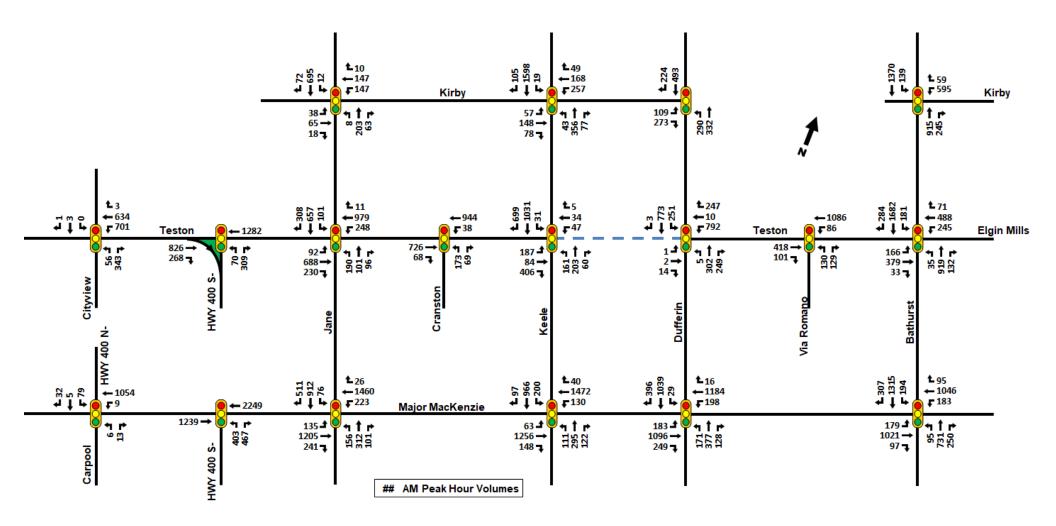


Figure 11: Existing Traffic Volumes (2020)



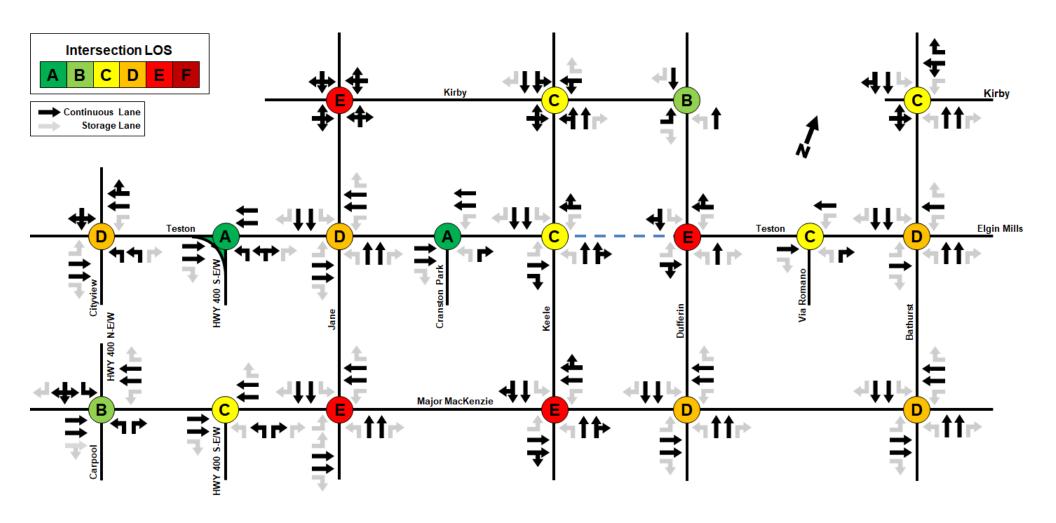


Figure 12: Existing Intersection Operational Performance (2020)



3.9 Existing Intersection Operational Performance Analysis (2020)

An evaluation of the performance of the signalized intersections within the study area was completed using Synchro 10 for the existing conditions (2020) during the morning peak hour.

The following assumptions are based on City of Vaughan Transportation Impact Study Guidelines (2018) and were used within the analysis:

- Saturation flow rate 1,900 vphpl;
- Peak Hour Factor (PHF) 0.97 (based on a review of traffic counts). A PHF of 1.00 was applied at movements exceeding capacity;
- Lost time: 5.0 seconds for main phases and 1.0 seconds for advance phases;
- Growth Rate 1% per year; and
- Percent Commercial Vehicles obtained from traffic data provided (per movement).

The summary of the traffic assessment is shown in **Table 18**. Detailed Synchro reports are provided in **Appendix C**. As shown in **Table 18** below, the existing condition includes several turning movements operating at, or slightly above, capacity along with congested and failing conditions (LOS E and F) as a result of delays experienced during the AM peak hour within the study area. Intersection performance within the study area was noted to be at a LOS E or better based on overall delay (see **Figure 12**).

Table 18: Intersection Performance – Existing Conditions (2020) – AM Peak Hour

| Intersections | Movements | Delay (s) | LOS | v/c Ratio | 95th Queue (m) |
|------------------------|-----------|-----------|-----|-----------|----------------|
| | EBL | 0 | Α | 0.00 | 0 |
| | EBT | 44 | D | 0.64 | 210 |
| | EBR | 41 | D | 0.45 | 90 |
| | WBL | 80 | E | 1.01 | 260 |
| Teston / Cityview | WBTR | 4 | Α | 0.25 | 44 |
| | NBL | 66 | E | 0.25 | 17 |
| | NBR | 67 | E | 0.25 | 34 |
| | SBLTR | 72 | E | 0.05 | 5 |
| | Overall | 46 | D | 0.75 | - |
| | EBT | 8 | Α | 0.39 | 37 |
| | EBR | 1 | Α | 0.18 | 0 |
| Teston / Highway 400 | WBT | 10 | Α | 0.60 | 69 |
| restorr/ riigriway 400 | NBLR | 25 | С | 0.19 | 15 |
| | NBR | 25 | С | 0.18 | 19 |
| | Overall | 10 | Α | 0.51 | - |
| | EBL | 33 | С | 0.45 | 24 |
| | EBT | 44 | D | 0.67 | 114 |
| | EBR | 36 | D | 0.16 | 20 |
| | WBL | 33 | С | 0.69 | 59 |
| Teston / Jane | WBT | 42 | D | 0.79 | 152 |
| reston / Jane | WBR | 28 | С | 0.01 | 0 |
| | NBL | 25 | С | 0.55 | 52 |
| | NBT | 20 | В | 0.07 | 15 |
| | NBR | 20 | В | 0.06 | 11 |
| | SBL | 29 | С | 0.21 | 37 |



| Intersections | Movements | Doloy (c) | LOS | v/c Ratio | 05th Ougus (m) |
|---------------------|------------------|-------------------|--------|---------------------|-----------------------|
| intersections | Movements SBT | Delay (s) 33 | C | 0.48 | 95th Queue (m) 104 |
| | SBR | 33 31 | C | 0.46 | 57 |
| | Overall | 36 | D | 0.53 | - - |
| | EBT | | A | 0.30 | 36 |
| | EBR | 6 4 | A | 0.30 | 4 |
| | WBL | 4 5 | A | 0.03 | 6 |
| Teston / Cranston | WBT | 6 | | | 49 |
| resion / Cransion | NBL | | A | 0.39 0.56 | 49 49 |
| | | 38 | D C | | |
| | NBR | 33 9 | | 0.05 0.42 | 11 |
| | Overall EBL | 36 | A D | 0.42 | - 61 |
| | EBT | 36 42 | D | | |
| | | | _ | 0.18 | 35 |
| | EBR | 49 | D | 0.46 | 67 |
| | WBL | 39 | D | 0.17 | 19 |
| Tantan / Maria | WBTR | 46 | D | 0.10 | 19 |
| Teston / Keele | NBL | 23 | C | 0.58 | 31 |
| | NBTR | 15 | В | 0.14 | 22 |
| | SBL | 22 | С | 0.06 | 12 |
| | SBT | 32 | С | 0.63 | 152 |
| | SBR | 30 | С | 0.50 | 47 |
| | Overall | 32 | C | 0.55 | - |
| | EBL | 39 | D | 0.00 | 1 |
| | EBTR | 44 | D | 0.01 | 7 |
| | WBL | 85 | F | 1.06 | 311 |
| | WBTR | 26 | С | 0.19 | 20 |
| Teston / Dufferin | NBL | 33 | С | 0.09 | 4 |
| | NBT | 38 | D | 0.49 | 93 |
| | NBR | 12 | В | 0.18 | 9 |
| | SBL | 34 | C | 0.64 | 62 |
| | SBTR Overall | 72 57 | E E | 1.00 0.99 | 301 |
| | EBT | 7 | A | 0.39 | 36 |
| | EBR | 5 | A | 0.39 | 4 |
| | WBL | 6 | A | 0.07 | 9 |
| Teston / Via Romano | WBT | 35 | Č | 0.10 | 189 |
| restorry via Romano | NBL | 19 | В | 0.36 | 23 |
| | NBR | 18 | В | 0.30 | 10 |
| | Overall | 23 | C | 0.82 | - |
| | EBL | 101 | F | 0.97 | 81 |
| | EBT | 62 | E | 0.81 | 156 |
| | EBR | 42 | D | 0.03 | 0 |
| | WBL | 146 | F | 1.13 | 105 |
| | WBT | 101 | F | 1.02 | 221 |
| | WBR | 42 | D | 0.05 | 8 |
| Teston / Bathurst | NBL | 95 | F | 0.73 | 32 |
| restorr/ Datridist | NBT | 26 | Ċ | 0.53 | 116 |
| | NBR | 19 | В | 0.09 | 11 |
| | SBL | 19 | В | 0.56 | 34 |
| | SBT | 28 | Č | 0.82 | 238 |
| | SBR | 15 | В | 0.22 | 23 |
| | Overall | 46 | D | 0.89 | - |
| Major Masters 15 / | EBTR | 14 | В | 0.74 | 238 |
| Major MacKenzie / | WBL | 11 | В | 0.11 | 2 |
| Highway 400 West | WBT | 7 | Ā | 0.42 | 82 |
| Ramp | NBL | 69 | Ε | 0.16 | 7 |



| Intono at the second | Mayamanta | Dolou (a) | 1.00 | v/a Datin | OF4h O |
|----------------------|-----------|------------|--------------------|---------------------|----------------|
| Intersections | Movements | Delay (s) | LOS | v/c Ratio | 95th Queue (m) |
| | NBR | 67 | E | 0.01 | 0 |
| | SBL | 69 | E | 0.37 | 27 |
| | SBLTR | 69 | E | 0.38 | 27 |
| | SBR | 65 | E | 0.03 | 0 |
| | Overall | 13 | В | 0.67 | - |
| | EBT | 9 | Α | 0.50 | 114 |
| Major MacKenzie / | WBT | 14 | В | 0.90 | 431 |
| Highway 400 East | NBL | 65 | E | 0.69 | 77 |
| Ramp | NBR | 69 | E | 0.76 | 78 |
| | Overall | 23 | С | 0.88 | - |
| | EBL | 69 | Ē | 0.48 | 34 |
| | EBT | 50 | D | 0.82 | 204 |
| | EBR | 70 | Ē | 0.18 | 35 |
| | WBL | 70 | Ē | 0.87 | 94 |
| | WBT | 47 | D | 0.90 | 262 |
| | WBR | 24 | C | 0.04 | 11 |
| Major MacKenzie / | NBL | 6 2 | Ē | 0.04 0.81 | 73 |
| Jane | | | | | |
| | NBT | 45 | D | 0.33 | 57 |
| | NBR | 42 | D | 0.07 | 10 |
| | SBL | 35 | C | 0.21 | 27 |
| | SBT | 72 | E | 0.93 | 193 |
| | SBR | 84 | F | 0.94 | 199 |
| | Overall | 58 | E | 0.90 | - |
| | EBL | 37 | D | 0.42 | 20 |
| | EBTR | 60 | E | 0.96 | 285 |
| | WBL | 51 | D | 0.69 | 49 |
| Major MacKanzia / | WBTR | 61 | E | 0.97 | 320 |
| Major MacKenzie / | NBL | 52 | D | 0.69 | 49 |
| Keele | NBTR | 48 | D | 0.43 | 74 |
| | SBL | 32 | С | 0.47 | 60 |
| | SBTR | 62 | E | 0.91 | 207 |
| | Overall | 57 | E | 0.90 | - |
| | EBL | 93 | F | 0.97 | 86 |
| | EBT | 46 | D | 0.85 | 181 |
| | EBR | 31 | Ċ | 0.27 | 40 |
| | WBL | 72 | Ē | 0.90 | 86 |
| | WBT | 47 | D | 0.88 | 199 |
| | WBR | 26 | C | 0.01 | 0 |
| Major MacKenzie / | NBL | 65 | F | 0.87 | 72 |
| Dufferin | NBT | 29 | C | 0.28 | 52 |
| | | 29 27 | E C C | | 13 |
| | NBR | | C | 0.09 | |
| | SBL | 24 | | 0.07 | 10 |
| | SBT | 44 | D | 0.82 | 164 |
| | SBR | 36 | D | 0.53 | 88 |
| | Overall | 46 | D | 0.88 | - |
| | EBL | 70 | E | 0.88 | 81 |
| | EBT | 60 | E | 0.92 | 191 |
| | EBR | 1 | A | 0.06 | 0 |
| | WBL | 65 | E E | 0.87 | 80 |
| Major MacKenzie / | WBT | 61 | E | 0.93 | 196 |
| Bathurst | WBR | 33 | С | 0.07 | 14 |
| | NBL | 31 | С | 0.51 | 28 |
| | NBT | 31 | С | 0.52 | 97 |
| | NBR | 27 | 0000 | 0.21 | 25 |
| | SBL | 24 | С | 0.57 | 42 |
| | | | | | |



| Intersections | Movements | Delay (s) | LOS | v/c Ratio | 95th Queue (m) |
|------------------|-----------|-----------|-----|-----------|----------------|
| Intersections | SBT | 46 | D | 0.90 | 210 |
| | SBR | 28 | C | 0.30 | 42 |
| | Overall | 46 | D | 0.86 | + <u>/</u> |
| | EBLTR | 111 | F | 0.90 | 72 |
| | WBLTR | 93 | F | 0.99 | 148 |
| Kirby / Jane | NBLTR | 25 | Ċ | 0.37 | 70 |
| Taby / Jane | SBLTR | 53 | D | 0.94 | 279 |
| | Overall | 61 | E | 0.95 | - |
| | EBLTR | 29 | Ċ | 0.57 | 78 |
| | WBLT | 62 | Ĕ | 0.94 | 158 |
| | WBR | 22 | Ċ | 0.03 | 8 |
| | NBLT | 18 | В | 0.39 | 41 |
| Kirby / Keele | NBR | 14 | В | 0.05 | 7 |
| | SBLT | 36 | D | 0.93 | 234 |
| | SBR | 15 | В | 0.07 | 8 |
| | Overall | 35 | C | 0.93 | - |
| | EBL | 52 | D | 0.51 | 43 |
| | EBR | 48 | D | 0.18 | 24 |
| | NBL | 6 | Α | 0.44 | 38 |
| Kirby / Dufferin | NBT | 4 | Α | 0.23 | 29 |
| • | SBT | 5 | Α | 0.34 | 47 |
| | SBR | 4 | Α | 0.14 | 5 |
| | Overall | 14 | В | 0.46 | - |
| | EBLTR | 0 | Α | 0.00 | 0 |
| | WBL | 30 | С | 0.50 | 84 |
| | WBLT | 30 | С | 0.50 | 84 |
| | WBR | 24 | С | 0.04 | 2 |
| Kirby / Bathurst | NBL | 0 | Α | 0.00 | 0 |
| Kirby / Bathurst | NBT | 25 | С | 0.58 | 101 |
| | NBR | 20 | В | 0.23 | 29 |
| | SBL | 16 | В | 0.44 | 23 |
| | SBTR | 22 | С | 0.72 | 145 |
| | Overall | 24 | С | 0.67 | - |
| | | | | | |

Note: LOS is based on average vehicle delays

3.10 Active Transportation Facility Assessment on Teston Road

The evaluation of the active transportation facilities for Teston Road was performed using the York Region's Transportation Mobility Plan Guidelines (November 2016). Although the Transportation Mobility Plan Guidelines are directed towards development applications, the evaluation process would be similar for assessing the performance and quality for all road users including pedestrians, cyclists, transit users and vehicles. For this assessment, the evaluation of the active transportation facilities was performed at each major intersection crossing of Teston Road and the roadway segments in-between. Please refer to **Appendix D** for a more detailed breakdown for the evaluation of the active transportation facilities on Teston Road.

A description of the active transportation facility assessment is described below for each mode.

 Automobile LOS: The automobile LOS is evaluated based on the intersection delays and capacity outputs from Section 3.9. The automobile



LOS was determined for each approach based on assigning a letter designation ranging from 'A' to 'F', representing the traffic conditions from free flow to congested. The target automobile LOS for York Region is LOS 'D' or better for both intersection delay and capacity.

- Transit LOS: The transit LOS is evaluated based on the transit headway and
 the performance of the transit vehicles at the intersection approach. The
 evaluation assesses the transit vehicles ability to navigate and interact with
 other vehicles along the roadway corridor and the quality of service that is
 provided to transit users. The target transit LOS for York Region is LOS 'C'
 or better for transit headway and LOS 'D' or better for transit intersection
 performance.
- Pedestrian LOS: The pedestrian LOS is evaluated based on the presence of
 pedestrian facilities at the intersection or roadway segments. The
 assessment evaluates the pedestrian facility based on the type of facility,
 sidewalk and buffer width, presence of a crosswalk and pedestrian signal
 heads to provide a safe and comfortable experience. The target pedestrian
 LOS for York Region is LOS 'C' or better which indicates the presence of at
 least a 1.5m sidewalk with no buffer, crosswalk, and pedestrian signal head.
- Bicycle LOS: The bicycle LOS is evaluated based on providing a facility that
 all bicyclists feel comfortable and safe. The assessment evaluates the bicycle
 facility based on the type of facility (i.e. separated, dedicated, or shared),
 facility width, presence of a buffer, and bicycle treatments at the intersection
 (bike box, signal heads, etc...). The target bicycle LOS for York Region is
 LOS 'C' or better which indicates a dedicated bicycle facility that is less than
 1.8m with no buffer and bicycle treatments.

3.10.1 Teston Road and Jane Street

A summary of the Multimodal Level of Service (MMLOS) results for the signalized intersection at Teston Road and Jane Street is shown below in **Table 19**. The MMLOS summary table identifies the LOS for each respective transportation mode by approach and identifies the approach(es) which do not meet the LOS targets established by York Region for each approach.

Table 19: MMLOS Intersection Summary at Teston Road and Jane Street

| | | | Intersection | Approach ¹ | |
|------------|--------------------------|--------|--------------|-----------------------|--------|
| Level of S | Level of Service Summary | | Street | Teston Road | |
| | | NB | SB | EB | WB |
| | Level of Service | С | С | D | D |
| Automobile | (Delay in seconds) | (25) | (33) | (44) | (42) |
| Automobile | Critical Movement | NBL | SBT | EBT | WBT |
| | [v/c ratio] | [0.55] | [0.48] | [0.67] | [0.79] |
| Transit | Transit Headway | N/A | N/A | С | N/A |
| Halloit | Intersection Approach | N/A | N/A | D | N/A |
| Pedestrian | Intersection | В | F | В | F |
| Bicycle | Intersection | F | D | F | F |

¹ All modes evaluated in direction of travel for each intersection approach.



Automobile LOS – The intersection of Teston Road and Jane Street operates acceptably in the morning peak hour with a LOS 'D' as shown in **Section 3.9**. Based on the four approaches to the intersection, all achieve the target LOS 'D'. The configuration of the existing intersection includes an auxiliary left and right turn lane at each approach. Additionally, the current signal timing for the intersection includes protected-permitted left turn movements from all approaches with the exception of the southbound direction.

Transit LOS – Apart from the south leg of Jane Street, Teston Road and Jane Street are not classified as part of York Region's Frequent Transit Network per York Regions TMP Map 12. At the intersection of Teston Road and Jane Street, the local community in the southwest corner of the intersection is serviced by YRT Local Route #20 which operates in a mixed traffic lane. YRT Route #20 runs north-south along Jane Street between Teston Road and TTC's Subway Line 1 Pioneer Village station providing intermediate connections to YRT's SmartVMC bus terminal and TTC's Highway 407 subway station. YRT's SmartVMC bus terminal provides transfers to Viva and Brampton Zum transit services that use the Highway 7 rapidway. At the intersection, the only current transit movement for Route #20 is the eastbound right turn as the route returns south towards the start at Pioneer Village, which meets the minimum LOS targets of 'C' and 'D', respectively, for transit headway and performance (delay & v/c ratio).

Pedestrian LOS – Along Teston Road in the eastbound direction and along Jane Street in the northbound direction, pedestrian facilities are provided resulting in a LOS 'B'. The sidewalk on the eastbound approach is 1.5m wide with a 1.0m grassed boulevard. For the northbound approach, a 1.5m wide sidewalk is buffered by the travelled lanes by a 1.0m wide grassed boulevard. which is mirrored on the west side. Both these sidewalks connect to a 3.0m multi-use pathway on the south side of Teston Road between Jane Street to Keele Street. In the southbound and westbound directions, the pedestrian LOS is failing since no facilities are provided in the primary direction of travel. At the intersection, pedestrian signal heads and painted crosswalks are provided on all approaches to indicate when it is safe to cross. Furthermore, a short-depressed sidewalk section is provided, at a minimum, on all intersection curb returns to allow pedestrians to provide refuge beyond the roadway. The pedestrian realm in the southeast and southwest corners of the intersection have enhanced facilities with additional landscaping, benches, and bike racks. Furthermore, the establishment of sidewalks current at the intersections and on the approaches is based on the presence of nearby residential and commercial developments. The gaps in the existing pedestrian network, notably along both edges of the northwest quadrant, abut undeveloped agricultural farmland.

Bicycle LOS – Bicycle facilities are only provided on the southbound approach to the intersection of Teston Road and Jane Street in the form of a narrow (<1.5m) dedicated bike lane resulting in a LOS 'D'. The remainder of the approaches do not have a cycling facility resulting in a failing LOS 'F'. The lack of cycling cross-rides at the intersection, in addition to the absence or narrow width of the existing cycling facilities, does not encourage the average



recreational cyclist from using this intersection as part of their cycling route. This intersection represents the southern end of the cycling network on Jane Street extending from Davis Drive West to the north as shown in York Regions TMP Map 10, providing only a connection to the multi-use pathway on Teston Road east of Jane Street towards Keele Street.

3.10.2 Teston Road between Jane Street to Keele Street

A summary of the MMLOS results for the segment of Teston Road between Jane Street and Keele Street is shown below in **Table 20**. The MMLOS summary table identifies the LOS for each respective transportation mode by segment and identifies the approach(es) which do not meet the LOS targets established by York Region for each approach.

Table 20: MMLOS Segment Summary between Jane Street to Keele Street

| | Level of Service Summary | | κ Segment |
|-------------------|----------------------------|--------|-----------|
| Le | | | n Road |
| | | EB | WB |
| | Level of Service | D | D |
| Automobile | (Delay in seconds)12 | (49) | (42) |
| Automobile | Critical Movement | EBR | WBT |
| | [v/c ratio] ^{1 2} | [0.46] | [0.79] |
| Transit | Transit Headway | N/A | N/A |
| Hansii | Intersection Approach | N/A | N/A |
| Pedestrian | Segment | Α | F |
| Bicycle | Segment | Α | F |

¹ EB segment delay and v/c ratio are for the EB approach to Keele Street.

Automobile LOS – The mid-block segment of Teston Road between Jane Street to Keele Street has a five lane cross section with the fifth lane being a two-way left-turn lane (TWLTL), providing access to properties fronting onto Teston Road, reducing delays caused by left turning vehicles. The LOS in both directions during the AM peak hour currently operates at an appropriate LOS 'D' or better with additional capacity available for the critical movements. The LOS for the eastbound direction is based on the eastbound approach to Keele Street while the westbound direction is based on the westbound approach to Jane Street.

Transit LOS – Teston Road between Jane Street to Keele Street is not designated as a transit corridor per York Regions TMP Map 12. The sole transit route using this corridor is YRT Local Route #107 which uses the section between Cranston Park Avenue to Keele Street and operates in mixed traffic. The transit route serves the communities on the south side of Teston Road which represent the northernmost residential community between Jane Street to Keele Street. Since there are no continuous transit routes along this section of Teston Road, the transit LOS targets are not achieved.

Pedestrian LOS – The roadway segment along Teston Road between Jane Street and Keele Street includes a 3.0m separated multi-use pathway



² WB segment delay and v/c ratio are for the WB approach to Jane Street.

separated from the travelled lanes by a grassed boulevard with no pedestrian facilities on the north side. The pedestrian LOS along this segment is LOS 'A' in the eastbound direction but LOS 'F' in the westbound direction. However, the multi-use pathway on the south side of Teston Road can currently serve the pedestrian needs in both directions along the corridor as majority of the pathway users are presumed to live in the abutting communities primarily located on the south side of the corridor while the north side mainly consists of undeveloped agricultural farmland. Access to the multi-use pathway on the south side of the corridor is provided by the network of trails and sidewalks in the residential community to the south and at the mid-block intersections.

Bicycle LOS – Similar to the pedestrian LOS, the bicycle LOS in the eastbound direction is LOS 'A' with a failing LOS 'F' in the opposing westbound direction. The separated multi-use pathway on the south side of Teston Road in the corridor serves cyclists needs in both directions complementing the side where most residents live, providing a comfortable facility for users of all ages and experiences.

3.10.3 Teston Road and Keele Street

A summary of the MMLOS results for the signalized intersection at Teston Road and Jane Street is shown below in **Table 21**. The MMLOS summary table identifies the LOS for each respective transportation mode by approach and identifies the approach(es) which do not meet the LOS targets established by York Region for each approach.

Table 21: MMLOS Intersection Summary at Teston Road and Keele Street

| Level of Service Summary | | Intersection Approach 1 | | | | | |
|--------------------------|-------------------------------|-------------------------|------------|-------------|----------------|--|--|
| | | Keele | Street | Teston Road | | | |
| | | NB | SB | EB | WB | | |
| | Level of Service | С | С | D | D | | |
| Automobile | (Delay in seconds) | (23) | (32) | (49) | (46) | | |
| Automobile | Critical Movement [v/c ratio] | NBL [0.58] | SBT [0.63] | EBR [0.46] | WBTR [0.10] | | |
| Transit | Transit Headway | E/F | E/F | D | N/A | | |
| Halloll | Intersection Approach | В | С | D | N/A | | |
| Pedestrian | Intersection | F | F | Α | F | | |
| Bicycle | Intersection | F | F | Α | F | | |

¹ All modes evaluated in direction of travel for each intersection approach.

Automobile LOS – The intersection of Teston Road and Keele Street operates acceptably in the morning peak hour with a LOS 'C', as shown in **Section 3.9**. Based on the four approaches to the intersection, all achieve the target LOS 'D'. The configuration of the current intersection includes an auxiliary left turn lane on all approaches with the north and west approach having an additional dedicated right turn lane. The current signal timing plan for the intersection includes protected-permitted left turn movements for all approaches except the southbound left which operates with a permitted left turn movement.



Transit LOS - Transit at the intersection of Teston Road and Keele Street is provided by YRT Local Route #96 & #107. YRT Route #96 travels in the north-south direction along Keele Street while YRT Route #107 performs an eastbound right turn at the intersection, both operating in mixed traffic. Based on York Region's TMP Map 12, only the south section of Jane Street is considered part of the Frequent Transit Network. Normally, YRT Route #107 travels along Keele Street between Teston Road and TTC's Subway Line 1 Pioneer Village station. However, exclusively during the weekday, YRT Route #107B services the Rutherford GO transit station. YRT Route #96 similarly begins at Pioneer Village travelling between the YRT's Newmarket Terminal servicing GO Transit's King City transit station along the way. At the intersection, the transit headway is 19 minutes for Route #107 and ranges between 25 - 32 minutes for Route #96, during the weekday peak hour, resulting in LOS that exceeds the target LOS 'C'. However, the transit performance at the intersection for the critical movements for each route meet the minimum target LOS 'D'.

Pedestrian LOS – Pedestrian facilities are limited at the intersection of Teston Road and Keele Street with a LOS 'F' for all approaches except the eastbound approach with a LOS 'A'. In the eastbound direction, the multi-use pathway along the south side of Teston Road from Jane Street connects into the intersection at Keele. In this southwest corner, there is a large refuge area for pedestrians indicating the Village of Maple. Along the section of Keele Street south of Teston Road, a 1.5m wide sidewalk extends south on the west side of the road. In the northwest and southwest corner of the intersection, only a short section of sidewalk is provided for a connection to the nearby bus stop pad. In the northeast corner of the intersection, only a depressed / mountable curb is provided without a sidewalk. On all approaches, depressed curbs, painted crosswalks and pedestrian crossing signal heads are provided. Therefore, based on the conditions described above, there are many existing gaps in the pedestrian network at this intersection.

Bicycle LOS – The bicycle LOS at all approaches for the intersection of Teston Road and Keele Street are LOS 'F' except for the eastbound approach. In the eastbound direction, the multi-use pathway provides a cycling connection to the intersection resulting in a bicycle LOS 'A' for the approach. The remainder of the approaches lack any form of a cycling facility towards the intersection, resulting in a LOS 'F'. Based on York Region's TMP Map 4 - Existing Cycling Network, there are existing bicycle facilities on Keele Street, albeit discontinuous on both approaches to Teston Road. However, in the Region's proposed 10 year (TMP Map 10), they have identified a dedicated cycling facility connecting the cycling facilities on Keele as well as a separate facility from Keele extending towards Dufferin Street.

3.10.4 Teston Road and Dufferin Street

A summary of the MMLOS results for the signalized intersection at Teston Road and Jane Street is shown below in **Table 22**. The MMLOS summary table identifies the LOS for each respective transportation mode by approach



and identifies the approach(es) which do not meet the LOS targets established by York Region for each approach.

Table 22: MMLOS Intersection Summary at Teston Road and Dufferin Street

| | | | Intersection | n Approach ¹ | |
|------------|-------------------------------|------------|---------------|-------------------------|------------|
| Level of S | Level of Service Summary | | Street | Teston | Road |
| | | NB | SB | EB | WB |
| | Level of Service | D | Е | D | F |
| Automobile | (Delay in seconds) | (38) | (72) | (44) | (85) |
| Automobile | Critical Movement [v/c ratio] | NBT [0.49] | SBT [1.00] | EBTR [0.01] | WBL [1.06] |
| Transit | Transit Headway | N/A | N/A | N/A | N/A |
| Halloll | Intersection Approach | N/A | N/A | N/A | N/A |
| Pedestrian | Intersection | F | F | В | F |
| Bicycle | Intersection | В | В | F | D |

¹ All modes evaluated in direction of travel for each intersection approach.

Automobile LOS – The overall intersection LOS for the intersection of Teston Road and Dufferin Street operates with a LOS 'E' during the morning peak hour, as summarized in **Section 3.9**. The southbound and westbound approaches currently fail to meet the target LOS 'D'. For the northbound and eastbound approaches, the LOS targets are achieved. The configuration of the intersection at Teston Road and Dufferin Street includes a dedicated left turn auxiliary lane and a through-right lane on three of the four approaches with the northbound approach having a dedicated lane for each left, through and right movement. Based on the current signal timing plan, the northbound left turn is the only movement with a permitted phasing with the remainder of the left turns protected-permitted.

Transit LOS – No transit facilities are present at the intersection of Teston Road and Dufferin Street and as a result cannot be evaluated.

Pedestrian LOS – Pedestrian facilities are limited at the intersection of Teston Road and Dufferin Street with a LOS 'F' for all approaches except the eastbound approach which has a 1.5m sidewalk with a grassed buffer approaching the intersection. The eastbound approach has a LOS 'B'. Based on York Region's TMP Map 5, the section west of the intersection has been identified as a potential active transportation link. At the intersection, pedestrian signal heads and painted crosswalks are present on all corners and approaches. At each corner, a section of sidewalk is provided with depressed curbs and tactile walking surface indicators at the crosswalk locations. In the immediate vicinity of the intersection, sidewalks are not provided since majority of the land in the northeast, southeast and southwest corner are either agricultural farmland or undisturbed woodland. The gaps in the pedestrian network are notable with the development of residential subdivisions beyond the intersection in the northwest and southeast quadrants. Additional pedestrian facilities on the approaches to the intersection can serve to connect the off-road trail networks in each community.



Bicycle LOS – Cycling facilities are provided on three of the approaches (northbound, southbound, and westbound) to the intersection at Teston Road and Dufferin Street in the form on on-street paved shoulder bike lanes. The existing bike lanes on the approach legs are approximately 1.5 – 2.0m wide. In both directions on Dufferin Street, the bicycle LOS is 'B'. On Teston Road, the LOS in the eastbound direction is 'F' due to the lack of bicycle facilities, while the LOS in the westbound direction is 'D' with a 1.5m paved shoulder bike lane.

3.10.5 Teston Road between Dufferin Street to Bathurst Street

A summary of the MMLOS results for the segment of Teston Road between Dufferin Street and Bathurst Street is shown below in **Table 23**. The MMLOS summary table identifies the LOS for each respective transportation mode by segment and identifies the approach(es) which do not meet the LOS targets established by York Region for each approach.

Table 23: MMLOS Segment Summary between Dufferin Street to Bathurst Street

| Level of Service Summary | | Mid-Block Segment Teston Road | | |
|--------------------------|--|-------------------------------|------------|--|
| | | EB | WB | |
| Automobile | Level of Service (Delay in seconds) 12 | F (101) | F (85) | |
| Automobile | Critical Movement [v/c ratio] 1 2 | EBL [0.97] | WBL [1.06] | |
| Transit | Transit Headway | N/A | N/A | |
| Halloll | Intersection Approach | N/A | N/A | |
| Pedestrian | Segment | F | F | |
| Bicycle | Segment | D | D | |

¹ EB segment delay and v/c ratio are for the EB approach to Bathurst Street.

Automobile LOS – The mid-block segment of Teston Road between Dufferin Street and Bathurst Street has a three lane cross section with the third lane being a two-way left turn lane (TWLTL), providing access to residential properties and side streets, reducing the delays caused by left turning vehicles with the single lane in the eastbound and westbound directions. The LOS in both directions is LOS 'F' based on the delays and v/c ratios approaching each of the respective intersections. The LOS for the eastbound direction is based on the eastbound approach to Bathurst Street while the westbound direction is based on the westbound approach to Dufferin Street.

Transit LOS – Teston Road between Jane Street to Keele Street is not designated as a transit corridor per York Region's TMP Map 12. The sole transit route using this corridor is YRT Local Rush Hour Only Route #23 which uses the section between Lady Fenyrose Avenue to Via Romano Boulevard and operates in mixed traffic. The transit route serves the communities on the south side of Teston Road, providing transit services to the schools and shopping malls between Go Transit's Finch terminal and Teston Road. The transit connection at Go Transit's Finch terminal also provides access to the TTC's Finch subway station and line. Since there are



² WB segment delay and v/c ratio are for the WB approach to Dufferin Street.

no continuous transit routes along this section of Teston Road, the transit LOS targets are not achieved.

Pedestrian LOS – The majority of Teston Road between Dufferin Street and Bathurst Street does not have any pedestrian facilities except for a section east of Torah Gate adjacent to the Forest View Park subdivision. The pedestrian facility between Torah Gate and Bathurst Street is a 1.5m wide sidewalk with a varying grassed boulevard approximately 6.5m wide which connects to a sidewalk that runs parallel to Teston Road in the Forest View Park subdivision. Since there is no continuous pedestrian facility along this section of Teston Road, the pedestrian LOS targets are not achieved.

Bicycle LOS – Cycling facilities are present in both directions along the whole section of Teston Road between Dufferin Street and Bathurst Street in the form of dedicated paved shoulder bike lanes. The width of the shoulder bike lanes is approximately 1.5m along this segment with no buffer to the travelled lanes resulting in a LOS 'D'. The cycling facilities provide a continuous connection between Dufferin Street and Bathurst Street, albeit there are no cycling facilities at Bathurst Street per York Region's TMP Map 4.

3.10.6 Teston Road and Bathurst Street

A summary of the MMLOS results for the signalized intersection at Teston Road and Jane Street is shown below in **Table 24**. The MMLOS summary table identifies the LOS for each respective transportation mode by approach and identifies the approach(es) which do not meet the LOS targets established by York Region for each approach.

Table 24: MMLOS Intersection Summary at Teston Rd / Elgin Mills Rd and Bathurst St

| Level of Service Summary | | Intersection Approach ¹ | | | | | |
|--------------------------|---|------------------------------------|------------|-------------|------------|--|--|
| | | Bathurs | t Street | Teston Road | | | |
| | | NB | SB | EB | WB | | |
| Automobile | Level of Service (Delay in seconds) | F (95) | C (28) | F (101) | F (146) | | |
| Automobile | Critical Movement <i>[v/c ratio]</i> | NBL [0.73] | SBT [0.82] | EBL [0.97] | WBL [1.13] | | |
| Transit | Transit Headway | С | E | N/A | F | | |
| Transit | Intersection Approach | С | С | N/A | D | | |
| Pedestrian | Intersection | В | В | В | В | | |
| Bicycle | Intersection | F | F | F | F | | |

¹ All modes evaluated in direction of travel for each intersection approach.

Automobile LOS – The intersection of Teston Road and Bathurst Street operates acceptably in the morning peak hour with a LOS 'D' as shown in **Section 3.9**. However, only the southbound approach meets the automobile LOS target of 'D'. The remaining three legs of the intersection all experience long delays greater than the 80 second with the accompanying critical movements operating at LOS 'F'. The configuration of the existing intersection includes a dedicated right and left turn lane in addition to the through lanes.



Transit LOS – Although Dufferin Street is not part of the York Region's Frequent Transit Network per York Regions TMP Map 12, the section of Bathurst Street north and south of Teston Road is. The intersection of Teston Road is serviced by 3 of York Region Transit's local routes including Route #80, 83 and 88. All of these transit routes operate in mixed traffic. YRT Route #80 runs along Elgin Mills Road West between the Elgin West Community Center and Woodbine Avenue to the east. YRT Route #83 which uses the intersection at Teston Road and Bathurst Street is a Limited Service weekday route which runs between YRT's Bernard and Richmond Hill terminals while passing by the Mackenzie Richmond Hill hospital. YRT Route #88 is a local route which runs primarily along Bathurst Street between Go Transit's Finch terminal and Seneca College's King Campus, with stops at YRT's Promenade bus terminal. From the current transit data, the transit LOS target is only met for the northbound approach. However, in terms of transit performance, the LOS target of 'D' is achieved by all approaches.

Pedestrian LOS – At the intersection of Teston Road and Bathurst Street, the pedestrian LOS target is achieved for all approaches. On all of the approaches, the pedestrian facilities include a minimum of a 1.5m concrete sidewalk separated by a grassed boulevard approximately 2.0m wide which narrows approaching the intersection. Furthermore, all intersection approaches include a painted crosswalk with pedestrian signal heads on each corner. Additionally, the sidewalks are depressed at all curb returns ensuring accessibility to the pedestrian facilities for all users.

Bicycle LOS – Contrary to the pedestrian facilities being provided on all approaches to the intersection of Teston Road and Bathurst Street, there are however no cycling facilities resulting in a LOS 'F'. The shoulder bike lanes that are present on Teston Avenue from Dufferin Street do not continue to the intersection. In the area around the intersection per York Region's TMP Map 4, there are limited and discontinuous cycling facilities providing not much desire for bicyclists to use this intersection as part of their bike route.

3.11 Collisions Review

General historical collision records from AIS were obtained from York Region for all arterial roads within the study area for a 5-year period between 2015 to 2019. The collision history database provides the detail of collisions reported within the project limits, including details such as the time and location, classification, environment (weather and light condition), as well as other related information to describe the collision event.

3.11.1 Teston Road (York Region Road 49)

There was a total of 300 collisions on Teston Road between Cityview Boulevard and Bathurst Street for the 5-year period. **Figure 13** illustrates the number of collisions by each year. The average number of collisions per year are 60, with the least recorded in 2017 (42 collisions) and the most recorded in 2015 (71 collisions). Furthermore, most of the collisions (29%) occurred during the autumn season (September, October, and November)



while the least number of collisions (23%) occurred during the spring season (March, April, and May), as depicted in **Figure 14**.

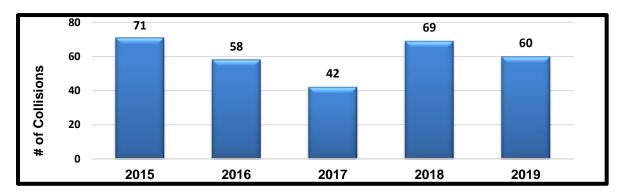


Figure 13: Total Number of Collisions Reported along Teston Road

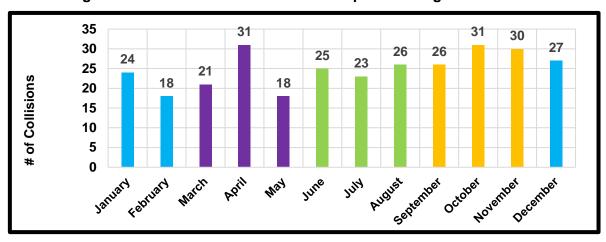


Figure 14: Total Number of Collisions along Teston Road by Month

No fatal collisions were reported during the 5-year analysis period with the majority classified as property damage only (71%). The remainder of the collisions were classified as non-fatal injury with 2 non-reportable as illustrated in **Figure 15**. None of the reported collisions involved pedestrians, although 3 collisions involved cyclists. A brief summary of the collisions involving the cyclists are included below in **Table 25**.

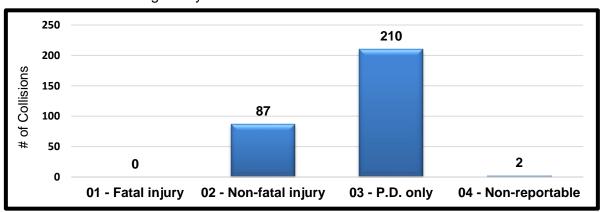


Figure 15: Number of Collisions on Teston Road based on Collision Type



Table 25: Summary of Collisions along Teston Road involving Cyclists

| Date | Location | Vehicle Type | Vehicle Maneuver | Classification of Collision | Environmental Condition | Surface Condition | Light Condition | Driver Condition / Action |
|------------------------|-------------------------------------|------------------|---------------------|-----------------------------|----------------------------|----------------------|--------------------|---|
| 10/15/2015 Thursday | Keele Street & Teston Road | Dump Truck | Turning left | Injury | Clear | Dry | Daylight | Normal / Improper passing |
| 6/7/2018 Thursday | Keele Street & Teston Road | Passenger Car | Turning right | PDO | Clear | Dry | Daylight | Normal / Driving properly |
| 9/20/2016 Tuesday | Teston Road & Exit 37 | Passenger Car | Turning right | Injury | Clear | Dry | Daylight | Normal / Failed to yield right- of-way |

The review of the collision history indicated majority of the collisions occurred at intersections (89%) while the remainder occurred mid-block between intersections or at residential driveways off Teston Road. One collision was recorded at the railway crossing on Teston Road east of Keele Street while another collision was unclassified (i.e. other).

The intersection that recorded the most collisions during the analysis period was at Bathurst Street and Elgin Mills Road West/Teston Road with 79 collisions. The mid-block segment which recorded the most collisions was along Teston Road between Torah Gate and Bathurst Street with 8 collisions.

A review of the collision impact type indicated that rear end collisions were the most common, representing 44% of all collisions. The subsequent most common impact types are turning (22%), sideswipe (13%), and angle (12%). **Figure 16** illustrates the proportion of each impact type relative to the collisions within the study area on Teston Road.

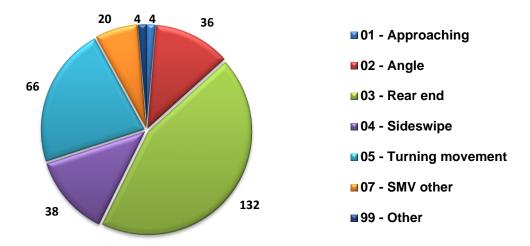


Figure 16: Number of Collisions on Teston Road based on Impact Type



Many of the collisions (82%) occurred when the road had clear weather conditions. Of the remaining collisions, the weather conditions included rain (13%), snow (4%), strong wind, fog / mist, and other. Additionally, the bulk of the collisions also occurred when the roadway surface was dry (73%). The remaining proportion of collisions occurred when there was some form of precipitation on the roadway surface such as rain, snow, or ice. The proportion of each weather condition is shown in **Figure 17** and the proportion of each surface condition is shown in **Figure 18**.

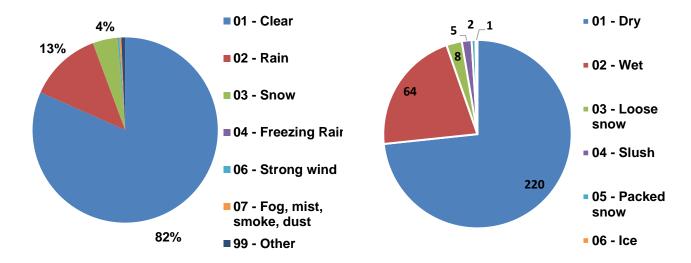


Figure 17: Number of Collisions on Teston Road based on Environmental Conditions

Figure 18: Number of Collisions on Teston Road based on Surface Condition

Furthermore, 70% of the collisions occurred during daylight conditions as shown in **Figure 19**. The remaining collisions either occurred during the night (21%), dawn (4%) or dusk (5%).

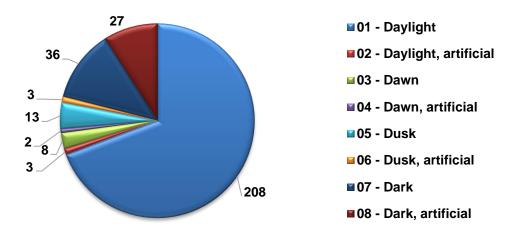


Figure 19: Number of Collisions on Teston Road based on Light Conditions



In assessing the condition of the drivers involved in the collision, most of the drivers were reported to be normal (63%) and uninhibited. Another 21% of the drivers were reported to be inattentive, suggesting they were not monitoring the roadway conditions prior to the collision. Three of the reported drivers should not have been driving as they were reported to have been drinking with one over the legal limit. Two other drivers were reported to be fatigued while the remaining drivers' condition were not reported or indicated as other. **Figure 20** illustrates the proportion of collisions by the primary driver's condition.

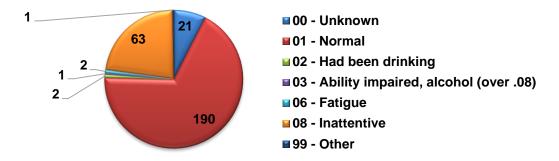


Figure 20: Number of Collisions on Teston Road based on Primary Driver Condition

The most prevalent primary event for the collisions reported was between two motor vehicles at 92%. Additionally, 81% of all collisions were the result of the primary drivers' actions. The leading cause of the collisions includes following too close to the vehicle ahead (27%), improper turn (14%), or failing to yield the right-of-way (13%). A distribution of each driver action resulting in the collision is shown in **Figure 21**. 9% of the reported collisions revealed the primary driver was driving appropriately, implying the collision was the result of the secondary vehicle / driver.

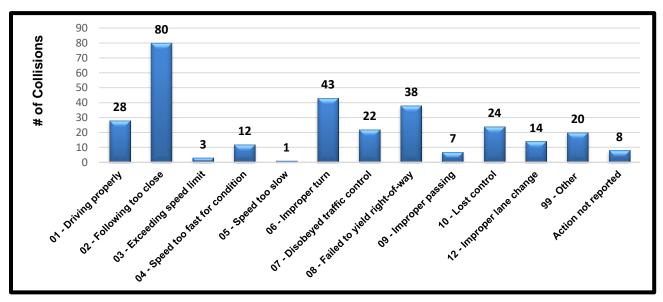


Figure 21: Number of Collisions on Teston Road based on Primary Driver Action



As shown in **Table 26**, the collision rates along Teston Road were calculated based on the number of collisions recorded per million vehicle kilometers (MVK). The collision rate equation is shown below:

Site Specific Collision Rate =
$$\frac{\text{No. of Collisions x } 10^6}{\text{AADT x Segment Length x No. of Years x 365 days/year}}$$

The AADT volume at Teston Road (from Highway 400 to Bathurst Street) was in the range of 2,222 vpd to 16,285 veh/day. Based on these volumes, the 66 midblock collisions along Teston Road would correlate to an average collision rate in the order of 0.55 to 2.47 collisions per Million Vehicle Kilometers (MVKM).

Collision Rate Number of collisions Segment **Location Description** AADT (vpd) Length (km) (2015-2019) (MVK) Hwy 400 to Jane St 1.0 5,309 (2019) 15 1.55 Jane St to Keele St 2.0 6,476 (2018) 13 0.55 2,222 (2019) Keele St to Rodinea Rd 0.5 5 2.47 Dufferin St to Bathurst St 2.0 16,285 (2018) 33 0.56

Table 26: Collision Rates along Teston Road

For the comparison of the collisions on each arterial road, York Region's collision rate is based on the number of collisions for each 100,000 population. Population statistics are not available along the study area arterial roadways, so comparisons for this metric cannot be made. However, collision rates based on million vehicle kilometers travelled have been provided.

3.11.2 Kirby Road (City of Vaughan)

Along the section of Kirby Road between Highway 400 to Dufferin Street, 73 collisions were reported between 2015 and 2019. Majority of the collisions were reported at or related to intersections as there was limited information provided for the mid-block segments along the corridor. No fatal collisions were reported in the corridor with most collisions resulting in property damage only (64%). Many of the collisions were between two motor vehicles (90%) with no collisions reported involving pedestrians or cyclists. The most common impact types included rear end and turning movements which accounted for approximately 36% each. 65% of all collisions also occurred when the conditions were dry and clear during the day. The midblock collision summary along Kirby Road is not available.

3.11.3 Major Mackenzie Drive (York Regional Road 25)

A review of the historical collision record for Major Mackenzie Drive between the limits of Highway 400 to Bathurst Street between 2015 and 2019



resulted in 1,066 individual entries. More than half of the collisions occurred during clear, daylight conditions when the roadway was dry. 75% of the collisions recorded were related to intersections along Major Mackenzie Drive. The most common impact type reported was rear-end collisions (48%) which related to 34% of drivers following too closely. The ensuing order for the impact type were turning movements (20%), sideswipes (13%) and angle (11%). Majority of the collisions (91%) involved passenger vehicles with 25 collisions involving pedestrians and 14 involving cyclists. A summary of all collisions involving pedestrians and cyclists are included in **Appendix E**. Most of the collisions reported were classified as either nonfatal (26%) or property damage only (73%) with two collisions classified as fatal. The fatal collisions are summarized in **Table 27** below.

Table 27: Summary of Fatal Collisions along Major Mackenzie Drive

| | Date | Location | Vehicle Maneuver | Vehicle Maneuver | Classification of Collision | Environmental Condition | Surface Condition | Light Condition | Driver Condition / Action ¹ |
|---|----------------------|--|--|-------------------------------------|-----------------------------|----------------------------|----------------------|---------------------|--|
| (| 09/10/2018 Monday | Major Mackenzie Drive West & Dufferin Street | Passenger Car (Passenger Car) | U-Turn (Going Ahead) | Fatal | Fog, Mist, Smoke, Dust | Wet | Dark, Artificial | Normal / Other (Normal / Driving Properly) |
| (| 08/10/2018 Friday | Major Mackenzie Drive West b/w Exit 35 & Jane Street | Motorcycle (Passenger Car) | Going Ahead (Turning Left) | Fatal | Clear | Dry | Dark | Normal / Exceeding Speed Limit (Normal / Driving Properly) |

¹ Details of the collision is reported for both vehicles: Vehicle 1 (Vehicle 2)

As shown in **Table 28**, the AADT volume at Major Mackenzie Drive (from Highway 400 to Bathurst Street) was in the range of 34,336 vpd to 63,533 veh/day. Based on these volumes, the 591 midblock collisions along Major Mackenzie Drive would correlate to an average collision rate in the order of 0.50 to 1.40 collisions per MVKM.

Table 28: Collision Rates along Major Mackenzie Drive

| Location Description | Segment Length (km) | AADT (vpd) | Number of collisions (2015-2019) | Collision Rate (MVK) |
|--------------------------------|------------------------|---------------|-------------------------------------|-------------------------|
| Hwy 400 to Jane St | 1.0 | 63,533 (2019) | 67 | 0.58 |
| Jane St to Keele St | 2.0 | 58,053 (2018) | 297 | 1.40 |
| Keele St to Dufferin Street | 2.1 | 34,336 (2019) | 163 | 1.24 |
| Dufferin St to Bathurst St | 2.0 | 35,176 (2018) | 64 | 0.50 |

3.11.4 Bathurst Street (York Regional Road 38)

Collision data for Bathurst Street between Kirby Road and Major Mackenzie Drive West obtained from the Regional Municipality of York reported 200



collisions between 2015 and 2019. The majority (75%) of the collisions reported occurred at intersections compared to other locations (e.g. midblock, driveway). The primary cause of collisions reported was the vehicles were following too close (23%) resulting in primarily rear end impacts (41%). No fatal collisions were reported with the majority resulting in property damage only (70%). Half of the collisions occurred when the environmental conditions were dry and clear during the day. Four collisions involved pedestrians and one included a cyclist (Refer to **Appendix E**).

As shown in **Table 29**, the AADT volume at Bathurst Street (between Kirby Road and Major Mackenzie Drive West) was in the range of 33,838 vpd to 38,877 veh/day. Based on these volumes, the 70 midblock collisions along Bathurst Street would correlate to an average collision rate in the order of 0.16 to 0.64 collisions per MVKM.

Table 29: Collision Rates along Bathurst Street

| Location Description | Segment Length (km) | AADT (vpd) | Number of collisions (2015-2019) | Collision Rate (MVK) |
|---|---------------------------|---------------|----------------------------------|----------------------------|
| Major Mackenzie Dr to Mill St/Queen Filomena Ave | 0.8 | 38,877 (2018) | 9 | 0.16 |
| Oxford St/Lady Dolores Ave and Elgin Mills Rd/Teston Rd | 0.3 | 34,478 (2019) | 12 | 0.64 |
| Teston Rd to Kirby Road | 2.0 | 33,838 (2018) | 49 | 0.40 |

3.11.5 Dufferin Street (York Regional Road 53)

Between 2015 and 2019, 78 collisions were reported along Dufferin Street between Kirby Road and Major Mackenzie Drive. Mid-block collisions accounted for approximately 60% of the total number of reported collisions. Majority of the collisions (74%) reported resulted in property damage only with only 1 reported as fatal. The details for the fatal collision are summarized in **Table 30** below. 41% of the collisions were reported during the day when the weather was clear, and the roadway surface was dry. The surface condition for most of the collisions was dry (77%). Most of the collisions involved passenger vehicles (88%) with one fatal collision involving a cyclist as described in **Table 30**. The most common impact type reported are rear-end collisions.



Right-of-Way)

Vehicle **Vehicle Driver** Classification **Environmental Surface** Light **Date** Location Maneuver Maneuve Condition Condition Condition Condition of Collision r 1 / Action 1 Normal / Dufferin Driving Street Properly Going btwn Sir Passenger (Impaired 08/01/2015 Ahead Benson Fatal Clear Dry Dark - Drugs / Car Saturday (Going Drive & (Cyclist) Failed to Ahead) Teston Yield

Table 30: Summary of Fatal Collisions along Dufferin Street

Road

As shown in **Table 31**, the AADT volume at Dufferin Street (between Kirby Road and Major Mackenzie Drive) was in the range of 12,051 vpd to 18,553 veh/day. Based on these volumes, the 48 midblock collisions along Dufferin Street would correlate to an average collision rate in the order of 0.13 to 0.62 collisions per MVKM.

Table 31: Collision Rates along Dufferin Street

| Location Description | Segment Length (km) | AADT (vpd) | Number of collisions (2015-2019) | Collision Rate (MVK) |
|---------------------------------|---------------------------|---------------|----------------------------------|----------------------------|
| Major Mackenzie Dr to Teston Rd | 2.0 | 18,553 (2018) | 42 | 0.62 |
| Hunterwood Chase to Beakes Cres | 0.6 | 14,430 (2019) | 2 | 0.13 |
| Athabasca Dr and Kirby Rd | 0.7 | 12,051 (2018) | 4 | 0.26 |

3.11.6 Keele Street (York Regional Road 6)

297 collisions were reported along Keele Street between Kirby Road and Major Mackenzie Drive between 2015 and 2019. Approximately 80% of the collisions occurred at the intersections within the limits. Most of the collisions (70%) resulted in property damage only while the remainder were non-fatal. No fatal collisions were reported. The most common impact type reported was rear end collisions accounting for 40% of all reported collisions. Many of the collisions involved another motor vehicle (86%), with six involving pedestrians and 5 involving cyclists (Refer to **Appendix E**). Additionally, 60% of the collisions occurred during clear daylight conditions when the road was dry.

As shown in **Table 32**, the AADT volume at Keele Street (between Kirby Road and Major Mackenzie Drive) was in the range of 15,234 vpd to 21,957 veh/day. Based on these volumes, the 57 midblock collisions along Keele Street would correlate to an average collision rate in the order of 0.42 to 0.85 collisions per MVKM.



¹ Details of the collision is reported for both vehicles: Vehicle 1 (Vehicle 2)

Table 32: Collision Rates along Keele Street

| Location Description | Segment Length (km) | AADT (vpd) | Number of collisions (2015-2019) | Collision Rate (MVK) |
|--|---------------------------|---------------|----------------------------------|----------------------------|
| Major Mackenzie Dr W and Railway St/Killian Rd | 0.2 | 21,957 (2019) | 4 | 0.50 |
| Maple Health Centre and Drummond Dr | 0.4 | 19,357 (2018) | 6 | 0.42 |
| Teston Rd to Kirby Rd | 2.0 | 15,234 (2019) | 47 | 0.85 |

3.11.7 Jane Street (York Regional Road 55)

Along the section of Jane Street between Kirby Road and Major Mackenzie Drive, 135 collisions were reported during a 5-year period between 2015 and 2019. 70% of the reported collisions were located at intersections along Jane Street. No fatalities were reported with most collisions resulting in property damage only (67%). Most of the collisions (57%) occurred when the conditions were dry and clear during the day. The most common impact types included rear end (31%), angle (19%), Single Motor Vehicle (19%), and turning movement (18%). Many of the collisions involved another motor vehicle (86%), with 14 involving pedestrians and 5 involving cyclists (Refer to **Appendix E**).

As shown in **Table 33**, the AADT volume at Jane Street (between Kirby Road and Major Mackenzie Drive) was in the range of 12,374 vpd to 36,093 veh/day. Based on these volumes, the 44 midblock collisions along Jane Street would correlate to an average collision rate in the order of 0.15 to 0.84 collisions per MVKM.

Table 33: Collision Rates along Jane Street

| Location Description | Segment Length (km) | AADT (vpd) | Number of collisions (2015-2019) | Collision Rate (MVK) |
|--|---------------------------|---------------|----------------------------------|----------------------------|
| Major Mackenzie Dr and Roseheath Dr/Grand Valley Blvd | 0.45 | 36,093 (2019) | 12 | 0.40 |
| Ahmadiyya Ave and Teston Rd | 0.3 | 12,374 (2018) | 1 | 0.15 |
| Teston Rd and Kirby Rd | 2.0 | 6,837 (2019) | 21 | 0.84 |



4. FUTURE CONDITIONS

4.1 City of Vaughan Active (Proposed) Land Use Developments

The City of Vaughan maintains a geospatial database, referred to as PLANit, which identifies current active development proposals within the City's jurisdiction. The PLANit database includes planned subdivisions, zoning by-law changes, official plan amendments, site plan and condominium applications. A summary of active proposals, in addition to other planned developments, which may contribute to increased traffic within the study area are discussed below.

4.1.1 North Maple Regional Park

The North Maple Regional Park (NMRP) sits south of Kirby Road between Keele Street and Dufferin Street on the former Avondale Compost lands. It is currently roughly 81 hectares of parklands with walking trails, soccer fields as well as washrooms and other amenities. Phase 1 of the park (81 hectares) was opened in 2019.

The City of Vaughan has plans to increase the size of the park through a phased planning approach. The expected final size of the park will be roughly 365 hectares and will cover the land of the former Vaughan Landfill and the former Keele Valley Landfill. The plan also includes integration with a Teston Road missing link between Keele Street and Dufferin Street.

The NMRP will include a portion of the proposed Vaughan Super Trail which will create a 100km city-wide trail system.

4.1.2 Maple Go Station Improvements

Maple GO Station is a train and bus station on GO Transit's Barrie line, located in Maple, Ontario. Metrolinx has been committed to improving the Maple GO Station while maintaining the heritage aspects of the station. Since 2012, improvements at Maple GO Station have included the expansion of the existing parking facilities, a pedestrian walkway from Eagle Rock Way, and two pedestrian tunnels. The future improvements planned specifically at this station include a new second track and platform for increased service, further expansion of the current parking facilities, an upgraded bus loop and a PPUDO area. Furthermore, future plans for the area separate from the improvements at the station include grade separating the existing rail crossing at McNaughton Road to improve traffic and safety at the junction.

4.1.3 Cortelluci Vaughan Hospital

The Cortelluci Vaughan Hospital, slated to open in 2020, will be the first smart hospital in Canada, expanding the health care services and capacity to the surrounding communities. The construction of the 1.2 million square foot facility hospital, costing \$1.6 billion, located in the northwest corner of Jane



Street and Major Mackenzie Drive, will include a wealth of facilities including a 37,000 square foot state of the art emergency department, 12,000 square foot pharmacy, 350 beds with capacity to expand to 550 beds, specialized ambulatory clinics and 21 critical care beds. The location of the hospital near Highway 400 and nearby Highway 407 and Highway 401 provides convenient access for the greater community.

4.1.4 Block 27

Block 27 is a proposed plan to redevelop approximately 400 hectares of mainly undeveloped land on the north side of Teston Road between Jane Street and Keele Street up to Kirby Road. The area includes part of the West Don River, Greenbelt and an east-west section of the TransCanada Pipeline. In 2018, the City of Vaughan approved a secondary plan for the area to guide the development of the lands to focus on transit-oriented development which supports a compact, vibrant, and inclusive community. The proposed community is planned to include a mix of commercial, residential and community facilities with a potential GO station along the existing railway corridor in the northeast quadrant of the lands near the intersection of Kirby Road and Keele Street.

4.1.5 Part of Lot 28, Concession 5

A proposed warehouse and distribution development centre have been proposed along Janes Street midway between Teston Road and Kirby Road. The development is planned within the Highway 400 North Employment Area and will have a total gross floor area of 70,308 m2 when the site is fully developed.

The Highway 400 North Employment area is a largely undeveloped section of land on both sides of the regional Highway 400 corridor area surrounding the Highway 400 corridor between Teston Road and King Vaughan Road. The portion overlapping the IEA study area bounded by Highway 400, Teston Road, Jane Street and Kirby Road has been approved by the City of Vaughan to support a mix of prestige, general employment and mixed-use developments.

4.1.6 11333 Dufferin Street

Located in the south-east quadrant of Dufferin Street and Kirby Road, the proposed development is comprised of a residential subdivision consisting of 526 lots for detached dwellings, a park, stormwater management, natural areas and municipal roads. The site is currently zoned as Future Urban Area Zone, as such there is a zoning amendment application in progress to change the zoning to allow for single family detached dwellings, park lands and open space.



4.1.7 981 Teston Road

Located along Teston Road midway between Bathurst Street and Dufferin Street, the proposed development is comprised of a residential subdivision consisting of 49 single detached dwellings, natural area, stormwater management, and municipal roads. The site is currently zoned Agricultural Zone, as such a zoning amendment will be required.

4.1.8 1600 Teston Road

A planning application has been submitted to construct a new subdivision at 1600 Teston Road. The planned subdivision located on the north side of Teston Road, west of the intersection with Dufferin Street, is planned to include 96 low-rise residential subdivision properties. The new subdivision will access Teston Road via the existing unopened road allowance west of Teston Road between Keele Street and Dufferin Street.

4.1.9 2975, 2985 and 2993 Teston Road

An application for an 11-story residential apartment complex has been submitted in the southeast corner of Jane Street and Teston Road. The proposed development shall include 176 residential units and 205 parking spaces, with a full movement driveway access to Teston Road and a right-in right-out access at Jane Street.

4.1.10 Developments on Rodinea Road

Planning applications have been submitted for three properties along Rodinea Road. These applications include construction of two new two-story accessory office spaces and an addition to an existing building. The two new proposed office spaces are at 200 and 290 Rodinea Road with a total gross floor area of 1236m2 and 1257m2, respectively. The proposed addition at 311 Rodinea Road is a 346m2 addition to the existing industrial building.

4.2 Future Road Network

4.2.1 The City of Vaughan and York Region's Road Improvements

Figure 22 illustrates the proposed road network in York Region's 2016 TMP for the year 2041.



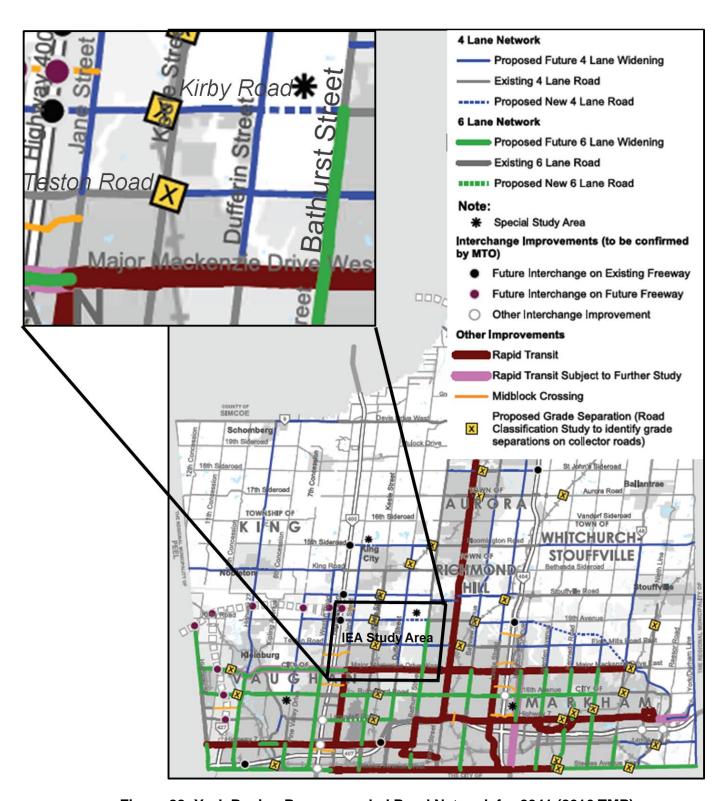


Figure 22: York Region Recommended Road Network for 2041 (2016 TMP)



The City of Vaughan and York Region have both identified the following planned improvements and additions to the transportation system:

4.2.1.1 Teston Road (York Region Road 49)

York Region's TMP includes widening of the existing Teston Road to four lanes between Pine Valley Drive and Weston Road and from Dufferin Street to Yonge Street. In addition, it is recommended to extend Teston Road between Keele Street and Dufferin Street as a four-lane roadway to accommodate additional traffic from anticipated developments.

4.2.1.2 Kirby Road (City of Vaughan)

York Region's TMP includes widening of Kirby Road between Pine Valley Drive and Dufferin Street from two to four lanes and the extension of Kirby Road between Dufferin Street and Bathurst Street as a four-lane roadway including a potential Kirby Road interchange with Highway 400.

4.2.1.3 Major Mackenzie Drive (York Regional Road 25)

The York Region's TMP includes the widening of Major Mackenzie Drive between Highway 50 and Jane Street from four to six lanes. Based on the York Region's TMP, there will be a dedicated transit rapidway on Major Mackenzie Drive (occurring 2027-2031).

4.2.1.4 Bathurst Street (York Regional Road 38)

The York Region's TMP includes widening of Bathurst Street between Highway 7 and Kirby Road from four to six lanes.

4.2.1.5 Dufferin Street (York Regional Road 53)

The York Region's TMP includes widening of Dufferin Street between Major Mackenzie Drive and 15th Sideroad (Y.R. 40), located north of Kirby Road, from two to four lanes.

4.2.1.6 Keele Street (York Regional Road 6)

There are no identified recommended improvements along Keele Street in the York Region TMP.

4.2.1.7 Jane Street (York Regional Road 55)

York Region's TMP includes widening of Jane Street between Teston Road and 15th Sideroad (Y.R. 40) from two to four lanes.



4.2.2 Other Road Improvements

4.2.2.1 Highway 400

Currently there is ongoing construction on Highway 400 (between Major Mackenzie Drive north to King Road) to widen Highway 400 from six to eight lanes.

4.2.2.2 Canada Drive-America Avenue Bridge

The City of Vaughan's Official Plan identifies the need to establish a primary road connection over Highway 400 between Major Mackenzie Drive and Teston Road in Block 33. This road connection is not only a key component of the area multi-modal transportation system (accommodating vehicles, cyclists and pedestrians) but also a means of providing the residents in the communities on either side of Highway 400 with better access to community services, reduced travel times and improved emergency response services. Subsequently, the location of the mid-block connection between Canada Drive and America Avenue was identified through the development planning process for Block 33. The preferred design includes a 2-lane roadway, sidewalks and bicycle lanes on a mostly straight alignment slightly shifted to the south side of the right of way and intersections at Cityview Boulevard/Canada Drive (requiring re-grading) and John Deisman Boulevard/ America Avenue.

4.2.2.3 GTA West Highway Corridor

MTO is in the process of confirming the Preferred Route for a new 400-series highway and transit corridor across York, Peel and Halton regions to make commuting and travel easier in the Greater Toronto Area.

The GTA West corridor will include a four-to-six lane 400-series highway, separate infrastructure dedicated for transit and passenger stations, as well as intelligent transportation features and truck parking. The EA for the GTA West Corridor is expected to be complete by the end of 2022. **Figure 23** illustrates the GTA West route planning study area.



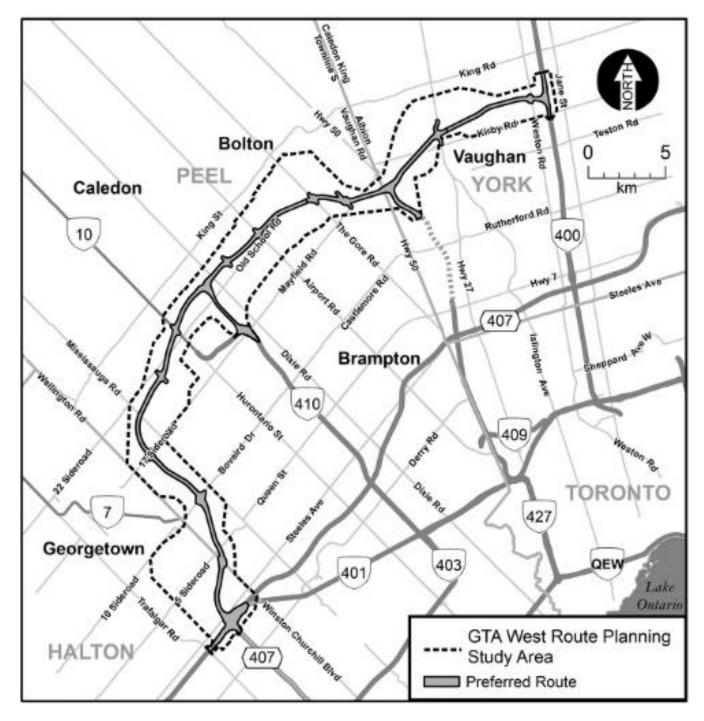


Figure 23: GTA West Route Planning Study Area

4.2.2.4 Highway 427 Expansion and Extension

The MTO and Infrastructure Ontario (IO) have signed a \$616 million fixed-price contract for the Link 427 consortium to design, build, finance and maintain the expansion project.



The expansion project includes an extension of the highway corridor by 6.6 km from Highway 7 to Major Mackenzie Drive, widening of the existing highway to 8 lanes between Finch Avenue and Highway 7, and new interchanges at Langstaff Road, Rutherford Road and Major Mackenzie Drive. The extension project will include 8 lanes between Highway 7 and Rutherford Drive and 6 lanes from Rutherford to Major Mackenzie Drive. The project which began in August 2017 is expected to be completed in 2021, with Link 427 providing ongoing highway maintenance for the next 30 years. Refer to **Figure 24** illustrating the improvements for Highway 427.

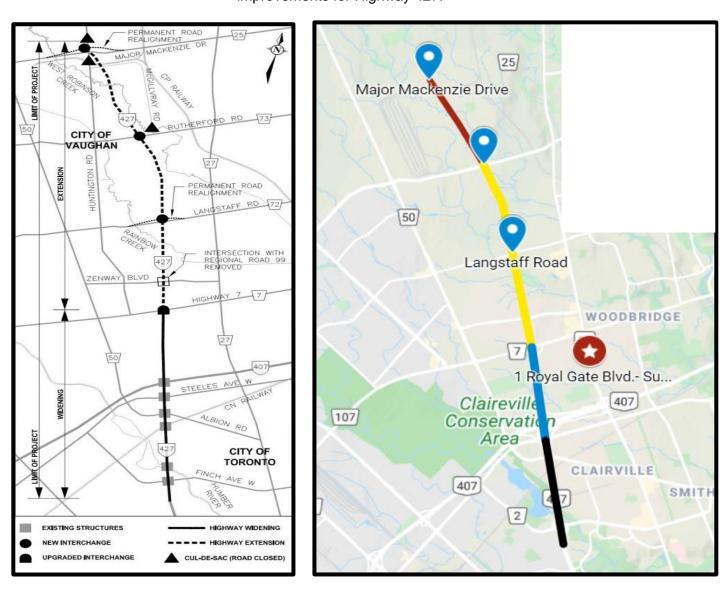


Figure 24: Highway 427 Expansion and Extension



5. MODEL REVIEW

York Region provided Travel Demand Forecasting Subarea Models (EMME) for years 2016, 2031 and 2041 (with and without GTA West) during the AM peak hour of a typical day. As mentioned in **Section 1.2**, the limits of the subarea models were extended to include Yonge Street, Pine Valley Drive, King Vaughan Road and Rutherford Road (Refer to **Figure 1**).

5.1 2016 Subarea EMME Model

The Region's current 2016 EMME model was calibrated at the Regional screenline level using data from the 2011 TTS. However, the calibrated Region's model is not sufficient for any subarea studies. Therefore, the 2016 subarea model was calibrated based on the provided traffic counts.

5.1.1 Calibrating 2016 EMME Subarea Model

Calibration is a process of comparing the model to the field data to test the accuracy of simulated data. The measures of effectiveness (MOE) that were used for the purpose of calibration comparisons between the simulated runs and the existing conditions included hourly traffic volumes for all arterial roads within the study area. The model was considered calibrated when hourly traffic volumes satisfied the criteria provided in **Table 34**.

Table 34: EMME Model Calibration Criteria

| Criteria | Measure | Greater Than | Less Than | Calibration Target |
|----------|-------------|--------------|------------|-----------------------|
| | | - | 700 veh/h | Within 100 veh/h |
| | Hourly Link | 700 veh/h | 2700 veh/h | Within 15% |
| Traffic | Volumes | 2700 veh/h | - | Within 400 veh/h |
| Volumes | | GEH Stat | tistic | Less Than 5.00 |
| | Total Link | - | | Within 5% |
| | Volumes | GEH Stat | tistic | Less Than 4.00 |

The GEH Statistic is a formula used in traffic modelling to compare two sets of traffic volumes. The formula for the "GEH Statistic" is:

$$GEH = \sqrt{\frac{2(M-C)^2}{M+C}}$$

Where M is the hourly traffic volume from the traffic model and C is the real-world hourly traffic count.

Table 35: 2016 AM Peak Hour Traffic Volume Calibration

| | Arterial Road | Segment | Bidirectional Model Volume | Bidirectional Observed Volume | Difference (%) | | GEH Statistic |
|----------|---------------------|--------------------|----------------------------------|-------------------------------------|-------------------|------|------------------|
| | Kirby Dd | Hwy 400 to Jane St | 363 | 347 | 5% | 16 | 0.85 |
| Kirby Rd | Jane St to Keele St | 601 | 576 | 4% | 25 | 1.03 | |



| Teston Rd | Hwy 400 to Jane St Jane St to Keele St Dufferin St to Bathurst St | 2,189 1,849 908 | 2,390 1,765 838 | -8% 5% 8% | -201 84 70 | 4.20 1.98 2.37 |
|-----------------------|--|----------------------------------|----------------------------------|---------------------------|------------------------------------|------------------------------|
| Major Mackenzie Dr | Hwy 400 to Jane St Jane St to Keele St Keele St to Dufferin St Dufferin St to Bathurst St | 3,265 2,940 2,390 2,686 | 3,831 3,294 2,616 2,699 | -15% -11% -9% 0% | -566 -354 -226 -13 | 9.50 6.34 4.52 0.25 |
| | Rutherford Rd to Major Mackenzie Dr | 2,804 | 2,902 | -3% | -98 | 1.83 |
| Bathurst St | Major Mackenzie Dr to Mill St/Queen Filomena Ave | 2,874 | 3,237 | -11% | -363 | 6.57 |
| | Oxford St/Lady Dolores Ave to Teston Rd | 2,648 | 2,747 | -4% | -99 | 1.91 |
| | Teston Rd to Kirby Rd Kirby Rd to King Vaughan Rd | 2,873 2,569 | 2,843 2,298 | 1% 12% | 30 271 | 0.56 5.49 |
| | Rutherford Rd to Major Mackenzie Dr | 2,247 | 2,330 | -4% | -83 | 1.74 |
| Dufferin St | Major Mackenzie Dr to Teston Rd | 1,351 | 1,517 | -11% | -166 | 4.38 |
| | Teston Rd to Kirby Rd Kirby Rd to King Vaughan Rd | 1,312 987 | 1,344 1,000 | -2% -1% | -32 -13 | 0.88 0.41 |
| | Dina Rd to Cromwell Rd/Fieldgate Dr | 2,137 | 1,883 | 13% | 254 | 5.67 |
| | Naylon St to Church St. Mid- Block Pedestrian Crossing | 2,138 | 2,197 | -3% | -59 | 1.27 |
| Keele St | Major Mackenzie Dr to Railway St/Killian Rd | 1,998 | 1,970 | 1% | 28 | 0.63 |
| | Maple Health Centre to Drummond Dr | 1,630 | 1,715 | -5% | -85 | 2.08 |
| | Teston Rd to Kirby Rd Kirby Rd to King Vaughan Rd | 1,734 1,691 | 1,858 1,712 | -7% -1% | -124 -21 | 2.93 0.51 |
| | Rutherford Rd to Auto Vaughan Dr | 2,507 | 2,195 | 14% | 312 | 6.43 |
| | Avro Rd to Major Mackenzie Dr Major Mackenzie Dr to | 2,225 | 2,207 | 1% | 18 | 0.38 |
| Jane St | Roseheath Dr/Grand Valley | 2,593 | 2,587 | 00/ | | 0.40 |
| | Blvd Ahmadiyya Ave to Teston Rd | 1,171 | 1,199 | 0% -2% | 6 -28 | 0.12 0.81 |
| | Teston Rd to Kirby Rd Kirby Rd to King Vaughan Rd | 1,162 1,030 | 1,053 1,010 | 10% 2% | 109 20 | 3.28 0.63 |
| | Total | 58,842 | 60,160 | -2% | -1,318 | 5.40 |
| | | | | | | |

As shown above, the hourly traffic volumes reported from the model correspond strongly with the observed volumes. As a result of the analysis provided, the EMME model is considered to be accurately calibrated to the observed hourly traffic volumes along all arterial roads, representing the 2016 year within the study area. The results of the calibration indicate that the 2016 model is appropriate to use as a basis for developing future traffic volume projections.



5.1.2 2016 Link Analysis

The existing roadways in the study area range from multi-lane arterial roadways (e.g. Major Mackenzie Drive) to single lane facilities (e.g. Gamble Road). Each facility has a finite capacity - the number of vehicles that can be serviced in a lane in a given hour.

Based on York Region Travel Demand Forecasting Model Update Report (2014), lane capacities in the EMME models were reviewed and adjustments were made based on a set of rules, including road classifications, posted speed limit, number of signalized intersections and geometric aspects (Refer to **Table 36**). MH has reviewed and confirmed the lane capacity in the model based on available turning movement counts.

Table 36: Lane Capacities in the EMME Models

| Road Classification | Posted Speed (km/hr) | Capacity (Veh/Ln/hr) |
|---------------------|-------------------------|----------------------|
| Centroid Connectors | 40 | 9999 |
| Local Roads | 40 | 400 - 500 |
| Local Roads | 50 | 700 - 800 |
| Arterial Roads | 60 | 700 - 1000 |
| Arterial Roads | 70 | 900 - 1200 |
| Arterial Roads | 80 | 1000 |
| Highway 400 | 110 | 1800 |
| Highway 400 Ramps | 50 - 70 | 1400 |

The 2016 traffic volumes reported from the model during the morning peak hour are then applied to this capacity of the roadway and the quality of performance is determined. Roadway performance is typically expressed in terms of the Volume to Capacity (V/C) ratio, whereby a V/C ratio that exceeds 0.90 is typically considered "congested condition" and improvements are generally warranted (see **Table 37**).

Table 37: Link Volume to Capacity Ratio and Operating Condition for Arterial Roads

| Volume to Capacity Ratio | LOS | Operating Condition |
|--------------------------|-----|---------------------------------|
| Less than 0.60 | Α | Free-flow Conditions |
| 0.61 to 0.70 | В | Reasonably Unimpeded Operations |
| 0.71 to 0.80 | С | Stable Operations |
| 0.81 to 0.90 | D | Approaching Unstable Operations |



| Volume to Capacity Ratio | LOS | Operating Condition |
|--------------------------|-----|---------------------------|
| 0.91 to 1.00 | Е | Congested Conditions |
| Greater Than 1.00 | F | Very Congested Conditions |

Figure 25 illustrates the 2016 V/C ratios for each key roadway. The figure indicates that numerous locations exhibit over-capacity conditions.

The analysis results indicate that under 2016 AM conditions Kirby Road, Teston Road and Major Mackenzie Drive are operating at free flow conditions in the eastbound direction, while congested conditions exist in the westbound direction due to the predominant westbound traffic during the morning peak hour.

All north-south arterial roads are operating at free flow conditions in the northbound direction, while the majority of southbound movements experience very congested conditions particularly south of Teston Road due to the predominant southbound traffic during the morning peak hour.

A similar reversed traffic pattern is expected during the afternoon peak hour, with predominantly eastbound and northbound directions of traffic flow.

A snapshot of the 2016 EMME subarea network is included in **Appendix F**.



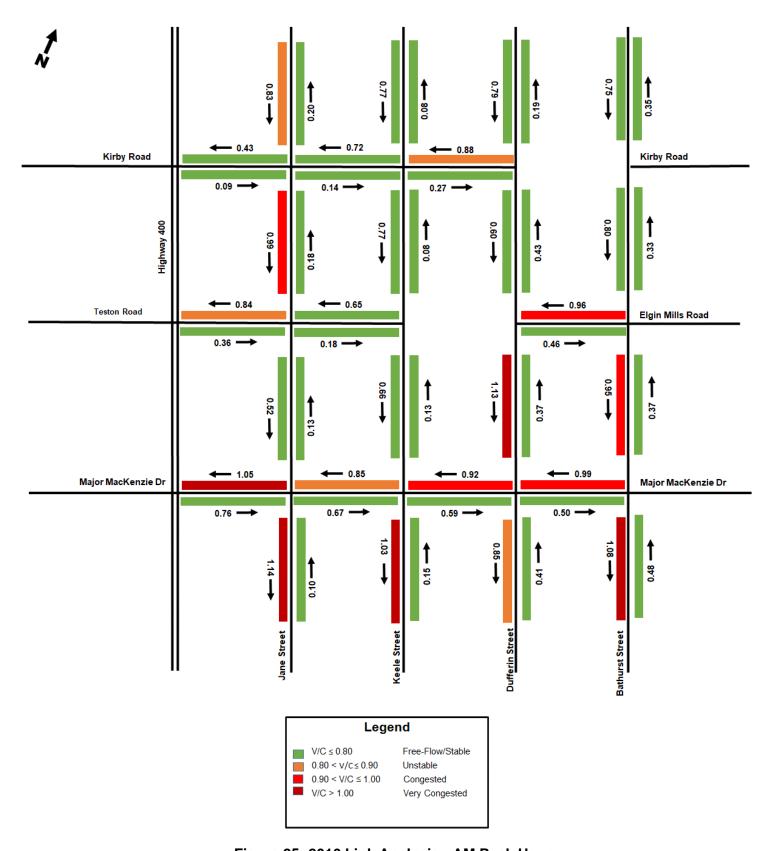


Figure 25: 2016 Link Analysis - AM Peak Hour



5.1.3 2016 Screenline Analysis

The travel demands were developed at strategic screenlines or an imaginary boundary which extends across a series of roadways and typically located where travel constraints exist such as rivers, rail corridors, and greenspaces. The 2016 peak direction (westbound and southbound) travel demands at five screenlines were then compared with the available capacity and the travel deficiency or surplus was derived. **Figure 26** illustrates the location of these five screenlines.

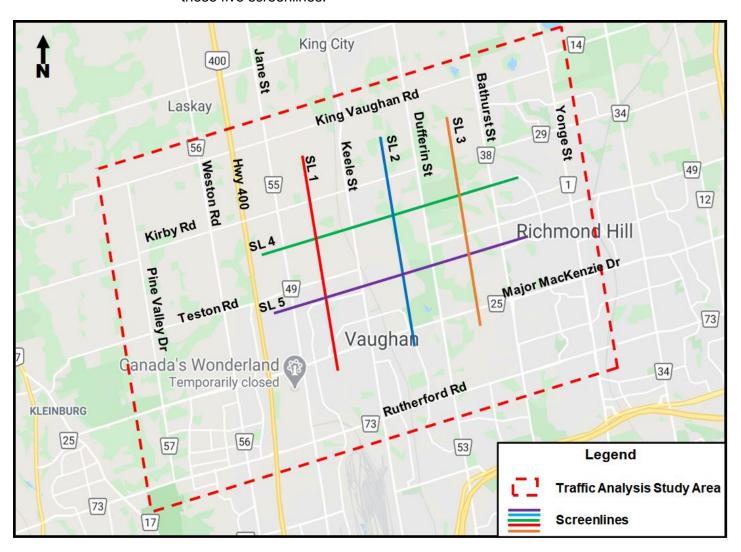


Figure 26: Study Area Screenlines

Table 38 summarizes 2016 AM peak hour volumes and the V/C ratio for each key roadway at the five screenlines in the study area. **Table 38** indicates that the overall V/C for Screenlines SL2 and SL3 exhibit values of 0.91 and 0.98, respectively, suggesting that the demand exceeds the available capacity. It is evident that without the Kirby Road and Teston Road connections Major Mackenzie Drive experiences delay and congestion.



Table 38: AM Peak Hour / Peak Direction Assigned Volumes and V/C (2016 EMME Model)

| Section | Volume | # Lanes (Per Direction) | Lane Capacity (Per Direction) | Total Capacity (Per Direction) | V/C |
|--------------------|--------|----------------------------|----------------------------------|--------------------------------|------|
| | | Screenlin | | | |
| Major Mackenzie Dr | 1,362 | 2 | 800 | 1,600 | 0.85 |
| Teston Rd | 1,175 | 2 | 900 | 1,800 | 0.65 |
| Kirby Rd | 504 | 1 | 700 | 700 | 0.72 |
| Screenline Total | 3,041 | 5 | | 4,100 | 0.74 |
| | | Screenlin | e 2 | | |
| Major Mackenzie Dr | 1,651 | 2 | 900 | 1,800 | 0.92 |
| Kirby Rd | 619 | 1 | 700 | 700 | 0.88 |
| Screenline Total | 2,270 | 3 | | 2,500 | 0.91 |
| | | Screenlin | e 3 | | |
| Major Mackenzie Dr | 1,780 | 2 | 900 | 1,800 | 0.99 |
| Teston Rd | 768 | 1 | 800 | 800 | 0.96 |
| Screenline Total | 2,548 | 3 | | 2600 | 0.98 |
| | | Screenlin | e 4 | | |
| Jane St | 986 | 1 | 1000 | 1000 | 0.99 |
| Keele St | 1,548 | 2 | 1000 | 2000 | 0.77 |
| Dufferin St | 598 | 1 | 1000 | 1000 | 0.60 |
| Bathurst St | 1,931 | 2 | 1200 | 2400 | 0.80 |
| Screenline Total | 5,063 | 6 | | 6,400 | 0.79 |
| | | Screenlin | e 5 | | |
| Jane St | 939 | 2 | 900 | 1800 | 0.52 |
| Keele St | 1,051 | 2 | 800 | 1600 | 0.66 |
| Dufferin St | 1,018 | 1 | 900 | 900 | 1.13 |
| Bathurst St | 1,903 | 2 | 1000 | 2000 | 0.95 |
| Screenline Total | 4,911 | 7 | | 6,300 | 0.78 |

The corresponding 2016 projected am peak hour transit demand (i.e. transit person trips) at each screenline developed in the EMME model is summarized in **Table 39**.

The 3-hour transit trips (between 6:00 a.m. and 8:59 a.m.) were factored by 2.0 to establish average am peak hour transit passenger trips. This factor was estimated based on the assumption that 50% of the a.m. peak period of transit demand takes place during the a.m. peak hour.

In general terms, transit trips are higher at the eastern and southern limits of the study area where the various transit facilities converge.



Table 39: AM Peak Hour / Peak Direction Transit Person Trips (2016 EMME Model)

| Section | 1-hour Auto trips | 1-hour Passenger Car Equivalent ¹ | 3-hour Transit Passenger Trips | 1-hour Transit Passenger Trips | 1-hour Total Passenger Trips | Transit Mode Share | | | |
|--------------------|-------------------------|--|---|---|------------------------------------|--------------------------|--|--|--|
| | Screenline 1 | | | | | | | | |
| Major Mackenzie Dr | 1,362 | 1,580 | 130 | 65 | 1,645 | 4% | | | |
| Teston Rd | 1,175 | 1,363 | 0 | 0 | 1,363 | 0% | | | |
| Kirby Rd | 504 | 585 | 0 | 0 | 585 | 0% | | | |
| Screenline Total | 3,041 | 3,528 | 130 | 65 | 3,593 | 2% | | | |
| | | Scre | enline 2 (WB) | | | | | | |
| Major Mackenzie Dr | 1,651 | 1,915 | 169 | 85 | 2,000 | 4% | | | |
| Kirby Rd | 619 | 718 | 0 | 0 | 718 | 0% | | | |
| Screenline Total | 2,270 | 2,633 | 169 | 85 | 2,718 | 3% | | | |
| | | Scre | enline 3 (WB) | | | | | | |
| Major Mackenzie Dr | 1,780 | 2,065 | 183 | 92 | 2,156 | 4% | | | |
| Teston Rd | 768 | 891 | 0 | 0 | 891 | 0% | | | |
| Screenline Total | 2,548 | 2,956 | 183 | 92 | 3,047 | 3% | | | |
| | , | Scre | eenline 4 (SB) | | , | | | | |
| Jane St | 986 | 1,144 | 1 | 1 | 1,144 | 0% | | | |
| Keele St | 1,548 | 1,796 | 59 | 30 | 1,825 | 2% | | | |
| Dufferin St | 598 | 694 | 0 | 0 | 694 | 0% | | | |
| Bathurst St | 1,931 | 2,240 | 455 | 228 | 2,467 | 9% | | | |
| Screenline Total | 5,063 | 5,873 | 515 | 258 | 6,131 | 4% | | | |
| | | Scre | eenline 5 (SB) | | | | | | |
| Jane St | 939 | 1,089 | 0 | 0 | 1,089 | 0% | | | |
| Keele St | 1,051 | 1,219 | 49 | 25 | 1,244 | 2% | | | |
| Dufferin St | 1,018 | 1,181 | 0 | 0 | 1,181 | 0% | | | |
| Bathurst St | 1,903 | 2,207 | 372 | 186 | 2,393 | 8% | | | |
| Screenline Total | 4,911 | 5,697 | 421 | 211 | 5,907 | 4% | | | |

Note: Based on 2011 TTS, the passenger-car equivalent is 1.16. persons/car

5.2 2031 Subarea EMME Model

The Region's 2031 EMME model includes all planned/proposed network improvements identified in the York Region's 2020 10-year Capital Program:

- Dufferin Street widened between Major Mackenzie Drive and Teston Road from two to four lanes:
- Bathurst Street widened between Highway 7 and Major Mackenzie Drive from four to six lanes;
- Major Mackenzie Drive widened between Highway 50 and Jane Street from four to six lanes.
- Teston Road widened between Pine Valley Drive and Weston Road from two to four lanes;
- Teston Road widened between Bathurst Street and Yonge Street from two to four lanes; and



 Highway 400 widened between Major Mackenzie Drive to King Road from six to eight lanes.

The GTA West freeway, Kirby Road and Teston Road extensions are not part of the roadway network in this horizon year.

Figure 27 illustrates the 2031 V/C ratios for each key roadway. The figure indicates that virtually all westbound and southbound movements along arterial roads are functioning with a V/C ratio that exceeds 0.90 suggesting that the demand well exceeds the proposed capacity. A snapshot of the 2031 EMME subarea network is included in **Appendix G**.

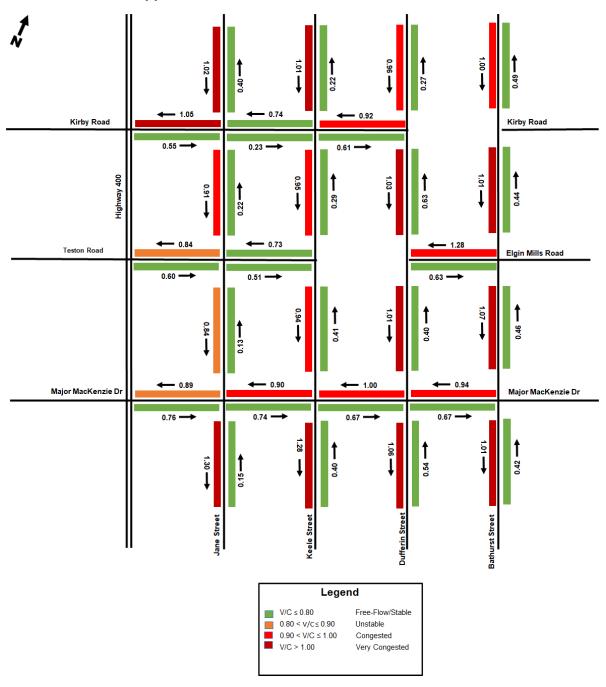


Figure 27: 2031 Link Analysis - AM Peak Hour



Table 40 illustrates the V/C ratio for each key roadway at the five screenlines in the study area for the year 2031. **Table 40** indicates that virtually all major arterial roads crossing Screenlines SL2, SL3, SL4 and SL5 are functioning with a V/C ratio that exceeds 0.90 (i.e. volume exceeds capacity).

Table 40: AM Peak Hour / Peak Direction Assigned Volumes and V/C (2031 EMME Model)

| Section | Volume | # Lanes (Per Direction) | Lane Capacity (Per Direction) | Total Capacity (Per Direction) | V/C |
|--------------------|--------|----------------------------|-------------------------------|--------------------------------|------|
| | | Screenline | | | |
| Major Mackenzie Dr | 1,439 | 2 | 800 | 1,600 | 0.90 |
| Teston Rd | 1,321 | 2 | 900 | 1,800 | 0.73 |
| Kirby Rd | 521 | 1 | 700 | 700 | 0.74 |
| Screenline Total | 3,281 | 5 | | 4,100 | 0.80 |
| | | Screenline | e 2 | | |
| Major Mackenzie Dr | 1,801 | 2 | 900 | 1,800 | 1.00 |
| Kirby Rd | 646 | 1 | 700 | 700 | 0.92 |
| Screenline Total | 2,447 | 3 | | 2,500 | 0.98 |
| | | Screenline | e 3 | | |
| Major Mackenzie Dr | 1,699 | 2 | 900 | 1,800 | 0.94 |
| Teston Rd | 1,026 | 1 | 800 | 800 | 1.28 |
| Screenline Total | 2,725 | 3 | | 2,600 | 1.05 |
| | | Screenline | | | |
| Jane St | 912 | 1 | 1000 | 1,000 | 0.91 |
| Keele St | 1,710 | 2 | 900 | 1,800 | 0.95 |
| Dufferin St | 1,032 | 1 | 1000 | 1,000 | 1.03 |
| Bathurst St | 2,422 | 2 | 1200 | 2,400 | 1.01 |
| Screenline Total | 6,076 | 6 | | 6,200 | 0.98 |
| | | Screenline | | | |
| Jane St | 1,507 | 2 | 900 | 1,800 | 0.84 |
| Keele St | 1,510 | 2 | 800 | 1,600 | 0.94 |
| Dufferin St | 1,816 | 2 | 900 | 1,800 | 1.01 |
| Bathurst St | 2,142 | 2 | 1000 | 2,000 | 1.07 |
| Screenline Total | 6,975 | 8 | | 7,200 | 0.97 |

The corresponding 2031 projected am peak hour transit demand (i.e. transit person trips) at each screenline developed in the EMME model is summarized in **Table 41**.

It is evident that by 2031 the transit trips are expected to increase significantly along Major Mackenzie Drive, Jane Street and Keele Street.



Table 41: AM Peak Hour / Peak Direction Transit Person Trips (2031 EMME Model)

| Section | 1-hour Auto trips | 1-hour Passenger Car Equivalent ¹ | 3-hour Transit Passenger Trips | 1-hour Transit Passenger Trips | 1-hour Total Passenger Trips | Transit Mode Share |
|--------------------|-------------------------|---|---|---|------------------------------------|--------------------------|
| | | | creenline 1 | TTIPS | | |
| Major Mackenzie Dr | 1,439 | 1,669 | 1,073 | 537 | 2,206 | 24% |
| Teston Rd | 1,321 | 1,532 | 42 | 21 | 1,553 | 1% |
| Kirby Rd | 521 | 604 | 19 | 10 | 614 | 2% |
| Screenline Total | 3,281 | 3,806 | 1,134 | 567 | 4,373 | 13% |
| | | Scre | eenline 2 (WB) | | | |
| Major Mackenzie Dr | 1,801 | 2,089 | 966 | 483 | 2,572 | 19% |
| Kirby Rd | 646 | 749 | 0 | 0 | 749 | 0% |
| Screenline Total | 2,447 | 2,839 | 966 | 483 | 3,322 | 15% |
| | | Scre | enline 3 (WB) | | | |
| Major Mackenzie Dr | 1,699 | 1,971 | 870 | 435 | 2,406 | 18% |
| Teston Rd | 1,026 | 1,190 | 0 | 0 | 1,190 | 0% |
| Screenline Total | 2725 | 3,161 | 870 | 435 | 3,596 | 12% |
| | | Scr | eenline 4 (SB) | | , | |
| Jane St | 912 | 1,058 | 85 | 43 | 1,100 | 4% |
| Keele St | 1,710 | 1,984 | 492 | 246 | 2,230 | 11% |
| Dufferin St | 1,032 | 1,197 | 22 | 11 | 1,208 | 1% |
| Bathurst St | 2,422 | 2,810 | 668 | 334 | 3,144 | 11% |
| Screenline Total | 6,076 | 7,048 | 1,267 | 634 | 7,682 | 8% |
| | | Scr | eenline 5 (SB) | | | |
| Jane St | 1,507 | 1,748 | 35 | 18 | 1,766 | 1% |
| Keele St | 1,510 | 1,752 | 122 | 61 | 1,813 | 3% |
| Dufferin St | 1,816 | 2,107 | 0 | 0 | 2,107 | 0% |
| Bathurst St | 2,142 | 2,485 | 673 | 337 | 2,821 | 12% |
| Screenline Total | 6,975 | 8,091 | 830 | 415 | 8,506 | 5% |

Note: Based on 2011 TTS, the passenger-car equivalent is 1.16. persons/car

5.2.1 2031 EMME Network with 2041 Demand

A link analysis was conducted for the year 2041 using York Region's 2041 projected travel demand (Origin-Destination Matrix) and 2031 planned/proposed network improvements identified in the York Region's 2020 10-year Capital Program.

As shown in **Figure 28**, it can be observed that virtually all the V/C ratio in the westbound and southbound directions would exceed the threshold limit of 1.00 by 2041. The analysis results suggest that network improvements would be required to accommodate future travel needs for the 2041 horizon year.

A snapshot of the 2031 EMME subarea network with 2041 travel demand is included in **Appendix H**.



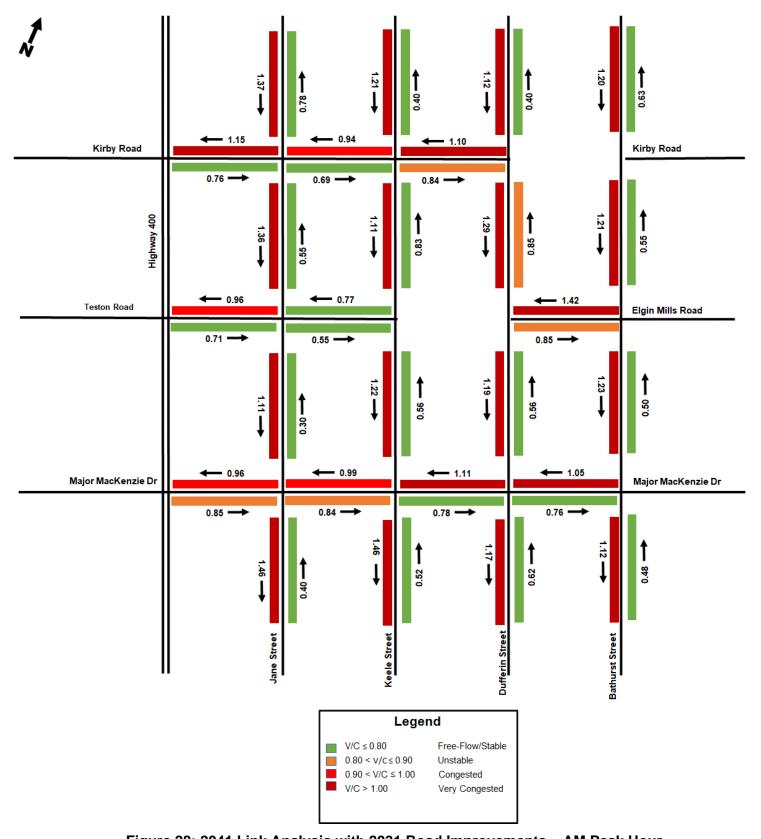


Figure 28: 2041 Link Analysis with 2031 Road Improvements - AM Peak Hour



Table 42 indicates that all major arterial roads crossing Screenlines SL2, SL3, SL4 and SL5 are functioning with a V/C ratio that exceeds 1.00 (i.e. volume exceeds capacity). The analysis results suggest that 2031 network cannot accommodate future travel needs for the 2041 horizon year and network improvements would be required.

Table 42: AM Peak Hour / Peak Direction Assigned Volumes and V/C (2031 EMME Model with 2041 Demand)

| Section | Volume | # Lanes (Per Direction) | Lane Capacity (Per Direction) | Total Capacity (Per Direction) | V/C |
|--------------------|--------|----------------------------|-------------------------------|--------------------------------|------|
| | | Screenline | | | |
| Major Mackenzie Dr | 1,590 | 2 | 800 | 1,600 | 0.99 |
| Teston Rd | 1,381 | 2 | 900 | 1,800 | 0.77 |
| Kirby Rd | 659 | 1 | 700 | 700 | 0.94 |
| Screenline Total | 3,630 | 5 | | 4100 | 0.89 |
| | | Screenline | | | |
| Major Mackenzie Dr | 2,006 | 2 | 900 | 1,800 | 1.11 |
| Kirby Rd | 773 | 1 | 700 | 700 | 1.10 |
| Screenline Total | 2,779 | 3 | | 2,500 | 1.11 |
| | | Screenline | | | |
| Major Mackenzie Dr | 1,882 | 2 | 900 | 1,800 | 1.05 |
| Teston Rd | 1,135 | 1 | 800 | 800 | 1.42 |
| Screenline Total | 3,017 | 3 | | 2,600 | 1.16 |
| | | Screenline | | | |
| Jane St | 1,362 | 1 | 1,000 | 1,000 | 1.36 |
| Keele St | 1,993 | 2 | 900 | 1,800 | 1.11 |
| Dufferin St | 1,293 | 1 | 1,000 | 1,000 | 1.29 |
| Bathurst St | 2,905 | 2 | 1,200 | 2,400 | 1.21 |
| Screenline Total | 7,553 | 6 | _ | 6,200 | 1.22 |
| | | Screenline | | | |
| Jane St | 1,994 | 2 | 900 | 1,800 | 1.11 |
| Keele St | 1,948 | 2 | 800 | 1,600 | 1.22 |
| Dufferin St | 2,150 | 2 | 900 | 1,800 | 1.19 |
| Bathurst St | 2,451 | 2 | 1000 | 2,000 | 1.23 |
| Screenline Total | 8,543 | 8 | | 7,200 | 1.19 |

5.3 2041 Subarea EMME Model

In addition to the planned/propose network improvements up to 2031 described previously, the Region's 2041 EMME model includes all additional planned/proposed network improvements identified in the York Region's 2016 TMP for the year 2041 (i.e. base case) condition:

- Jane Street widened between Teston Road and 15th Sideroad (Y.R. 40) from two to four lanes;
- Dufferin Street widened between Teston Road and 15th Sideroad (Y.R. 40) from two to four lanes;
- Bathurst Street widened between Major Mackenzie Drive and Kirby Road from four to six lanes;



- Kirby Road widened between Pine Valley Drive and Dufferin Street from two to four lanes;
- Kirby Road extended between Dufferin Street and Bathurst Street as a four-lane roadway. The City of Vaughan's EA for the Kirby Road Extension between Dufferin Street and Bathurst Street used the capacity of 900 veh/Lane/hr along Kirby Road in their modelling. As such, the capacity along Kirby Road was increased from 700 to 900 veh/Lane/hr for the year 2041 when the 4-lane widening is in place; and
- New Kirby Road / Highway 400 interchange at Highway 400.
- Teston Road widened between Dufferin Street and Bathurst Street from two to four lanes and the associated capacity was increased from 800 to 900 veh/Lane/hr for the year 2041 when the 4-lane widening is in place; and
- Teston Road was extended between Keele Street and Dufferin Street as a four-lane roadway. Teston Road extension will be excluded from the 2041 network while evaluating various future alternatives.
- A new mid-block connection across Highway 400 (Canada Drive-America Avenue Bridge). The new bridge includes a 2-lane roadway, sidewalks and bicycle lanes on a mostly straight alignment slightly shifted to the south side of the right of way and intersections at Cityview Boulevard/Canada Drive (requiring re-grading) and John Deisman Boulevard/ America Avenue.

5.3.1 Select Link Analysis for 2041 Network with and without GTA West

In August 2020 MTO confirmed the preferred route for the GTA West Multimodal Transportation Corridor (see **Figure 23**). However, as the project likely isn't funded yet by MTO further analysis was undertaken for the horizon year 2041 with and without the proposed GTA West freeway as part of the roadway network. A select link analysis was conducted for both options in order to identify the origins and destinations of forecast vehicles using Teston Road in the 2041 model during the AM peak hour.

5.3.1.1 2041 Model without GTA West

As mentioned above, the dominant traffic volumes during the morning peak hour are in the westbound and southbound directions. **Figures 29** illustrates that by 2041 without the GTA West freeway, the AM peak hour traffic volume in the westbound direction along Teston Road (between Keele Street and Dufferin Street) is in excess of 1,518 veh/h. The typical vehicle carrying capacity of a single lane on Teston Road is approximately 900 veh/h.

The 2041 forecast without GTA West indicates that projected vehicle flows along Teston Road are still significant and this section of Teston Road may require two lanes in each direction to



serve the forecast demand. Note that further analysis of this and other alternatives will be undertaken.

A snapshot of 2041 EMME subarea network without GTA West is included in **Appendix I**.

Figure 30 illustrates the 2041 V/C ratios without GTA West freeway for each key roadway. The figure indicates that virtually all southbound movements along arterial roads exhibit overcapacity conditions.

Table 43 illustrates the V/C ratio for each key roadway at the five screenlines in the study area for the year 2041 without the GTA West freeway. The overall V/C for Screenlines SL1 to SL4 exhibits values of 0.90 or less. However, Screenline SL5 is over-capacity (i.e V/C of 1.11) suggesting that all southbound traffic flow south of Teston Road are expected to be very congested by the year 2041.



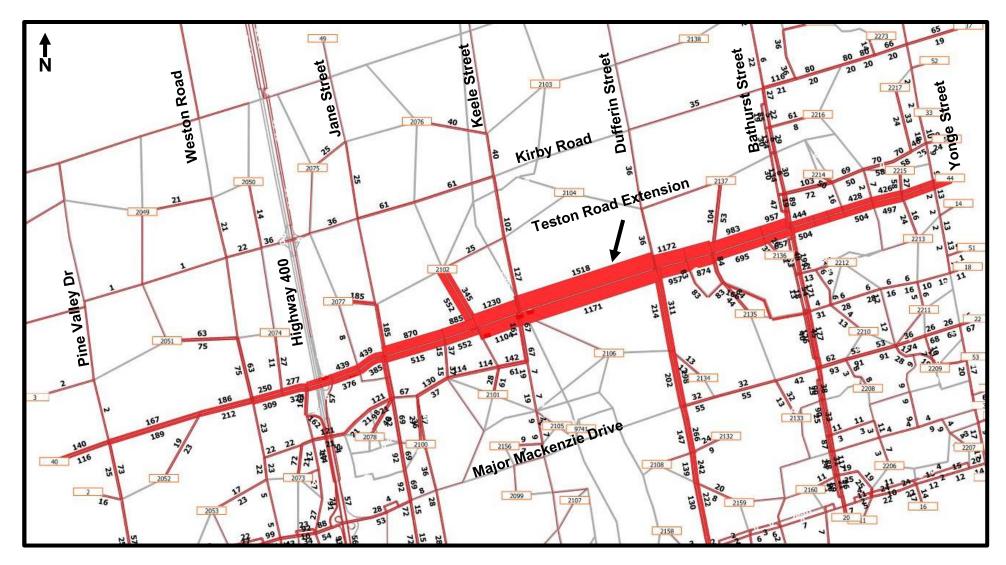


Figure 29: Select Link Analysis for Teston Road without GTA West - AM Peak Hour



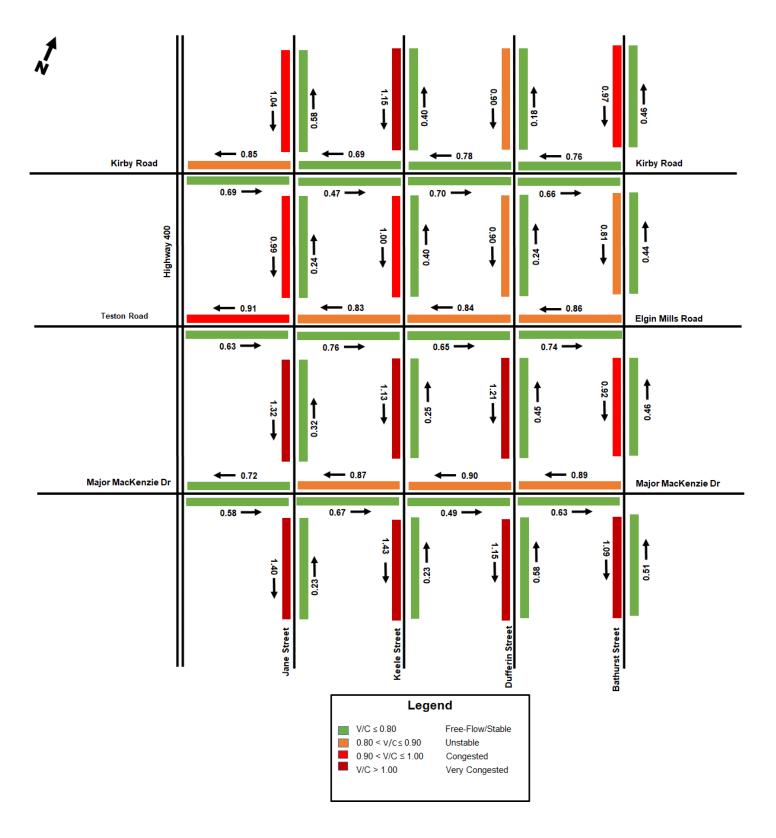


Figure 30: 2041 Link Analysis without GTA West - AM Peak Hour



Table 43: AM Peak Hour / Peak Direction Assigned Volumes and V/C (2041 EMME Model without GTA West)

| Section | Volume | # Lanes (Per Direction) | Lane Capacity (Per Direction) | Total Capacity (Per Direction) | V/C | | |
|--------------------|--------|----------------------------|----------------------------------|--------------------------------|------|--|--|
| Screenline 1 | | | | | | | |
| Major Mackenzie Dr | 1,385 | 2 | 800 | 1,600 | 0.87 | | |
| Teston Rd | 1,500 | 2 | 900 | 1,800 | 0.83 | | |
| Kirby Rd | 1,237 | 2 | 900 | 1,800 | 0.69 | | |
| Screenline Total | 4,122 | 6 | | 5,200 | 0.79 | | |
| | | Screenline | 2 | | | | |
| Major Mackenzie Dr | 1,628 | 2 | 900 | 1,800 | 0.90 | | |
| Teston Rd | 1,518 | 2 | 900 | 1,800 | 0.84 | | |
| Kirby Rd | 1,411 | 2 | 900 | 1,800 | 0.78 | | |
| Screenline Total | 4,557 | 6 | | 5,400 | 0.84 | | |
| | | Screenline | 3 | | | | |
| Major Mackenzie Dr | 1,610 | 2 | 900 | 1,800 | 0.89 | | |
| Teston Rd | 1,555 | 2 | 900 | 1,800 | 0.86 | | |
| Kirby Rd | 1,369 | 2 | 900 | 1,800 | 0.76 | | |
| Screenline Total | 4,534 | 6 | | 5,400 | 0.84 | | |
| | | Screenline | 9 4 | | | | |
| Jane St | 1,988 | 2 | 1000 | 2000 | 0.99 | | |
| Keele St | 1,798 | 2 | 900 | 1800 | 1.00 | | |
| Dufferin St | 1,792 | 2 | 1000 | 2000 | 0.90 | | |
| Bathurst St | 2,905 | 3 | 1200 | 3600 | 0.81 | | |
| Screenline Total | 8,483 | 9 | | 9,400 | 0.90 | | |
| | | Screenline | 2 5 | | | | |
| Jane St | 2,376 | 2 | 900 | 1800 | 1.32 | | |
| Keele St | 1,806 | 2 | 800 | 1600 | 1.13 | | |
| Dufferin St | 2,183 | 2 | 900 | 1800 | 1.21 | | |
| Bathurst St | 2,747 | 3 | 1000 | 3000 | 0.92 | | |
| Screenline Total | 9,112 | 9 | | 8,200 | 1.11 | | |

5.3.1.2 2041 Model with GTA West

Figures 31 illustrates that by 2041 with the GTA West freeway, the AM peak hour traffic volume in the westbound direction along Teston Road (between Keele Street and Dufferin Street) is in excess of 1,630 veh/h (only approximately 7% in excess of the volume without GTA West). The 2041 forecast with GTA West indicates that this section of Teston Road may require two lanes in each direction to serve the forecast demand. Note that further analysis of this and other alternatives will be undertaken.

A snapshot of 2041 EMME subarea network with GTA West is included in **Appendix J**.

Figure 32 illustrates the 2041 V/C ratios with GTA West freeway for each key roadway. The figure indicates that virtually all southbound movements along arterial roads exhibit over-capacity conditions, particularly south of Teston Road (although on



average approximately 5% better than without GTA West). However, all westbound movements along Kirby Road, Teston Road and Major Mackenzie Drive are functioning with a V/C ratio of 0.90 and less (although on average approximately 5% worse than without GTA West).

Table 44 illustrates the V/C ratio for each key roadway at the five screenlines in the study area for the year 2041 with the GTA West freeway. The overall V/C for Screenlines SL1 to SL4 exhibits values of 0.89 or less suggesting that the proposed capacity would accommodate future demand. However, Screenlines SL5 is over-capacity (i.e V/C of 1.06) suggesting that all southbound traffic flows south of Teston Road are expected to be very congested by the year 2041.

The corresponding 2041 projected am peak hour transit demand (i.e. transit person trips) at each screenline developed in the EMME model is summarized in **Table 45**. The summary of results indicates that by 2041 the transit trips are expected to increase significantly along all arterial roads, particularly along Major Mackenzie Drive (i.e. 623 westbound 2041 AM peak hour transit passenger trips and 25% Transit Mode Share between Dufferin and Keele). At SL2 westbound 2041 AM peak hour transit passenger trips are projected to increase from 85 trips and 3% Transit Mode Share in 2016 to 717 trips and 11% Transit Mode Share by 2041.

It is evident that by 2041 with the GTA West freeway in place and with the Kirby Road and Teston Road extensions available the area roads examined prove to be capable of accommodating primary peak hour peak direction demand flows.

Study area travel demand is higher in the scenario "with GTA West" in comparison to "without GTA West" and therefore, further scenario analysis including the GTA West corridor for this IEA is considered to be the most conservative approach. Based on the above assessment of the GTA West corridor, the 2041 option without GTA West freeway will be excluded from further traffic analysis.



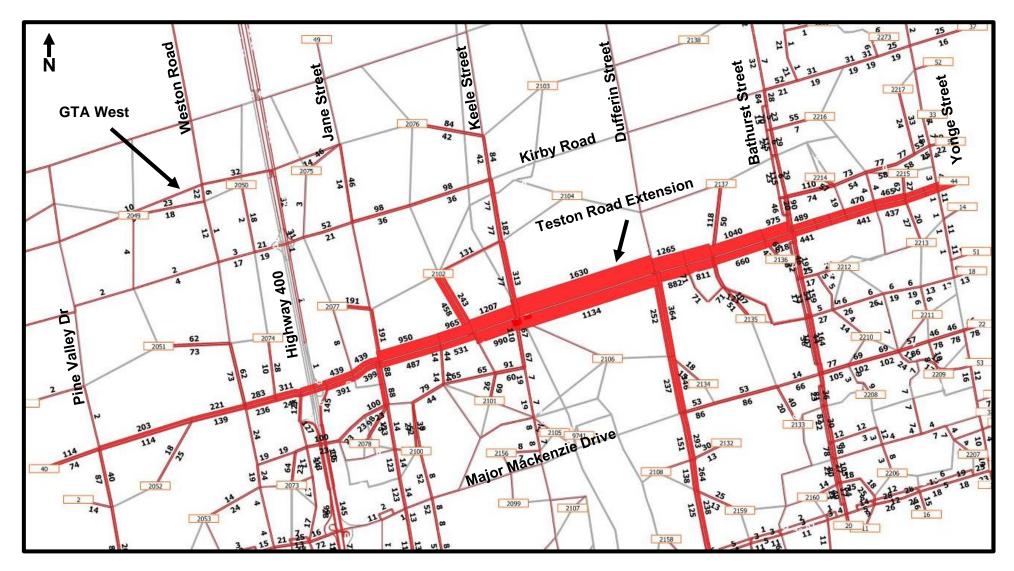


Figure 31: Select Link Analysis for Teston Road with GTA West - AM Peak Hour



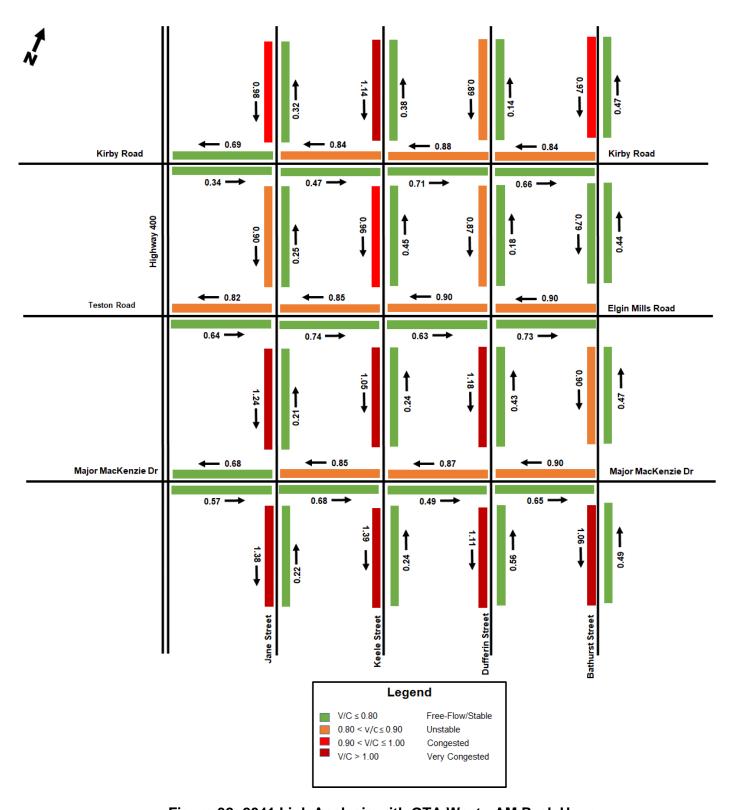


Figure 32: 2041 Link Analysis with GTA West - AM Peak Hour



Table 44: AM Peak Hour / Peak Direction Assigned Volumes and V/C (2041 EMME Model with GTA West)

| Section | Volume | # Lanes (Per Direction) | Lane Capacity (Per Direction) | Total Capacity (Per Direction) | V/C | | | |
|--------------------|--------------|----------------------------|-------------------------------|--------------------------------|------|--|--|--|
| Screenline 1 | | | | | | | | |
| Major Mackenzie Dr | 1,355 | 2 | 800 | 1,600 | 0.85 | | | |
| Teston Rd | 1,522 | 2 | 900 | 1,800 | 0.85 | | | |
| Kirby Rd | 1,503 | 2 | 900 | 1,800 | 0.84 | | | |
| Screenline Total | 4,380 | 6 | | 5,200 | 0.84 | | | |
| | Screenline 2 | | | | | | | |
| Major Mackenzie Dr | 1,568 | 2 | 900 | 1,800 | 0.87 | | | |
| Teston Rd | 1,637 | 2 | 900 | 1,800 | 0.91 | | | |
| Kirby Rd | 1,585 | 2 | 900 | 1,800 | 0.88 | | | |
| Screenline Total | 4,790 | 6 | | 5,400 | 0.89 | | | |
| | | Screenline | : 3 | | | | | |
| Major Mackenzie Dr | 1,616 | 2 | 900 | 1,800 | 0.90 | | | |
| Teston Rd | 1,611 | 2 | 900 | 1,800 | 0.90 | | | |
| Kirby Rd | 1,518 | 2 | 900 | 1,800 | 0.84 | | | |
| Screenline Total | 4,745 | 6 | | 5,400 | 0.88 | | | |
| | | Screenline | 4 | | | | | |
| Jane St | 1,805 | 2 | 1,000 | 2,000 | 0.90 | | | |
| Keele St | 1,723 | 2 | 900 | 1,800 | 0.96 | | | |
| Dufferin St | 1,747 | 2 | 1,000 | 20,00 | 0.87 | | | |
| Bathurst St | 2,840 | 3 | 1,200 | 3,600 | 0.79 | | | |
| Screenline Total | 8,115 | 9 | | 9,400 | 0.86 | | | |
| | | Screenline | 5 | | | | | |
| Jane St | 2,224 | 2 | 900 | 1,800 | 1.24 | | | |
| Keele St | 1,675 | 2 | 800 | 1,600 | 1.05 | | | |
| Dufferin St | 2,132 | 2 | 900 | 1,800 | 1.18 | | | |
| Bathurst St | 2,698 | 3 | 1,000 | 3,000 | 0.90 | | | |
| Screenline Total | 8,729 | 9 | | 8,200 | 1.06 | | | |



Table 45: AM Peak Hour / Peak Direction Transit Person Trips (2041 EMME Model with GTA West)

| Tabour Passenger Car Passenger Trips Transit Passenger Trips Transit Passenger Trips Transit Passenger Trips Transit Passenger Trips Trips Transit Passenger Trips | | | | | | | | | |
|--|--------------------|-------|---|-------------------------------|----------------------|-----------|------|--|--|
| Major Mackenzie Dr 1,355 1,572 1,220 610 2,182 28% Teston Rd 1,522 1,766 140 70 1,836 4% Kirby Rd 1,503 1,743 186 93 1,836 5% Screenline Total 4,380 5,081 1,546 773 5,854 13% Screenline Total 4,380 5,081 1,546 773 5,854 13% Screenline Total 4,380 5,081 1,546 773 5,854 13% Screenline 2 (WB) Major Mackenzie Dr 1,568 1,819 1,245 623 2,441 25% 1% Kirby Rd 1,585 1,839 135 68 1,906 4% Screenline Total 4,790 5,556 1,434 717 6,273 11% Magor Mackenzie Dr 1,616 1,875 1,144 572 2,447 23% 1% Kirby Rd 1,518 1,761 134 67 | Section | Auto | Passenger Car Equivalent ¹ | Transit Passenger Trips | Transit Passenger | Passenger | Mode | | |
| Teston Rd 1,522 1,766 140 70 1,836 4% Kirby Rd 1,503 1,743 186 93 1,836 5% Screenline Total 4,380 5,081 1,546 773 5,854 13% Screenline Total 4,380 5,081 1,546 773 5,854 13% Screenline Total 4,380 5,081 1,546 773 5,854 13% Screenline Z (WB) Major Mackenzie Dr 1,568 1,819 1,245 623 2,441 25% Teston Rd 1,637 1,899 54 27 1,926 1% Kirby Rd 1,585 1,839 135 68 1,906 4% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline Total 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline Total 4,745 5,504 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline Screenl | Screenline 1 | | | | | | | | |
| Kirby Rd 1,503 1,743 186 93 1,836 5% Screenline Total 4,380 5,081 1,546 773 5,854 13% Screenline Z (WB) Major Mackenzie Dr 1,568 1,819 1,245 623 2,441 25% Teston Rd 1,637 1,899 54 27 1,926 1% Kirby Rd 1,585 1,839 135 68 1,906 4% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline 3 (WB) Major Mackenzie Dr 1,616 1,875 1,144 572 2,447 23% Teston Rd 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Scree | Major Mackenzie Dr | 1,355 | 1,572 | 1,220 | 610 | 2,182 | 28% | | |
| Major Mackenzie Dr | Teston Rd | 1,522 | 1,766 | 140 | 70 | 1,836 | 4% | | |
| Screenline 2 (WB) Major Mackenzie Dr 1,568 1,819 1,245 623 2,441 25% Teston Rd 1,637 1,899 54 27 1,926 1% Kirby Rd 1,585 1,839 135 68 1,906 4% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline 3 (WB) Major Mackenzie Dr 1,616 1,875 1,144 572 2,447 23% Teston Rd 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline Total 4,745 2,094 218 109 2,203 5% < | Kirby Rd | 1,503 | 1,743 | 186 | 93 | 1,836 | 5% | | |
| Major Mackenzie Dr 1,568 1,819 1,245 623 2,441 25% Teston Rd 1,637 1,899 54 27 1,926 1% Kirby Rd 1,585 1,839 135 68 1,906 4% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline 3 (WB) Major Mackenzie Dr 1,616 1,875 1,144 572 2,447 23% Teston Rd 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,747 2,027 9 5 2,031 0% Bathurst St | Screenline Total | 4,380 | 5,081 | 1,546 | 773 | 5,854 | 13% | | |
| Teston Rd 1,637 1,899 54 27 1,926 1% Kirby Rd 1,585 1,839 135 68 1,906 4% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline 3 (WB) Major Mackenzie Dr 1,616 1,875 1,144 572 2,447 23% Teston Rd 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | | | Scre | enline 2 (WB) | | | | | |
| Kirby Rd 1,585 1,839 135 68 1,906 4% Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline 3 (WB) Major Mackenzie Dr 1,616 1,875 1,144 572 2,447 23% Teston Rd 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline 5 (SB) Jane St 2,224 2,580 < | Major Mackenzie Dr | 1,568 | 1,819 | 1,245 | 623 | 2,441 | 25% | | |
| Screenline Total 4,790 5,556 1,434 717 6,273 11% Screenline 3 (WB) Major Mackenzie Dr 1,616 1,875 1,144 572 2,447 23% Teston Rd 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) </td <td>Teston Rd</td> <td>1,637</td> <td>1,899</td> <td>54</td> <td>27</td> <td>1,926</td> <td>1%</td> | Teston Rd | 1,637 | 1,899 | 54 | 27 | 1,926 | 1% | | |
| Screenline 3 (WB) Major Mackenzie Dr 1,616 1,875 1,144 572 2,447 23% Teston Rd 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% <t< td=""><td>Kirby Rd</td><td>1,585</td><td>1,839</td><td>135</td><td>68</td><td>1,906</td><td>4%</td></t<> | Kirby Rd | 1,585 | 1,839 | 135 | 68 | 1,906 | 4% | | |
| Major Mackenzie Dr 1,616 1,875 1,144 572 2,447 23% Teston Rd 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 | Screenline Total | 4,790 | | | 717 | 6,273 | 11% | | |
| Teston Rd 1,611 1,869 55 28 1,896 1% Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | | | Scre | enline 3 (WB) | | | | | |
| Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 <t< td=""><td>Major Mackenzie Dr</td><td>1,616</td><td>1,875</td><td>1,144</td><td>572</td><td>2,447</td><td>23%</td></t<> | Major Mackenzie Dr | 1,616 | 1,875 | 1,144 | 572 | 2,447 | 23% | | |
| Kirby Rd 1,518 1,761 134 67 1,828 4% Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 <td>Teston Rd</td> <td>1,611</td> <td>1,869</td> <td>55</td> <td>28</td> <td>1,896</td> <td>1%</td> | Teston Rd | 1,611 | 1,869 | 55 | 28 | 1,896 | 1% | | |
| Screenline Total 4,745 5,504 1,333 667 6,171 11% Screenline 4 (SB) Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | Kirby Rd | 1,518 | 1,761 | 134 | 67 | 1,828 | | | |
| Jane St 1,805 2,094 218 109 2,203 5% Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | | | 5,504 | 1,333 | 667 | | 11% | | |
| Keele St 1,723 1,999 298 149 2,148 7% Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | | | | | | | | | |
| Dufferin St 1,747 2,027 9 5 2,031 0% Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | Jane St | 1,805 | 2,094 | 218 | 109 | 2,203 | 5% | | |
| Bathurst St 2,840 3,294 578 289 3,583 8% Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | Keele St | 1,723 | 1,999 | 298 | 149 | 2,148 | 7% | | |
| Screenline Total 8,115 9,413 1,103 552 9,965 6% Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | Dufferin St | 1,747 | 2,027 | 9 | 5 | 2,031 | 0% | | |
| Screenline 5 (SB) Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | | | 3,294 | | | 3,583 | 8% | | |
| Jane St 2,224 2,580 253 127 2,706 5% Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | Screenline Total | 8,115 | | | 552 | 9,965 | 6% | | |
| Keele St 1,675 1,943 592 296 2,239 13% Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | Screenline 5 (SB) | | | | | | | | |
| Dufferin St 2,132 2,473 35 18 2,491 1% Bathurst St 2,698 3,130 606 303 3,433 9% | Jane St | 2,224 | 2,580 | 253 | 127 | 2,706 | 5% | | |
| Bathurst St 2,698 3,130 606 303 3,433 9% | Keele St | 1,675 | 1,943 | 592 | 296 | 2,239 | 13% | | |
| | Dufferin St | 2,132 | 2,473 | 35 | 18 | 2,491 | 1% | | |
| Screenline Total 8,729 10,126 1,486 743 10,869 7% | Bathurst St | 2,698 | 3,130 | 606 | 303 | 3,433 | 9% | | |
| | Screenline Total | 8,729 | 10,126 | 1,486 | 743 | 10,869 | 7% | | |

Note: Based on 2011 TTS, the passenger-car equivalent is 1.16. persons/car



6. NOTHING OPTION

The Do-Nothing Option includes York Region's 2041 EMME model with all planned/ proposed network improvements identified in the York Region's 2016 TMP (e.g., GTA West) with the exception of the Teston Road extension between Keele Street and Dufferin Street.

A snapshot of the 2041 EMME subarea network for the Do-Nothing Option is included in **Appendix K**.

6.1 Link Analysis for Do-Nothing Option

A link analysis was conducted for the Do-Nothing Option using the 2041 traffic volumes reported from the model during the morning peak hour. **Figure 33** illustrates the 2041 V/C ratios for each key roadway. The figure indicates that virtually all westbound movements on parallel arterial roads north and south of Teston Road and all southbound movements along north-south arterial roads are expected to exceed capacity.

It is very evident that the traffic flow in order to complete their direction of travel causes increased vehicle movements on adjacent arterial roads (e.g. Keele Street) and creates a barrier to people from other subdivisions (e.g. Drummond Drive) to access these already congested roadways.

Figure 34 shows the change in Assigned Traffic Volumes in the EMME model comparing the 2041 with Teston Road Extension and 2041 Do-Nothing scenarios. **Figure 34** illustrates that by 2041 with the Teston Road Extension, the AM peak hour traffic volume in the westbound direction along Teston Road (between Keele Street and Dufferin Street) is in excess of 1,630 veh/h. If this project segment were not available this projected significant traffic flow would have to find alternate routes. The forecasted volumes indicate that the equivalent of two lanes of traffic capacity in each direction of travel would have to be found in one or more adjacent roadway corridors or be accommodated through some other mode of travel (i.e. transit) or other alternative solution.

In addition, the discontinuity on Teston Road between Keele Street and Dufferin Street results in longer trip distances which may increase greenhouse gas emissions and potentially have negative impacts on climate change.

Table 46 illustrates the V/C ratio for each key roadway at the five screenlines in the study area for the 2041 Do-Nothing Option. The overall V/C for Screenlines SL1, SL3 and SL4 exhibits values of 0.90 or less. However, Screenlines SL2 and SL5 exhibit values of 1.15 and 1.05, respectively, suggesting that the demand well exceeds the available capacity. Note that the above V/C for SL2 does not account for trips diverted to King Vaughan Road or to Rutherford Road in **Figure 34**.

Table 47 illustrates the AM peak hour / peak direction transit person trips for the Do-Nothing Option.



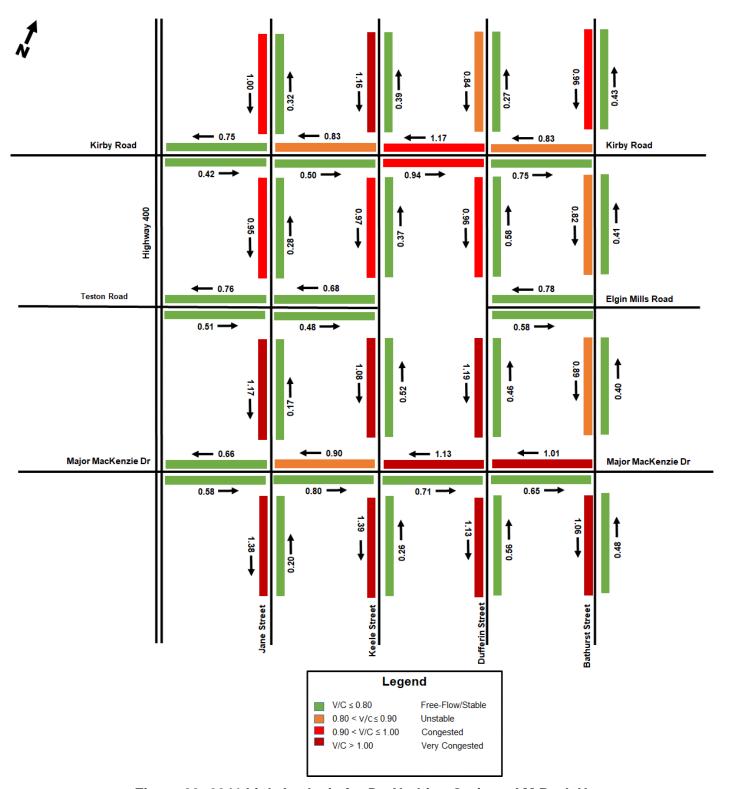


Figure 33: 2041 Link Analysis for Do-Nothing Option - AM Peak Hour





Figure 34: 2041 Do-Nothing Option vs. 2041 with Teston Road Extension (Assigned Traffic Volumes)



Table 46: AM Peak Hour / Peak Direction Assigned Volumes and V/C (2041 EMME Model for Do-Nothing Option)

| Section | Volume | # Lanes (Per Direction) | Lane Capacity (Per Direction) | Total Capacity (Per Direction) | V/C | | | |
|--------------------|--------------|----------------------------|----------------------------------|-----------------------------------|------|--|--|--|
| Screenline 1 | | | | | | | | |
| Major Mackenzie Dr | 1,439 | 2 | 800 | 1,600 | 0.90 | | | |
| Teston Rd | 1,217 | 2 | 900 | 1,800 | 0.68 | | | |
| Kirby Rd | 1,497 | 2 | 900 | 1,800 | 0.83 | | | |
| Screenline Total | 4,153 | 6 | | 5,200 | 0.80 | | | |
| | | Screenline | 2 | | | | | |
| Major Mackenzie Dr | 2,039 | 2 | 900 | 1,800 | 1.13 | | | |
| Kirby Rd | 2,114 | 2 | 900 | 1,800 | 1.17 | | | |
| Screenline Total | 4,153 | 4 | | 3,600 | 1.15 | | | |
| | | Screenline | 3 | | | | | |
| Major Mackenzie Dr | 1,823 | 2 | 900 | 1,800 | 1.01 | | | |
| Teston Rd | 1,406 | 2 | 900 | 1,800 | 0.78 | | | |
| Kirby Rd | 1,489 | 2 | 900 | 1,800 | 0.83 | | | |
| Screenline Total | 4,718 | 6 | | 5,400 | 0.87 | | | |
| | Screenline 4 | | | | | | | |
| Jane St | 1,901 | 2 | 1,000 | 2,000 | 0.95 | | | |
| Keele St | 1,748 | 2 | 900 | 1,800 | 0.97 | | | |
| Dufferin St | 1,914 | 2 | 1,000 | 2,000 | 0.96 | | | |
| Bathurst St | 2,942 | 3 | 1,200 | 3,600 | 0.82 | | | |
| Screenline Total | 8,505 | 9 | | 9,400 | 0.90 | | | |
| | | Screenline | | | | | | |
| Jane St | 2,112 | 2 | 900 | 1,800 | 1.17 | | | |
| Keele St | 1,728 | 2 | 800 | 1,600 | 1.08 | | | |
| Dufferin St | 2,139 | 2 | 900 | 1,800 | 1.19 | | | |
| Bathurst St | 2,657 | 3 | 1,000 | 3,000 | 0.89 | | | |
| Screenline Total | 8,636 | 9 | | 8,200 | 1.05 | | | |



Table 47: AM Peak Hour / Peak Direction Transit Person Trip (2041 EMME Model for Do-Nothing Option)

| Section | 1-hour Auto trips | 1-hour Passenger Car Equivalent | 3-hour Transit Passenger Trips | 1-hour Transit Passenger Trips | 1-hour Total Passenger Trips | Transit Mode Share | | | |
|--------------------|-------------------------|---------------------------------------|---|---|------------------------------------|--------------------------|--|--|--|
| Screenline 1 | | | | | | | | | |
| Major Mackenzie Dr | 1,439 | 1,669 | 1,229 | 615 | 2,284 | 27% | | | |
| Teston Rd | 1,217 | 1,412 | 129 | 65 | 1,476 | 4% | | | |
| Kirby Rd | 1,497 | 1,737 | 189 | 95 | 1,831 | 5% | | | |
| Screenline Total | 4,153 | 4,817 | 1,547 | 774 | 5,591 | 14% | | | |
| | | Scr | eenline 2 (WB) | | | | | | |
| Major Mackenzie Dr | 2,039 | 2,365 | 1,256 | 628 | 2,993 | 21% | | | |
| Kirby Rd | 2,114 | 2,452 | 174 | 87 | 2,539 | 3% | | | |
| Screenline Total | 4,153 | 4,817 | 1,430 | 715 | 5,532 | 13% | | | |
| | | Scr | eenline 3 (WB) | | | | | | |
| Major Mackenzie Dr | 1,823 | 2,115 | 1,153 | 577 | 2,691 | 21% | | | |
| Teston Rd | 1,406 | 1,631 | 36 | 18 | 1,649 | 1% | | | |
| Kirby Rd | 1,489 | 1,727 | 137 | 69 | 1,796 | 4% | | | |
| Screenline Total | 4,718 | 5,473 | 1,326 | 663 | 6,136 | 11% | | | |
| | , | | eenline 4 (SB) | | · | | | | |
| Jane St | 1,901 | 2,205 | 211 | 106 | 2,311 | 5% | | | |
| Keele St | 1,748 | 2,028 | 240 | 120 | 2,148 | 6% | | | |
| Dufferin St | 1,914 | 2,220 | 103 | 52 | 2,272 | 2% | | | |
| Bathurst St | 2,942 | 3,413 | 577 | 289 | 3,701 | 8% | | | |
| Screenline Total | 8,505 | 9,866 | 1,131 | 566 | 10,431 | 5% | | | |
| | | Scr | eenline 5 (SB) | | | | | | |
| Jane St | 2,112 | 2,450 | 254 | 127 | 2,577 | 5% | | | |
| Keele St | 1,728 | 2,004 | 615 | 308 | 2,312 | 13% | | | |
| Dufferin St | 2,139 | 2,481 | 45 | 23 | 2,504 | 1% | | | |
| Bathurst St | 2,657 | 3,082 | 598 | 299 | 3,381 | 9% | | | |
| Screenline Total | 8,636 | 10,018 | 1,512 | 756 | 10,774 | 7% | | | |
| | | | | | | | | | |

Note: Based on 2011 TTS, the passenger-car equivalent is 1.16. persons/car

6.2 Projected Intersection Traffic Volumes (2041)

Projected turning movement volumes were developed for the 2041 Do-Nothing Option based on the EMME model projections above. As previously mentioned, this scenario included all network modifications (i.e. road widenings) along study area roadways. **Figure 35** illustrates the projected AM peak hour turning movement volumes for the 2041 Do-Nothing scenario.



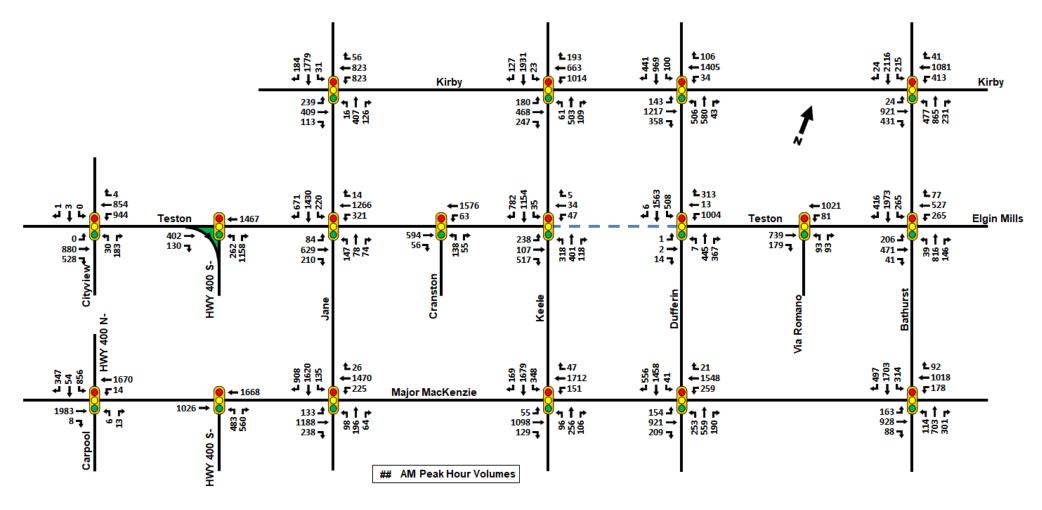
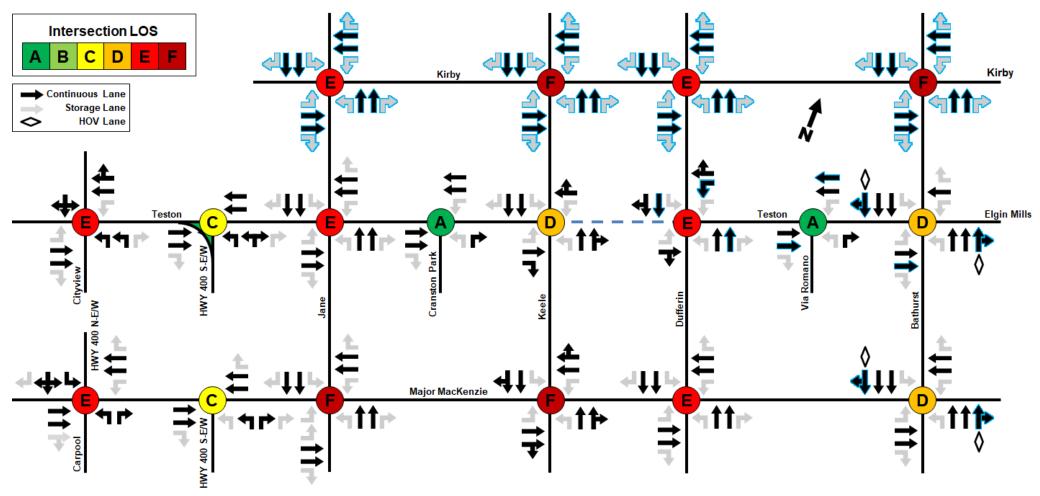


Figure 35: Projected Traffic Volumes (2041)





Lane arrows outlined in blue are new lanes from background study area road widenings.

Figure 36: Future Intersection Operational Performance (2041)



6.3 Projected Intersection Operational Performance Analysis (2041)

Traffic analysis was completed for the 2041 Do-Nothing scenario to provide an assessment of the projected traffic volume condition at study area intersections. This analysis included all network modifications (i.e. road widenings) anticipated for buildout by 2041. **Figure 36** and **Table 48** displays the results of this analysis. Detailed Synchro reports are provided in **Appendix L**.

Table 48: Intersection Performance – Projected Conditions (2041) – AM Peak Hour

| Intersections | Movements | Delay (s) | LOS | v/c Ratio | 95th Queue (m) |
|-------------------|-----------|-----------|-----|-----------|----------------|
| mioroodions | EBL | 0 | A | 0.00 | 0 |
| | EBT | 65 | E | 0.96 | 174 |
| | EBR | 42 | D | 0.52 | 65 |
| | WBL | 138 | F | 1.21 | 393 |
| Teston / Cityview | WBTR | 5 | A | 0.35 | 52 |
| . colon, on, non | NBL | 52 | D | 0.12 | 9 |
| | NBR | 52 | D | 0.13 | 22 |
| | SBLTR | 57 | Ē | 0.04 | 4 |
| | Overall | 65 | Ē | 0.94 | <u>.</u> |
| | EBT | 10 | Ā | 0.21 | 28 |
| | EBR | 1 | A | 0.09 | 0 |
| Teston / Highway | WBT | 17 | В | 0.77 | 144 |
| 400 | NBLR | 27 | C | 0.62 | 54 |
| | NBR | 34 | Ċ | 0.75 | 90 |
| | Overall | 21 | C | 0.76 | - |
| | EBL | 40 | D | 0.50 | 25 |
| | EBT | 47 | D | 0.64 | 107 |
| | EBR | 41 | D | 0.28 | 42 |
| | WBL | 49 | D | 0.86 | 100 |
| | WBT | 68 | E | 0.99 | 238 |
| | WBR | 30 | С | 0.01 | 0 |
| Teston / Jane | NBL | 70 | E | 0.85 | 65 |
| | NBT | 20 | В | 0.05 | 11 |
| | NBR | 20 | В | 0.05 | 4 |
| | SBL | 33 | С | 0.42 | 69 |
| | SBT | 63 | E | 0.99 | 270 |
| | SBR | 60 | E | 0.91 | 237 |
| | Overall | 57 | E | 0.95 | - |
| | EBT | 5 | Α | 0.24 | 26 |
| | EBR | 4 | Α | 0.04 | 3 |
| | WBL | 4 | Α | 0.11 | 8 |
| Teston / Cranston | WBT | 8 | Α | 0.63 | 97 |
| | NBL | 38 | D | 0.50 | 40 |
| | NBR | 34 | С | 0.04 | 10 |
| | Overall | 9 | Α | 0.61 | - |
| | EBL | 24 | С | 0.44 | 53 |
| | EBT | 30 | С | 0.21 | 32 |
| | EBR | 37 | D | 0.55 | 67 |
| Teston / Keele | WBL | 23 | С | 0.14 | 13 |
| 1 OSIOH / NOCIO | WBTR | 29 | С | 0.08 | 14 |
| | NBL | 88 | F | 1.01 | 109 |
| | NBTR | 17 | В | 0.33 | 42 |
| | SBL | 26 | С | 0.12 | 13 |



| | | | | _ | |
|-------------------|-------------------|------------------|--------|---------------------|----------------|
| Intersections | Movements | Delay (s) | LOS | v/c Ratio | 95th Queue (m) |
| | SBT | 56 | E | 0.97 | 176 |
| | SBR | 35 | С | 0.59 | 60 |
| | Overall | 42 | D | 0.77 | - |
| | EBL | 42 | D | 0.00 | 1 |
| | EBTR | 47 | D | 0.03 | 8 |
| | WBL | 113 | F | 1.09 | 205 |
| | WBT | 26 | С | 0.24 | 22 |
| Teston / Dufferin | NBL | 51 | D | 0.14 | 7 |
| 100ton/ Bunomi | NBT | 55 | D | 0.60 | 81 |
| | NBR | 21 | С | 0.26 | 14 |
| | SBL | 97 | F | 1.08 | 181 |
| | SBTR | 80 | E | 1.05 | 296 |
| | Overall | 77 | E | 0.88 | - |
| | EBT | 5 | Α | 0.34 | 25 |
| | EBR | 4 | Α | 0.13 | 5 |
| Teston / Via | WBL | 5 | Α | 0.19 | 9 |
| Romano | WBT | 6 | A | 0.45 | 38 |
| | NBL | 21 | C | 0.33 | 18 |
| | NBR | 20 | В | 0.06 | 9 |
| | Overall | 6 | A | 0.43 | - |
| | EBL | 107 | F | 1.02 | 95 77 |
| | EBT | 44 | D | 0.50 | 77 |
| | EBR | 38 | D | 0.03 | 0 |
| | WBL | 47 | D | 0.79 | 77 |
| | WBT | 97 | F | 1.03 | 223 |
| Teston / Bathurst | WBR | 38 | D | 0.06 | 8 |
| resion / bainursi | NBL NBT | 115 28 | F C | 0.82 0.52 | 34 104 |
| | NBR | 26 22 | C | 0.52 | 104 |
| | SBL | 31 | C | 0.78 | 55 |
| | SBT | 51 51 | D | 1.00 | 339 |
| | SBR | 19 | В | 0.35 | 43 |
| | Overall | 49 | D | 1.01 | - |
| | EBTR | 47 | D | 0.92 | 233 |
| | WBL | 30 | Č | 0.15 | 5 |
| | WBT | 65 | Ě | 1.02 | 316 |
| Major MacKenzie / | NBL | 70 | Ē | 0.16 | 7 |
| Highway 400 West | NBR | 67 | Ē | 0.01 | 0 |
| Ramp | SBL | 62 | Ē | 0.88 | 236 |
| r | SBLTR | 69 | E | 0.92 | 247 |
| | SBR | 47 | D | 0.67 | 116 |
| | Overall | 56 | E | 0.95 | - |
| | EBT | 9 | Α | 0.42 | 92 |
| Major MacKenzie / | WBT | 9 | Α | 0.68 | 77 |
| Highway 400 East | NBL | 65 | E | 0.75 | 91 |
| Ramp | NBR | 65 | E | 0.74 | 82 |
| | Overall | 24 | С | 0.71 | - |
| | EBL | 81 | F | 0.59 | 34 |
| | EBT | 68 | E | 0.98 | 243 |
| Major MacKenzie / | EBR | 38 | D | 0.32 | 57 |
| Jane | WBL | 154 | F | 1.13 | 120 |
| | WBT | 113 | F | 1.11 | 323 |
| | WBR | 33 | С | 0.06 | 13 |



| Intersections | Movements | Delay (s) | LOS | v/c Ratio | 95th Queue (m) |
|--------------------------|-----------|------------------|--------|----------------------|-----------------|
| | NBL | 47 | D | 0.66 | 39 |
| | NBT | 29 | С | 0.14 | 29 |
| | NBR | 27 | С | 0.05 | 4 |
| | SBL | 24 | С | 0.24 | 36 |
| | SBT | 89 | F | 1.07 | 340 |
| | SBR | 163 | F | 1.23 | 404 |
| | Overall | 96 | F | 1.14 | - |
| | EBL | 39 | D | 0.41 | 18 |
| | EBTR | 58 | E | 0.92 | 244 |
| | WBL | 93 | F | 0.92 | 78 |
| | WBTR | 153 | F | 1.22 | 410 |
| Major MacKenzie / | NBL | 50 | D | 0.65 | 38 |
| Keele | NBTR | 45 | D | 0.34 | 60 |
| | SBL | 31 | C | 0.65 | 95 |
| | SBTR | 191 | F | 1.31 | 437 |
| | Overall | 126 | F | 1.20 | 4 37 |
| | EBL | 76 | E | 0.90 | 68 |
| | EBT | 7 6 44 | D | 0. 90 0.75 | 145 |
| | | | | | |
| | EBR | 33 | C | 0.23 | 34 |
| | WBL | 58 | E | 0.88 | 93 |
| | WBT | 87 | F | 1.07 | 290 |
| Major MacKenzie / | WBR | 26 | C | 0.01 | 0 |
| Dufferin | NBL | 246 | F | 1.39 | 131 |
| 2 3.1.3.11. | NBT | 33 | C | 0.43 | 80 |
| | NBR | 29 | С | 0.13 | 16 |
| | SBL | 24 | С | 0.12 | 13 |
| | SBT | 101 | F | 1.10 | 284 |
| | SBR | 53 | D | 0.85 | 188 |
| | Overall | 76 | E | 1.08 | - |
| | EBL | 94 | F | 0.97 | 76 |
| | EBT | 66 | E | 0.94 | 177 |
| | EBR | 1 | Α | 0.06 | 0 |
| | WBL | 105 | F | 1.01 | 83 |
| | WBT | 73 | E | 0.98 | 193 |
| Major MacKenzie / | WBR | 36 | D | 0.06 | 7 |
| Bathurst | NBL | 39 | D | 0.64 | 39 |
| Datituist | NBT | 32 | С | 0.51 | 99 |
| | NBR | 29 | С | 0.31 | 47 |
| | SBL | 23 | C C | 0.69 | 61 |
| | SBT | 54 | D | 0.98 | 295 |
| | SBR | 27 | С | 0.55 | 101 |
| | Overall | 52 | D | 0.94 | - |
| | EBL | 54 | D | 0.85 | 65 |
| | EBT | 88 | F | 1.00 | 73 |
| | EBR | 40 | D | 0.07 | 9 |
| | WBL | 210 | F | 1.39 | 265 |
| | WBT | 38 | D | 0.80 | 100 |
| Kirby / Jane | WBR | 26 | Ċ | 0.04 | 2 |
| · , · · · · · · · | NBL | 18 | В | 0.26 | 8 |
| | NBT | 16 | В | 0.26 | 34 |
| | NBR | 16 | В | 0.18 | 24 |
| | SBL | 15 | В | 0.07 | 8 |
| | SBT | 65 | E | 1.06 | 242 |
| | וטט | 00 | _ | 1.00 | L7L |



| Intersections | Movements | Delay (s) | LOS | v/c Ratio | 95th Queue (m) |
|------------------|-----------|------------|--------|-------------|----------------|
| | SBR | 16 | В | 0.24 | 34 |
| | Overall | 77 | E | 1.14 | - |
| | EBL | 186 | F | 1.18 | 110 |
| | EBT | 53 | D | 0.61 | 83 |
| | EBR | 57 | E | 0.64 | 81 |
| | WBL | 384 | F | 1.76 | 474 |
| | WBT | 25 | С | 0.39 | 78 |
| | WBR | 22 | С | 0.13 | 13 |
| Kirby / Keele | NBL | 323 | F | 1.42 | 42 |
| | NBT | 26 | С | 0.33 | 61 |
| | NBR | 23 | С | 0.07 | 11 |
| | SBL | 23 | С | 0.09 | 10 |
| | SBT | 130 | F | 1.19 | 391 |
| | SBR | 24 | С | 0.14 | 24 |
| | Overall | 139 | F | 1.43 | - |
| | EBL | 45 | D | 0.75 | 52 |
| | EBT | 34 | С | 0.78 | 170 |
| | EBR | 25 | С | 0.36 | 52 |
| | WBL | 51 | D | 0.59 | 25 |
| | WBT | 95 | F | 1.09 | 255 |
| | WBR | 29 | С | 0.07 | 12 |
| Kirby / Dufferin | NBL | 143 | F | 1.18 | 204 |
| | NBT | 22 | C | 0.34 | 62 |
| | NBR | 20 | В | 0.03 | 4 |
| | SBL | 52 | D | 0.51 | 42 |
| | SBT | 78 | E | 1.01 | 177 |
| | SBR | 63 | E | 0.84 | 143 |
| | Overall | 65 | E | 1.03 | - |
| | EBL | 52 | D | 0.44 | 18 |
| | EBT | 105 | F | 1.07 | 190 |
| | EBR | 63 | E | 0.81 | 133 |
| | WBL | 408 | F | 1.78 | 219 |
| | WBT | 50 | D | 0.86 | 175 |
| ICH / Dath and | WBR | 31 | C | 0.03 | 4 |
| Kirby / Bathurst | NBL | 429 | F | 1.81 | 250 |
| | NBT | 27 | C C | 0.51 | 105 |
| | NBR | 21 | | 0.14 | 14 |
| | SBL | 19 166 | В | 0.55 | 37 |
| | SBT | 166 | F | 1.27 | 429 |
| | SBR | 21 | C F | 0.01 | 0 |
| | Overall | 137 | r | 1.30 | - |

Note: LOS is based on vehicle delays

As a result of the analysis shown above, it is evident that the projected traffic volumes cannot be accommodated within the background 2041 Do-Nothing scenario. Numerous failing (i.e. LOS F) turning movements were reported along with some locations reporting failing conditions for the whole intersection. The following **Table 49** provides a summary of intersections reporting the highest impacts to traffic operations within the study area.



Table 49: Critical Intersection Summary – 2041 Do-Nothing Scenario

| Intersections | Movements | Delay (s) | LOS | v/c Ratio | 95th Queue (m) |
|-------------------|-----------|-----------|-----|-----------|----------------|
| | NBL | 88 | F | 1.01 | 109 |
| Teston / Keele | SBT | 56 | E | 0.97 | 176 |
| | Overall | 42 | D | 0.77 | - |
| | WBL | 113 | F | 1.09 | 205 |
| Teston / Dufferin | SBL | 97 | F | 1.08 | 181 |
| restor/ Dunelin | SBTR | 80 | E | 1.05 | 296 |
| | Overall | 77 | E | 0.88 | - |
| | EBTR | 58 | E | 0.92 | 244 |
| Major Maakanzia / | WBL | 93 | F | 0.92 | 78 |
| Major MacKenzie / | WBTR | 153 | F | 1.22 | 410 |
| Keele | SBTR | 191 | F | 1.31 | 437 |
| | Overall | 126 | F | 1.20 | - |
| | EBL | 76 | E | 0.90 | 68 |
| | WBL | 58 | E | 0.88 | 93 |
| Major MacKenzie / | WBT | 87 | F | 1.07 | 290 |
| Dufferin | NBL | 246 | F | 1.39 | 131 |
| | SBT | 101 | F | 1.10 | 284 |
| | Overall | 76 | E | 1.08 | - |
| | EBL | 186 | F | 1.18 | 110 |
| | EBR | 57 | E | 0.64 | 81 |
| Kirby / Kaala | WBL | 384 | F | 1.76 | 474 |
| Kirby / Keele | NBL | 323 | F | 1.42 | 42 |
| | SBT | 130 | F | 1.19 | 391 |
| | Overall | 139 | F | 1.43 | - |
| | WBT | 95 | F | 1.09 | 255 |
| | NBL | 143 | F | 1.18 | 204 |
| Kirby / Dufferin | SBT | 78 | E | 1.01 | 177 |
| • | SBR | 63 | E | 0.84 | 143 |
| | Overall | 65 | Е | 1.03 | - |
| | | | | | |

To improve network performance issues identified from the 2041 Do-Nothing scenario, localized intersection improvements using Transportation System Management (TSM) techniques should be considered (e.g. traffic signal improvements, channelization, etc.). Additionally, Transportation Demand Management (TDM) and Smart Commute strategies (e.g. parking fees, carpool priority, discounted transit passes, bike racks, etc.) to promote and increase walking, cycling and transit use should be evaluated to estimate potential mode shift for the study area. In combination with traditional solutions such as building new roadways and widening existing roadways, these techniques and strategies will be included as possible solutions developed for the Alternatives to the Undertaking.



7. PROBLEMS / OPPORTUNITIES

Defining problems and opportunities is a key step that sets the stage for the range and types of alternatives to be considered and provides a baseline for the transportation evaluation criteria (or factors) to be used to select among alternatives. The following transportation problems/opportunities have been identified in the area:

- Future land-use change surrounding Teston Road from primarily rural to residential and mixed use will considerably increase future travel demand within the Study Area. The screenline analysis indicates that AM peak hour travel demand along arterial roads is projected to increase from 2016 to 2041 on average by 66% (SL 1, 2 and 3) and 72% (SL 4 and 5), respectively, in the westbound and southbound directions under the Do-Nothing scenario (i.e. 2041 TMP Network excluding a Teston Road Extension between Keele and Dufferin), with even higher increases under the 2041 TMP Network scenario (including GTA West).
- The estimated 2041 AM peak hour traffic volumes in the westbound direction between Keele Street and Dufferin Street exceed available capacity under the Do-Nothing scenario. The estimated 2041 AM peak hour traffic volumes in the southbound direction between Kirby Road and Major MacKenzie Drive generally exceed available capacity under the Do-Nothing scenario.
- The discontinuity on Teston Road between Keele Street and Dufferin Street is a
 barrier to local and regional east/west trips and adds traffic load to parallel east/west
 alternatives routes such as the already congested Major Mackenzie Drive and Kirby
 Road. AM peak hour over-capacity conditions are noted for Teston Road, Kirby
 Road and Major MacKenzie Drive at the Keele Street and Dufferin Streets
 intersections for movements.
- There is limited east-west accessibility along the Teston Road corridor to access existing and planned Highway 400 interchanges (i.e. Teston Road Interchange, Major Mackenzie Drive Interchange and Kirby Road Interchange). Current levels of congestion and out-of-way travel faced by commuters would be exacerbated by increasing traffic demands. While it is anticipated that links within the vicinity of Highway 400 would have greater capacity due to proposed future widenings, east of this facility, the same capacity is not provided which produces bottlenecks at major intersections.
- The discontinuity on Teston Road between Keele Street and Dufferin Street is a barrier to residents from better access to amenities (e.g. schools, parks, recreational facilities, emergency and other public services, etc.).
- The discontinuity on Teston Road between Keele Street and Dufferin Street results in longer trip distances which may increase greenhouse gas emissions and have negative impacts on climate change.



- The area of Teston Road between Keele Street and Dufferin Street is identified in York Region's TMP as having a separated cycling facility by 2041. The current network requires significant out-of-way travel by cyclists and pedestrians, channeling additional cycling and pedestrian traffic to Keele Street or Dufferin Street to use Kirby Road or Major Mackenzie Drive to cross this barrier.
- Westbound AM peak hour transit ridership and Transit Mode Share are both projected to increase significantly within the study area between 2016 and 2041 (e.g. at SL2 transit ridership to increase by 741% and Transit Modal Share from 3% to 13% for the Do Nothing Scenario). While the above is a very significant increase the opportunity may exist to further increase transit ridership and Transit Mode Share within the study area.
- Teston Road between Keele Street and Dufferin Street is identified in York Region's 2016 TMP to be served by frequent transit service by the year 2041. Currently, transit is only available on Teston Road in four short sections at Jane Street (Route 20), Keele Street (Route 107), Thornhill Woods (Route 23) and Elgin Mills (Route 80). The discontinuity on Teston Road between Keele Street and Dufferin Street is a barrier to increased transit service and ridership along this corridor.
- Based on the discussion with the Deputy Fire Chief, City of Vaughan Fire and Rescue Service, there is a need for another fire station on the west side of the study area. The location of the station depends on the findings of the IEA.



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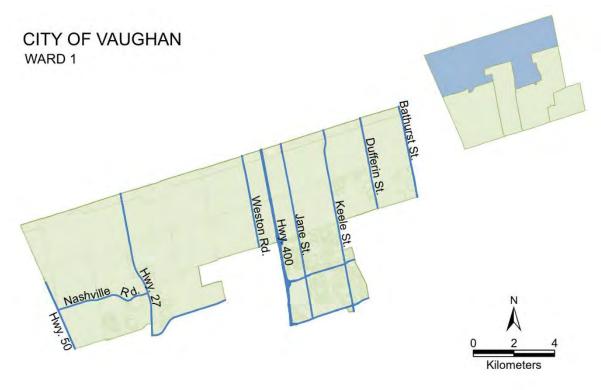
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Appendix A: 2016 Transportation Tomorrow Survey (TTS) for City of Vaughan





WARD 1

| VVAILD I | | | | | | | | | | | | | | | | | | |
|------------|-------|------------|-----------|-----|-----|-----------|-------|--------|------|----------|------------|-----------|----|---------|---------|-----------|----------|-----------|
| | | | | | | HOU | SEHOL | .D CHA | RACT | ERISTI | CS | | | | | | | |
| | Dv | welling Ty | /pe | | Но | usehold S | Size | | 1 | Number o | f Availabl | e Vehicle | !S | | House | ehold Ave | erages | |
| Households | House | Townhouse | Apartment | 1 | 2 | æ | 4 | 2+ | 0 | 1 | 2 | 3 | 4+ | Persons | Workers | Drivers | Vehicles | Trips/Day |
| 20,400 | 74% | 12% | 13% | 11% | 21% | 19% | 28% | 20% | 4% | 22% | 49% | 17% | 8% | 3.3 | 2.0 | 2.3 | 2.0 | 6.3 |

| | | | | | | POP | ULATIC | ON CHA | ARACT | ERISTICS | | | | | | |
|------------|-----|-----|------|------|------|-----|--------|-------------------------------------|------------------------|------------|--------------|--------------|------------|---------|----------|-----------------|
| | | | | Age | | | | | er | | Emp | ployment T | уре | | | |
| Population | | 2 | 5 | 2 | 4 | | ian | Daily Trips per Person (age 11+) | Work Trips p Worker | Population | Full Time | Part Time | At Home | Student | Licensed | Transit Pass |
| | -10 | 1-1 | 16-2 | 26-4 | 46-6 | 2+ | Median | Per | aily | | | ١ | Male | | | |
| | 0 | 1 | 1 | 2 | 4 | 9 | 2 | | Q | 33,600 | 49% | 7% | 4% | 25% | 73% | 10% |
| | | | | | | | | | | | | Fe | emale | | | |
| 68,300 | 13% | 7% | 16% | 26% | 28% | 10% | 37.7 | 2.2 | 0.74 | 34,700 | 38% | 11% | 3% | 25% | 66% | 13% |

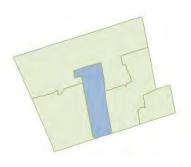
| | | | | | | TRIPS M | ADE BY I | RESIDEN | TS OF CI | TY OF V | AUGHAN | WARD | 1 | | | | |
|---|----------------|---------|-----------|------|--------|---------|----------|---------|----------|---------|-------------|-----------------|-------|--------|--------------|------------|-------------|
| ĺ | Time | | 0/ | | Trip I | Purpose | | | | Mode o | of Travel | | | N | ∕ledian Trip | Length (km |) |
| | Time Period | Trips | % 24hr | HB-W | HB-S | HB-D | N-HB | Driver | Pass. | Transit | GO Train | Walk & Cycle | Other | Driver | Pass. | Transit | GO Train |
| ĺ | 6-9 AM | 34,900 | 27% | 50% | 21% | 20% | 9% | 66% | 13% | 4% | 4% | 5% | 8% | 9.9 | 2.7 | 21.6 | 25.4 |
| ſ | 24 Hrs | 129.300 | | 38% | 13% | 35% | 13% | 71% | 14% | 5% | 2% | 4% | 5% | 8.4 | 4.7 | 13.3 | 25.4 |

| | | | TRI | PS MAD | E TO CI | TY OF V | AUGHAN | I WARE |) 1 BY F | RESIDEN | TS OF TH | IE TTS AI | REA | | | |
|--------|--------|------------|------|--------|---------|---------|--------|--------|----------|-------------|-----------------|-----------|--------|-------------|------------|-------------|
| Time | | % 24 | | Trip P | urpose | | | | Mode o | of Travel | | | N | 1edian Trip | Length (km | 1) |
| Period | Trips | % 24 hr | Work | School | Home | Other | Driver | Pass. | Transit | GO Train | Walk & Cycle | Other | Driver | Pass. | Transit | GO Train |
| 6-9 AM | 17,200 | 18.6% | 40% | 24% | 10% | 26% | 67% | 17% | 2% | * | 9% | 4% | 6.8 | 2.0 | 6.8 | * |
| 24 Hrs | 92,400 | | 12% | 5% | 60% | 23% | 71% | 16% | 3% | 2% | 5% | 4% | 8.0 | 3.8 | 11.0 | 25.4 |



CITY OF VAUGHAN WARD 3







WARD 3

| | WARD 3 | | | | | | | | | | | | | | | | | | |
|---|------------|-------|------------|-----------|----|-----|-----------|-------|--------|------|----------|------------|-----------|----|---------|---------|-----------|----------|-----------|
| I | | | | | | | HOU | SEHOL | .D CHA | RACT | ERISTI | CS | | | | | | | |
| ſ | | D۱ | welling Ty | /ре | | Но | usehold S | Size | | ١ | Number o | f Availabl | e Vehicle | S | | House | ehold Ave | erages | |
| | Households | House | Townhouse | Apartment | 1 | 2 | 3 | 4 | 5+ | 0 | 1 | 2 | 3 | 4+ | Persons | Workers | Drivers | Vehicles | Trips/Day |
| | 18,100 | 86% | 13% | 2% | 7% | 23% | 19% | 30% | 21% | 0% | 22% | 55% | 14% | 8% | 3.4 | 1.9 | 2.4 | 2.1 | 6.4 |

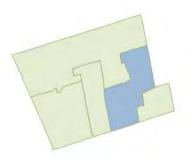
| I | | | | | | | POP | ULATIO | N CH | ARACT | ERISTICS | | | | | | |
|---|------------|-----|-----|-----|-----|-----|-----|--------|------------------------------------|-------------------------|------------|--------------|--------------|------------|---------|----------|-----------------|
| ı | | | | | Age | | | | | _ | | Emp | ployment T | уре | | | |
| | Population | | 2 | 5 | 5 | 4 | | ian | Daily Trips per erson (age 11+) | work Trips pe Worker | Population | Full Time | Part Time | At Home | Student | Licensed | Transit Pass |
| | | -10 | 1-1 | 6-2 | 6-4 | 9-9 | 2+ | Median | Der | Daily | | | 1 | Male | | | |
| | | 0 | 1 | 1 | 7 | 4 | 9 | 2 | | Э | 30,400 | 47% | 5% | 4% | 26% | 70% | 8% |
| | | | | | , | | | | | | | | Fe | emale | • | • | |
| ĺ | 61,800 | 15% | 7% | 12% | 28% | 26% | 12% | 39.1 | 2.2 | 0.79 | 31,400 | 37% | 10% | 3% | 25% | 66% | 11% |

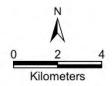
| ١ | | | | | | TRIPS M | ADE BY I | RESIDEN | TS OF CI | TY OF V | AUGHAN | WARD | 3 | | | | |
|---|----------------|---------|-----------|------|--------|---------|----------|---------|----------|---------|-------------|-----------------|-------|--------|--------------|------------|-------------|
| ĺ | Time | | 0/ | | Trip I | Purpose | | | | Mode o | of Travel | | | N | ∕ledian Trip | Length (km | 1) |
| | Time Period | Trips | % 24hr | HB-W | HB-S | HB-D | N-HB | Driver | Pass. | Transit | GO Train | Walk & Cycle | Other | Driver | Pass. | Transit | GO Train |
| ĺ | 6-9 AM | 32,700 | 28.2% | 47% | 20% | 22% | 11% | 69% | 13% | 6% | 2% | 7% | 2% | 8.5 | 3.4 | 20.2 | 25.2 |
| ſ | 24 Hrs | 115.900 | | 39% | 13% | 35% | 13% | 73% | 14% | 5% | 1% | 6% | 2% | 6.9 | 3.9 | 19.3 | 25.2 |

| | | | TRII | PS MAD | E TO CI | TY OF V | AUGHAI | N WARI | D 3 BY | RESIDEN | TS OF TH | HE TTS A | REA | | | | | |
|--------|---------|------------|------|--------|---------|---------|----------------|--------|---------|-------------|-----------------|----------|--------|-------------------------|---------|-------------|--|--|
| Time | | % 24 | | Trip P | urpose | | Mode of Travel | | | | | | | Median Trip Length (km) | | | | |
| Period | Trips | % 24 hr | Work | School | Home | Other | Driver | Pass. | Transit | GO Train | Walk & Cycle | Other | Driver | Pass. | Transit | GO Train | | |
| 6-9 AM | 33,100 | 26.1% | 58% | 15% | 5% | 22% | 74% | 12% | 3% | * | 7% | 3% | 8.9 | 2.8 | 5.5 | * | | |
| 24 Hrs | 127,000 | | 25% | 4% | 39% | 31% | 75% | 14% | 4% | 1% | 5% | 1% | 6.8 | 4.2 | 11.3 | 25.2 | | |

CITY OF VAUGHAN WARD 4







WARD 4

| | WARD 4 | | | | | | | | | | | | | | | | | | |
|---|------------|-------|------------|-----------|----------------|-----|-----|-------|------------------------------|------|--------|-----|-----|--------------------|---------|---------|---------|----------|-----------|
| ı | | | | | | | HOU | SEHOL | .D CHA | RACT | ERISTI | CS | | | | | | | |
| I | | D۱ | welling Ty | /ре | Household Size | | | | Number of Available Vehicles | | | | | Household Averages | | | | | |
| | Households | esnoH | Townhouse | Apartment | 1 | 2 | ĸ | 4 | 5+ | 0 | 1 | 2 | 3 | 4+ | Persons | Workers | Drivers | Vehicles | Trips/Day |
| I | 15,700 | 78% | 16% | 6% | 9% | 19% | 22% | 30% | 20% | 2% | 23% | 62% | 10% | 3% | 3.4 | 2.0 | 2.2 | 1.9 | 6.5 |

| | | | | | | POP | ULATIO | ON CH | ARACT | ERISTICS | | | | | | |
|------------|-----|-----|-----|-----|-----|-----|--------|------------------------------------|-------------------------|------------|--------------|--------------|------------|---------|----------|-----------------|
| | | | | Age | | | | | ŗ. | | Emp | ployment T | уре | | | |
| Population | | 2 | 2 | 5 | 4 | | an | Daily Trips per erson (age 11+) | Work Trips pe Worker | Population | Full Time | Part Time | At Home | Student | Licensed | Transit Pass |
| | -10 | 1-1 | 6-2 | 6-4 | 9-9 | 65+ | Median | Da | Daily | | | 1 | Male | | | |
| | 0 | 1 | 1 | 2 | 4 | 9 | 2 | | | 26,100 | 48% | 5% | 5% | 28% | 66% | 14% |
| | | | | | | | | | | | | Fe | emale | | | |
| 53,400 | 19% | 8% | 10% | 32% | 24% | 8% | 36.6 | 2.4 | 0.77 | 27,300 | 37% | 7% | 5% | 26% | 61% | 15% |

| | | | | | TRIPS M | ADE BY I | RESIDEN' | TS OF CI | TY OF V | AUGHAN | WARD | 4 | | | | | | | | |
|--------|---------|-------|------|--------|---------|----------|----------|----------------|---------|-------------|-----------------|-------|--------|-------|-------------------------|-------------|--|--|--|--|
| Time | | % | | Trip I | Purpose | | | Mode of Travel | | | | | | | Median Trip Length (km) | | | | | |
| Period | Trips | 24hr | HB-W | HB-S | HB-D | N-HB | Driver | Pass. | Transit | GO Train | Walk & Cycle | Other | Driver | Pass. | Transit | GO Train | | | | |
| 6-9 AM | 29,800 | 29.2% | 47% | 18% | 24% | 11% | 65% | 12% | 8% | 5% | 7% | 3% | 8.2 | 3.6 | 19.6 | 23.6 | | | | |
| 24 Hrs | 101,900 | | 36% | 13% | 36% | 15% | 70% | 13% | 7% | 3% | 5% | 2% | 7.0 | 4.6 | 19.1 | 23.6 | | | | |

| | | | TRII | PS MAD | E TO CI | TY OF V | AUGHAI | N WARI | D4 BY | RESIDEN | TS OF TH | HE TTS A | REA | | | | | |
|--------|---------|------------|------|--------|---------|---------|----------------|--------|---------|-------------|-----------------|----------|--------|-------------------------|---------|-------------|--|--|
| Time | | % 24 | | Trip P | urpose | | Mode of Travel | | | | | | | Median Trip Length (km) | | | | |
| Period | Trips | % 24 hr | Work | School | Home | Other | Driver | Pass. | Transit | GO Train | Walk & Cycle | Other | Driver | Pass. | Transit | GO Train | | |
| 6-9 AM | 62,000 | 35.5% | 79% | 5% | 3% | 13% | 83% | 9% | 4% | * | 3% | 1% | 12.7 | 6.7 | 8.8 | * | | |
| 24 Hrs | 174,700 | | 45% | 2% | 25% | 28% | 78% | 12% | 5% | 1% | 3% | 1% | 9.5 | 6.2 | 10.2 | 23.5 | | |

Appendix B: Existing Traffic Data



AADT Midblocks Report

| | | | | | | | | | | _ |
|--|-------|--------------|--------------|--------|-------|---------------|----------------|----------------|---------------|---------------|
| Description | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | 2017 | 2018 | 2019 |
| Bathurst Street blwn Elgin Mills Road West/Teston Road & Woodland Acres Crescent | 28361 | | 29911 | | 31666 | | 32811 | | 33838 | |
| Bathurst Street btwn Gamble Road & Hearthside Avenue | 21108 | | 22217 | | 23516 | 23357 | | 25552 | | 24518 |
| Bathurst Street btwn Major Mackenzie Drive West & Mill Street/Queen Filomena Avenue | | | | 39375 | | | 40474 | | 38877 | |
| Bathurst Street btwn McCallum Drive/Valley Vista Drive & Major Mackenzie Drive West | 34204 | | 34548 | | 36622 | 36051 | | 38887 | | 37672 |
| Bathurst Street btwn Oxford Street/Lady Dolores Avenue & Elgin Mills Road West/Teston Road | 31031 | | 31298 | | 33121 | 33002 | | 35610 | | 34478 |
| Carrville Road btwn Bathurst Street & Okanagan Drive | 26971 | | 27523 | | 29099 | 29305 | | 32260 | | 29939 |
| Carrville Road btwn Plaisance Road & Carville Avenue @ Hillcrest Mall | 25445 | | 26162 | | 27710 | | 25456 | | 27735 | |
| Dufferin Street btwn Athabasca Drive & Kirby Road | 10774 | | 10859 | | 11472 | | 11568 | | 12051 | |
| Dufferin Street btwn District Avenue/Marc Santi Boulevard & Maurier Boulevard | 19075 | | 19850 | | 20934 | 21012 | | 34909 | | 29671 |
| Dufferin Street btwn Hunterwood Chase & Beakes Crescent | 12513 | | 12894 | | 11435 | 11659 | | 15193 | | 14430 |
| Dufferin Street blwn Kirby Road & King Vaughan Road Dufferin Street blwn Sir Benson Drive & Teston Road | 8821 | | 9055 | 22945 | 9543 | 9759 | 43297 | 11841 29572 | 18553 | 9491 |
| Elgin Mills Road West btwn Bathurst Street & Hiram Road | | 16783 | | 18696 | | 17819 | 43297 | 19528 | 16333 | 18703 |
| Elgin Mills Road West blwn Creekview Avenue & Yonge Street | 19635 | 10763 | 20695 | 10090 | 21882 | 17019 | 21777 | 19326 | 22228 | 10703 |
| Jane Street blwn Ahmadiyya Avenue & Teston Road | 10330 | | 11084 | | 11707 | | 11760 | | 12374 | |
| Jane Street btwn Avro Road & Major Mackenzie Drive West | 24226 | | 24881 | | 26270 | | 25892 | | 27493 | |
| Jane Street btwn Kirby Road & King Vaughan Road | | 5321 | | 5561 | | | 6601 | | 6888 | |
| Jane Street btwn Major Mackenzie Drive West & Roseheath Drive/Grand Valley Boulevard | | | | 37466 | | 37173 | | 37798 | | 36093 |
| Jane Street blwn Rutherford Road & Auto Vaughan Drive | 24932 | | 25395 | | 26781 | 26320 | | 28838 | | 27619 |
| Jane Street btwn Teston Road & Kirby Road | 6278 | | 6111 | | 6439 | 6542 | | 7205 | | 6837 |
| Keele Street btwn Dina Road & Cromwell Road/Fieldgate Drive | | | | | | | | 19151 | | |
| Keele Street btwn Keele Street @ Maple Health Centre & Drummond Drive | 16086 | | 17094 | | 18100 | | 18227 | | 19357 | |
| Keele Street blwn Kirby Road & Maloy Street | | 8243 | | 8820 | | | 13577 | | 14032 | |
| Keele Street btwn Major Mackenzie Drive West & Railway Street/Killian Road | 19681 | | 19617 | | 20746 | 20649 | | 23042 | | 21957 |
| Keele Street btwn Naylon Street & Church St. Mid Block Pedestrian Crossing | | 18025 | | 18884 | | | 19259 | | 20095 | |
| Keele Street btwn Teston Road & Peak Point Boulevard | | | | 13107 | | 13524 | | 15115 | | 15234 |
| King Vaughan Rd btwn Highway 400 & Jane Street | | | | | | | 3142 | | 322 | |
| King Vaughan Road btwn Bathurst Street & Dufferin Street | | | | | | | | | 8856 | |
| King Vaughan Road blwn Dufferin Street & Keele Street | | | | | | | | | 8791 | |
| King Vaughan Road btwn Highway 400 & Weston Road | | | | | | | | | 577 | |
| King Vaughan Road btwn Jane Street & Stallions Court | | | | | | | | | 5035 | |
| King Vaughan Road btwn Keele Street & Stallions Court | | | | | | | | | 5042 | |
| King Vaughan Road btwn Pine Valley Drive & Weston Road | | | | | | | 0070 | | 1248 | |
| Kirby Rd S btwn Highway 400 & Jane St Kirby Rd S btwn Jane St & Keele St | | 3787 | | | | | 2878 | | \vdash | |
| Major Mackenzie Drive West btwn Atkinson Street & Yonge Street | | 3/6/ | | 27887 | | 27238 | | 30646 | \vdash | 28438 |
| Major Mackenzie Drive West btwn Exit 35 & Jane Street | | | | 54409 | | 54452 | 47736 | 62966 | 63409 | 63533 |
| Major Mackenzie Drive West btwn Fortinos / Longos Entrance & Melville Avenue | | 22047 | | 42471 | | | 51879 | | 58053 | |
| Major Mackenzie Drive West btwn Ilan Ramon Boulevard & Bathurst Street | | | | | | | 37082 | | | |
| Major Mackenzie Drive West btwn Jutland Street & Weston Road | | | | | | | | | | 34703 |
| Major Mackenzie Drive West btwn Keele Street & Richmond Street | 30402 | | 31222 | | 32936 | 32899 | | 37279 | | 34336 |
| Major Mackenzie Drive West btwn Pine Valley Drive & Woodend Place | 17389 | | 17821 | 20260 | 18798 | 18703 | | 21067 | | 21257 |
| Major Mackenzie Drive West btwn Sir Benson Drive & Thomas Cook Avenue | 31675 | | 31522 | | 32620 | | 31350 | | 35176 | |
| Major Mackenzie Drive West btwn Vellore Woods Boulevard/Cityview Boulevard & Exit 35/GO Carpool Lot - Hwy 400 & Major Mackenzie Drive West | 34293 | | 35916 | | 37815 | 37370 | 36307 | 42569 | 39755 | 43802 |
| Pine Valley Drive btwn Major Mackenzie Drive West & Teston Road | 1932 | | 2051 | | 2169 | | 2181 | | 2287 | |
| Pine Valley Drive btwn Rutherford Road & Davos Road | | 1538 | | 1619 | | 1658 | | 1792 | | 1713 |
| Rutherford Road btwn Exit 33 & Sweetriver Boulevard | | 60948 | | | | 57961 | 54017 | 65129 | 61385 | 61554 |
| Rutherford Road btwn Fossil Hill Road & Rutherford Road @ Rutherford Road Plaza | | 40807 | | 43928 | | 42023 | | 42465 | | 45837 |
| Rutherford Road btwn Ilan Ramon Boulevard & Bathurst Street | | | | | | | 28791 | | | |
| Rutherford Road btwn Jacob Keffer Parkway & Barrhill Road/Westburne Drive | 41805 | | 42292 | | 44596 | 44439 | | 39229 | | 37892 |
| Rutherford Road btwn Jane Street & Rutherford Road @ Southwest Yard | | | | | | | | | | 47554 |
| Rutherford Road btwn Julliard Drive & Jane Street | | | | 57205 | | 57589 | | 64858 | | 60253 |
| Rutherford Road btwn Melville Avenue/Creditstone Road & Rotational Dr. | | | | | | | | | | 53283 |
| Rutherford Road btwn Sherwood Park Drive & Wedgewood Place | 47668 | | 46421 | | 48847 | | 45938 | | 51149 | |
| Rutherford Road btwn Thornhill Woods Drive/Thomas Cook Avenue & Ilan Ramon Boulevard | | | 27563 | | 29037 | | 26951 | | 29998 | |
| Rutherford Road btwn Weston Road & Vellore Woods Boulevard Testes Road btwn Felt 37 & Magazia Cata | 46097 | 3598 | 48036 | | 50600 | 49636 4866 | 47008 24804 | 57405 5669 | 52863 5221 | 52312 5309 |
| Teston Road btwn Exit 37 & Mosque Gate Teston Road btwn Jane Street & Cranston Park Avenue | 5320 | 3598 6790 | 4716 5818 | | 6157 | 4600 | 24804 6164 | 2009 | 5221 6476 | 5309 |
| Teston Road blwn Jane Street & Cranston Park Avenue Teston Road blwn Keele Street & Rodinea Road | 1919 | 0,90 | 1904 | | 2033 | 2125 | 0.104 | 2351 | 0470 | 2222 |
| Teston Road btwn Pine Valley Drive & Weston Road | 1919 | | | 3627 | 2000 | -120 | 3583 | 2001 | 4027 | |
| Teston Road btwn Quail Run Boulevard & Torah Gate | | | | 13838 | | | 15430 | | 16285 | |
| Teston Road blwn Weston Road & Cityriew Boulevard | 3225 | | 2843 | . 5000 | 3022 | 3038 | 3473 | 3499 | 3190 | 3247 |
| Weston Road btwn Kirby Road & King Vaughan Road | 0220 | | | 4020 | | | 6513 | - 700 | 6720 | |
| Weston Road blwn Major Mackenzie Drive West & Retreat Boulevard/Chatfield Drive | 8082 | | 8823 | | 9318 | | 9348 | | 15122 | |
| Weston Road btwn Maria Antonia Road/Hawstone Road & Major Mackenzie Drive West | 16177 | | 16991 | | 17925 | | 17647 | | 18826 | |
| Weston Road blwn Mattucci Court & Kirby Road | .5 | | | 6223 | | 6448 | | 7024 | | 6748 |
| Yonge Street btwn Baif Boulevard/Observatory Lane & Weldrick Road West/Weldrick Road East | 34732 | 37507 | 38317 | 41100 | 40467 | <u> </u> | 43692 | | 39959 | |
| Yonge Street blwn Hopkins Street/Elmwood Avenue & Major Mackenzie Drive West/Major Mackenzie Drive East | 29468 | | 30573 | 33249 | 32362 | 31439 | 35587 | 35936 | 32751 | 33026 |
| Yonge Street btwn Jefferson Sideroad & Stouffville Road | | 23326 | | 24869 | | 23817 | 23644 | 25983 | | 24816 |
| Yonge Street btwn Leonard Street & Private Entrance - LBS Development | 40349 | 45360 | 41771 | 45629 | 44102 | 43226 | 43243 | 47116 | | 45204 |
| · · · · · · · · · · · · · · · · · · · | | | | | | | | | | |

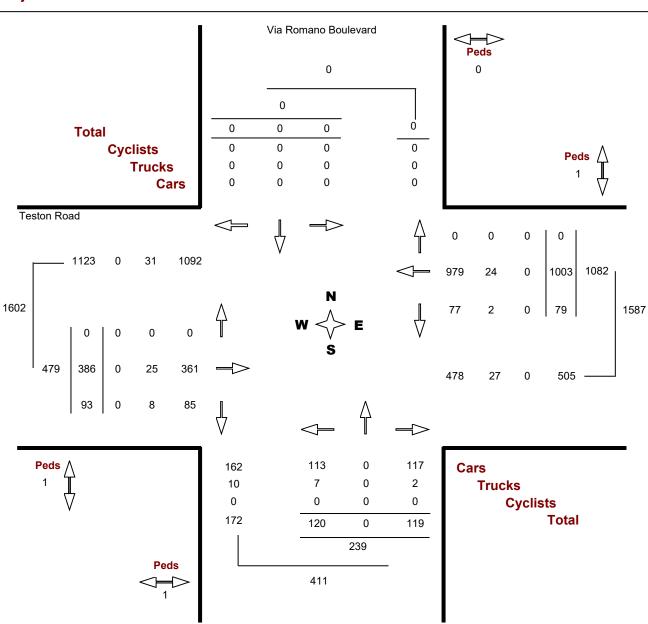


Location...... Teston Road & Via Romano Boulevard GeolD...... 4C3E19E1

Municipality. Vaughan Count Date. Wednesday, 03 October, 2012

Traffic Cont. Traffic signal **Count Period.** 07:00 AM — 09:00 AM

Major Dir.... None **Peak Hour....** 07:30 AM — 08:30 AM



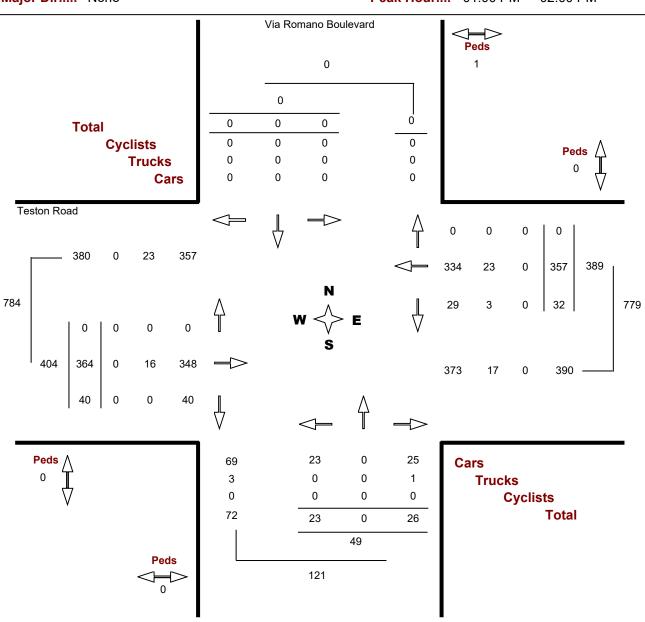


Location...... Teston Road & Via Romano Boulevard GeolD...... 4C3E19E1

Municipality. Vaughan Count Date. Wednesday, 03 October, 2012

Traffic Cont. Traffic signal **Count Period.** 11:00 AM — 02:00 PM

Major Dir.... None **Peak Hour...** 01:00 PM — 02:00 PM



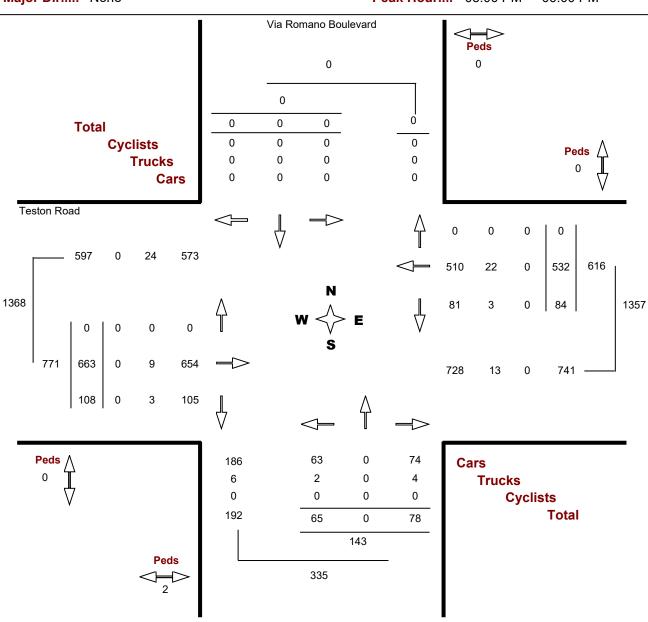


Location...... Teston Road & Via Romano Boulevard GeolD...... 4C3E19E1

Municipality. Vaughan Count Date. Wednesday, 03 October, 2012

Traffic Cont. Traffic signal **Count Period.** 03:00 PM — 06:00 PM

Major Dir.... None **Peak Hour...** 05:00 PM — 06:00 PM





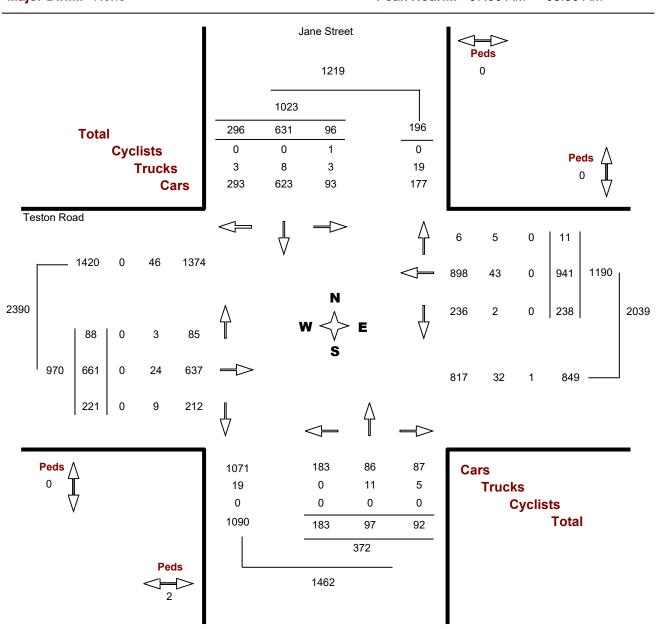
Location...... Teston Road & Jane Street GeolD...... EC354822

Municipality. Vaughan Count Date. Wednesday, 07 December,

2016

Traffic Cont. Traffic signal **Count Period.** 07:00 AM — 09:00 AM

Major Dir.... None **Peak Hour....** 07:30 AM — 08:30 AM





Location...... Teston Road & Jane Street

Municipality. Vaughan

Traffic Cont. Traffic signal

Major Dir..... None

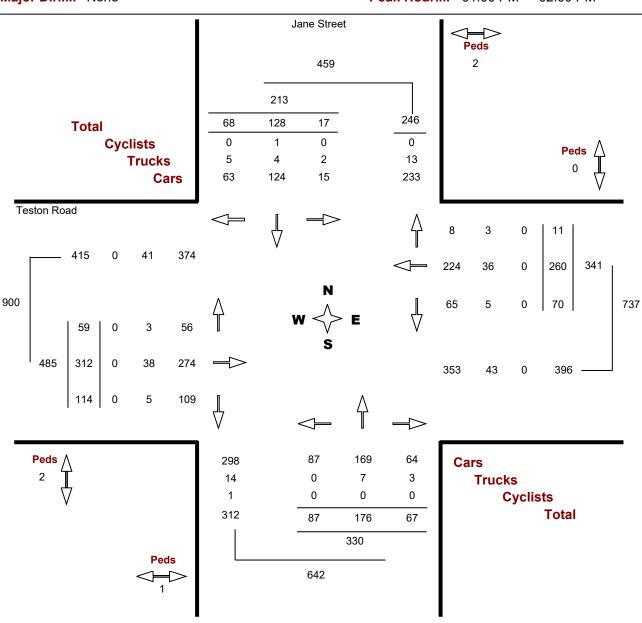
GeolD..... EC354822

Count Date. Wednesday, 07 December,

2016

Count Period. 11:00 AM — 02:00 PM

Peak Hour.... 01:00 PM — 02:00 PM





Location...... Teston Road & Jane Street

GeoID...... EC354822

Municipality. Vaughan

Count Date. Wednesday, 07 December,

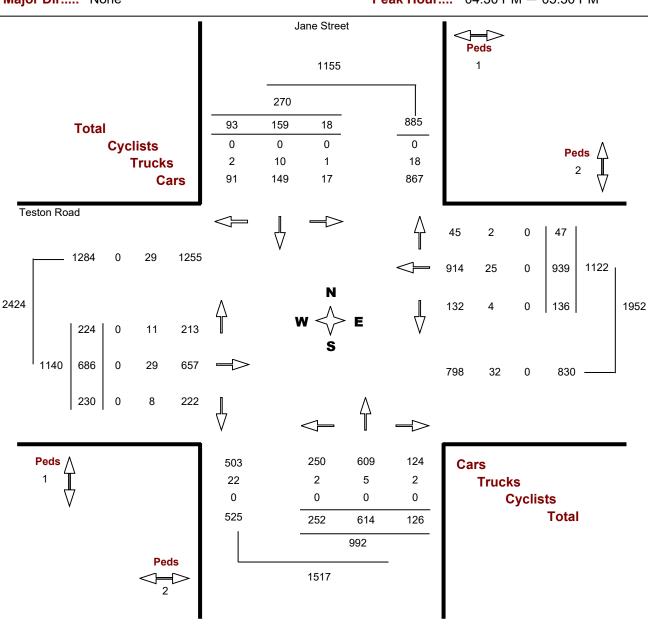
2016

Traffic Cont. Traffic signal

Count Period. 03:00 PM — 06:00 PM

Major Dir..... None

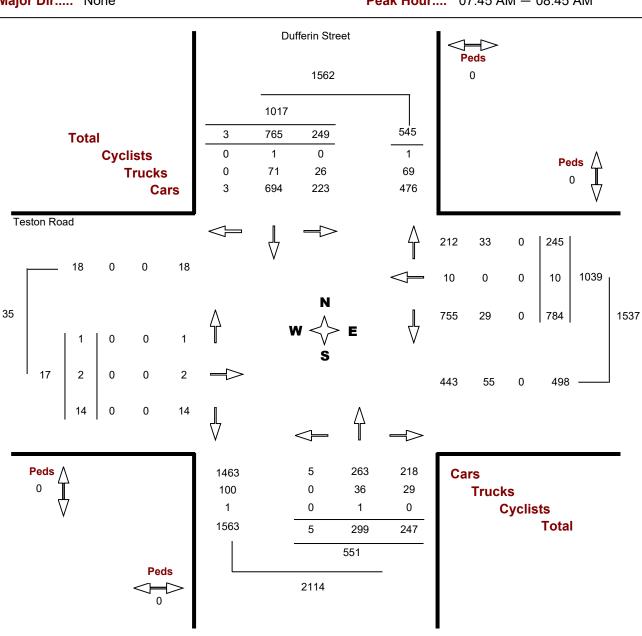
Peak Hour.... 04:30 PM — 05:30 PM





Location...... Teston Road & Dufferin Street GeolD...... 9661E84C

Municipality.VaughanCount Date.Tuesday, 25 June, 2019Traffic Cont.Traffic signalCount Period.07:00 AM — 09:00 AMMajor Dir.....NonePeak Hour....07:45 AM — 08:45 AM





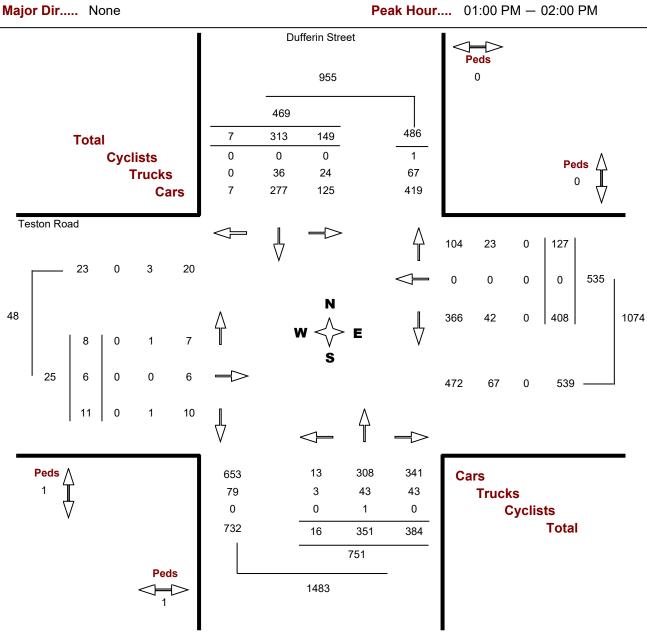
Location...... Teston Road & Dufferin Street GeolD...... 9661E84C

Municipality. Vaughan

Count Date. Tuesday, 25 June, 2019

Traffic Cont. Traffic signal

Count Period. 11:00 AM — 02:00 PM





Location...... Teston Road & Dufferin Street GeolD...... 9661E84C

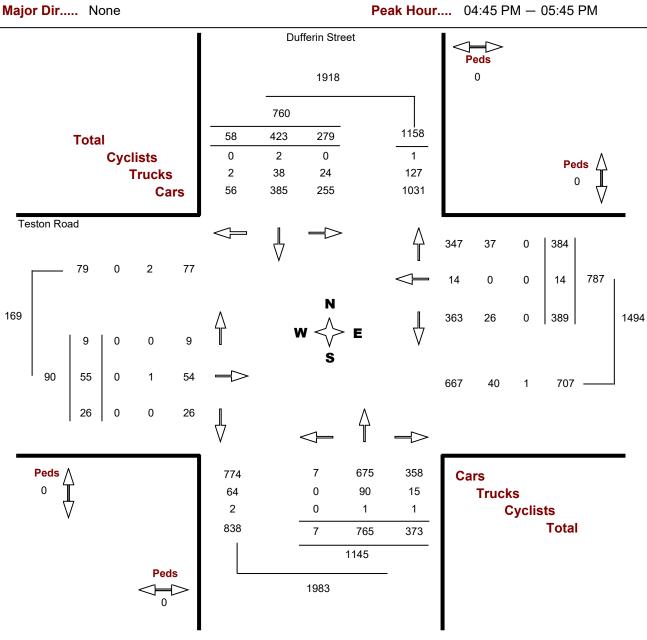
Municipality. Vaughan

Count Date. Tuesday, 25 June, 2019

Traffic Cont. Traffic signal

Count Period. 03:00 PM — 06:00 PM

Major Direct Name (2014 PM) (201



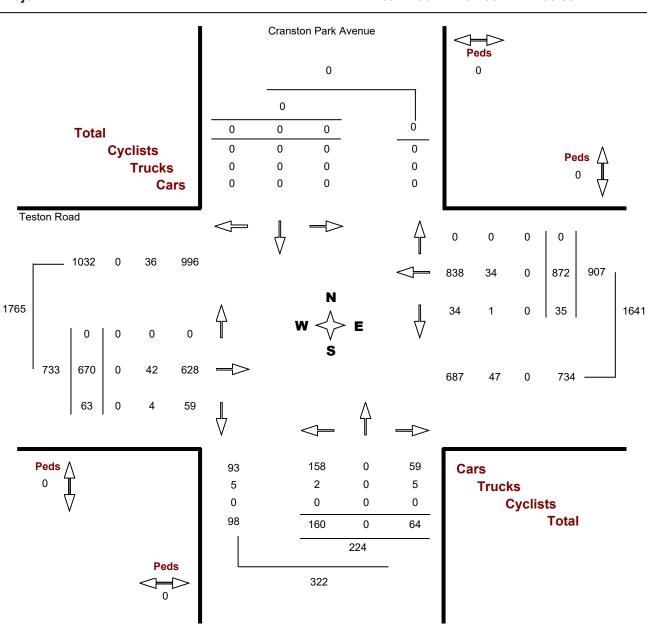


Location...... Teston Road & Cranston Park Avenue GeolD...... A5E0C75C

Municipality. Vaughan Count Date. Tuesday, 16 October, 2012

Traffic Cont. Traffic signal **Count Period.** 07:00 AM — 09:00 AM

Major Dir.... None **Peak Hour....** 07:30 AM — 08:30 AM



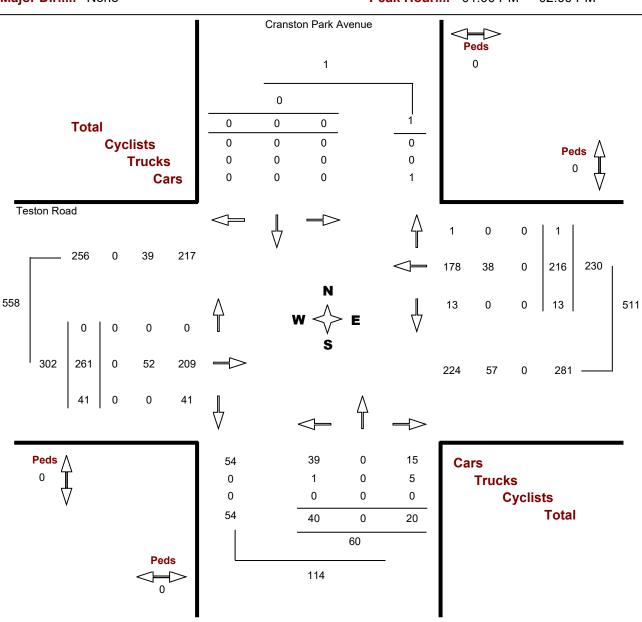


Location...... Teston Road & Cranston Park Avenue GeolD...... A5E0C75C

Municipality. Vaughan Count Date. Tuesday, 16 October, 2012

Traffic Cont. Traffic signal **Count Period.** 11:00 AM — 02:00 PM

Major Dir.... None **Peak Hour....** 01:00 PM — 02:00 PM



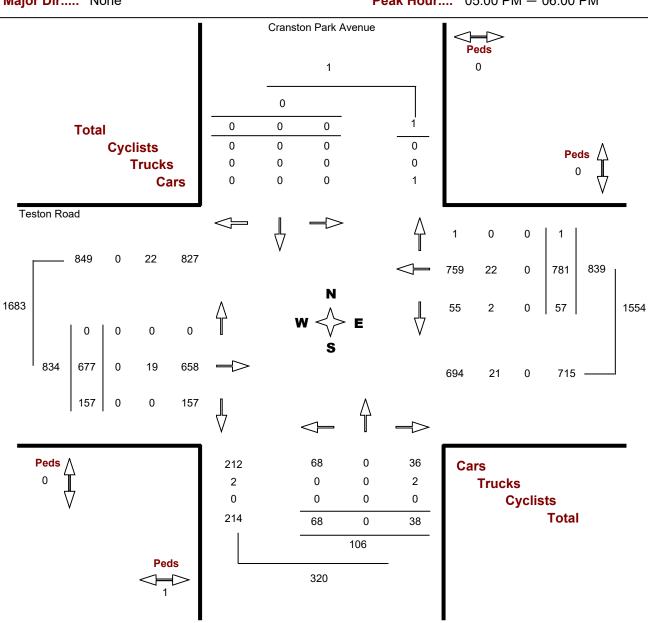


Location...... Teston Road & Cranston Park Avenue GeolD...... A5E0C75C

Municipality. Vaughan Count Date. Tuesday, 16 October, 2012

Traffic Cont. Traffic signal **Count Period.** 03:00 PM — 06:00 PM

Major Dir.... None **Peak Hour....** 05:00 PM — 06:00 PM



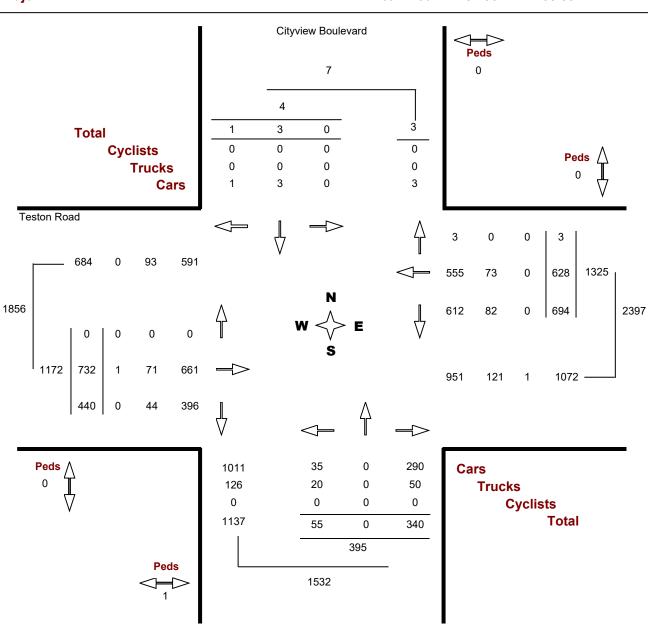


Location...... Teston Road & Cityview Boulevard GeolD...... 531ECD19

Municipality. Vaughan Count Date. Tuesday, 22 October, 2019

Traffic Cont. Traffic signal **Count Period.** 07:00 AM — 09:00 AM

Major Dir.... None **Peak Hour...** 07:30 AM — 08:30 AM



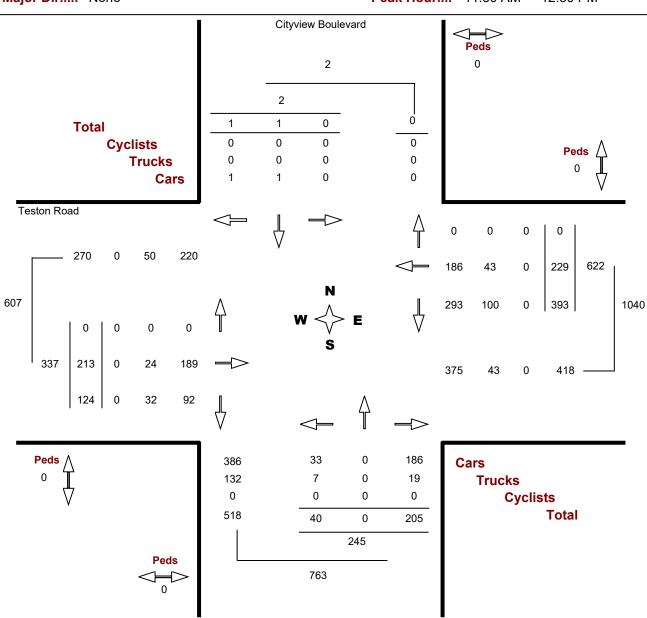


Location...... Teston Road & Cityview Boulevard GeolD...... 531ECD19

Municipality. Vaughan Count Date. Tuesday, 22 October, 2019

Traffic Cont. Traffic signal **Count Period.** 11:00 AM — 02:00 PM

Major Dir.... None **Peak Hour....** 11:30 AM — 12:30 PM



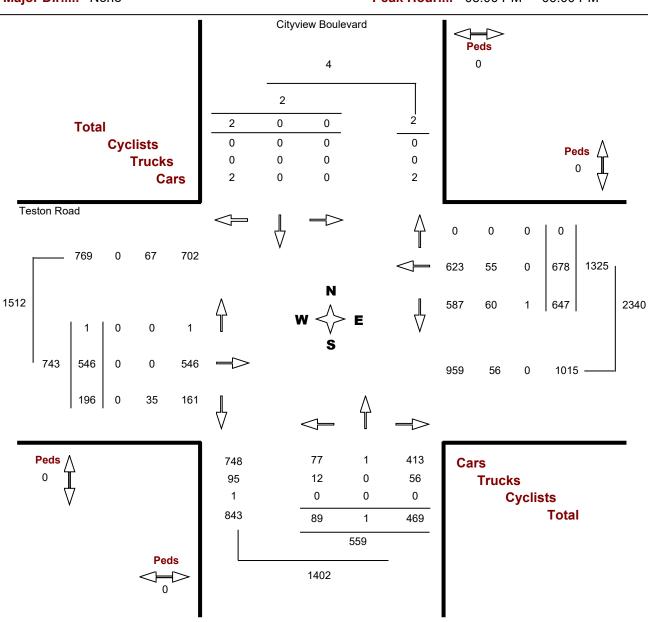


Location...... Teston Road & Cityview Boulevard GeolD...... 531ECD19

Municipality. Vaughan Count Date. Tuesday, 22 October, 2019

Traffic Cont. Traffic signal **Count Period.** 03:00 PM — 06:00 PM

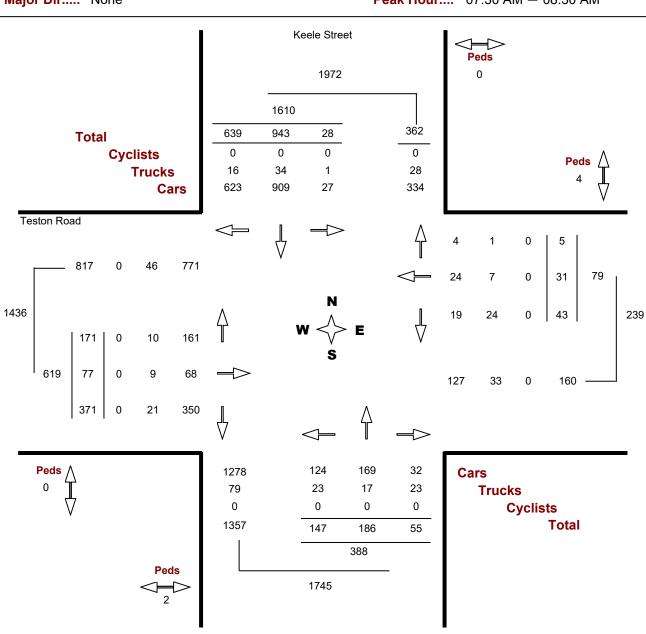
Major Dir.... None **Peak Hour....** 05:00 PM — 06:00 PM





Location...... Keele Street & Teston Road GeolD...... C8F21BE9

Municipality.VaughanCount Date.Tuesday, 14 June, 2011Traffic Cont.Traffic signalCount Period.07:00 AM — 09:00 AMMajor Dir.....NonePeak Hour....07:30 AM — 08:30 AM





Location...... Keele Street & Teston Road GeolD...... C8F21BE9

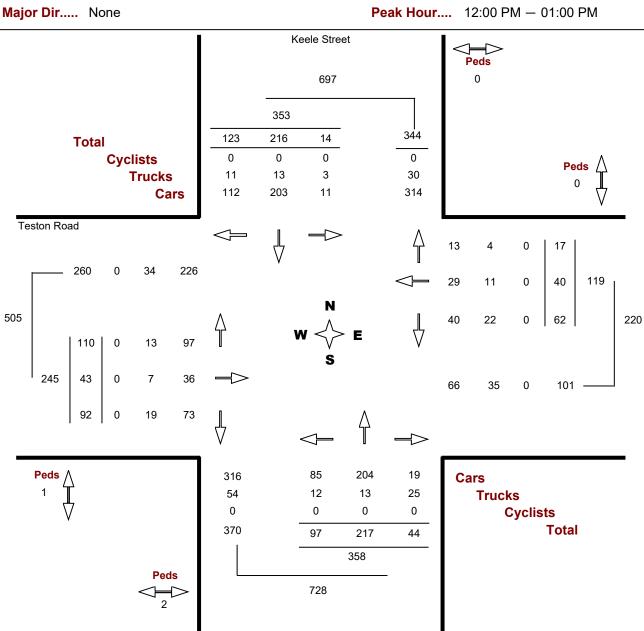
Municipality. Vaughan

Count Date. Tuesday, 14 June, 2011

Traffic Cont. Traffic signal

Count Period. 11:00 AM — 02:00 PM

Major Dir. Name.





Location...... Keele Street & Teston Road GeolD...... C8F21BE9

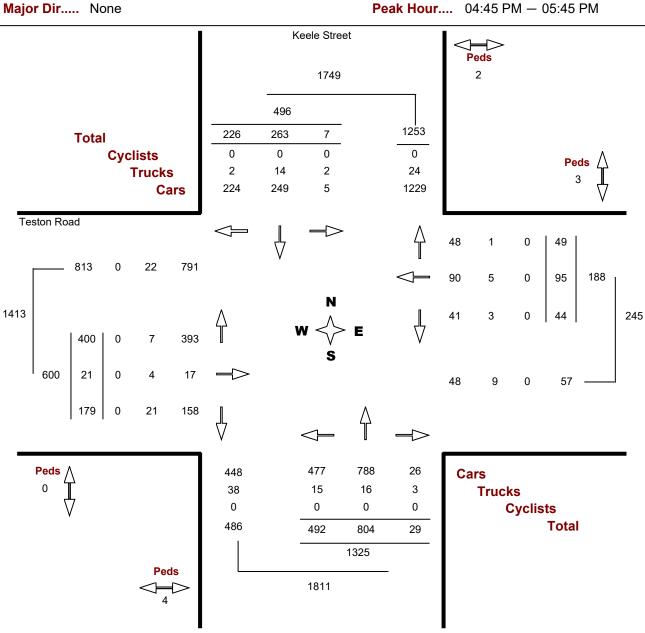
Municipality. Vaughan

Count Date. Tuesday, 14 June, 2011

Traffic Cont. Traffic signal

Count Period. 03:00 PM — 06:00 PM

Major Dir. Name 04:45 PM — 05:45 PM





Location...... Bathurst Street & Elgin Mills Road

West/Teston Road

Municipality. Vaughan

Traffic Cont. Traffic signal

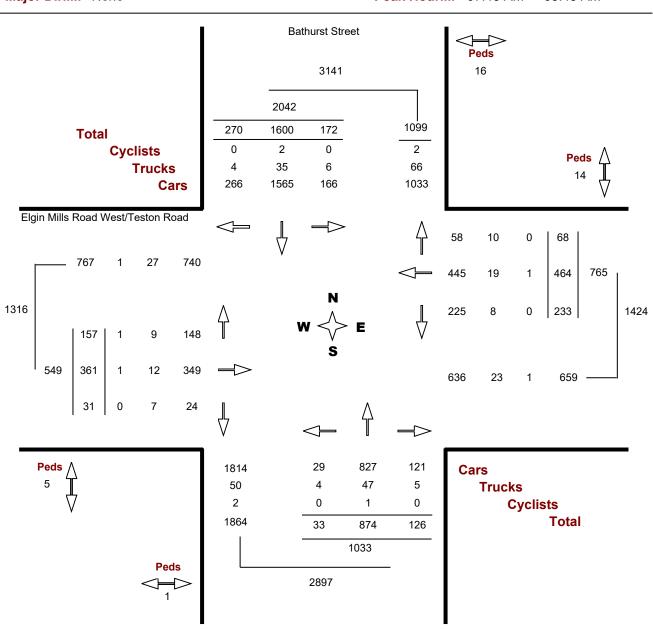
Major Dir..... None

GeoID...... DA6AE471

Count Date. Tuesday, 15 September, 2015

Count Period. 07:00 AM — 09:00 AM

Peak Hour.... 07:45 AM — 08:45 AM





Location...... Bathurst Street & Elgin Mills Road

West/Teston Road

Municipality. Vaughan

Traffic Cont. Traffic signal

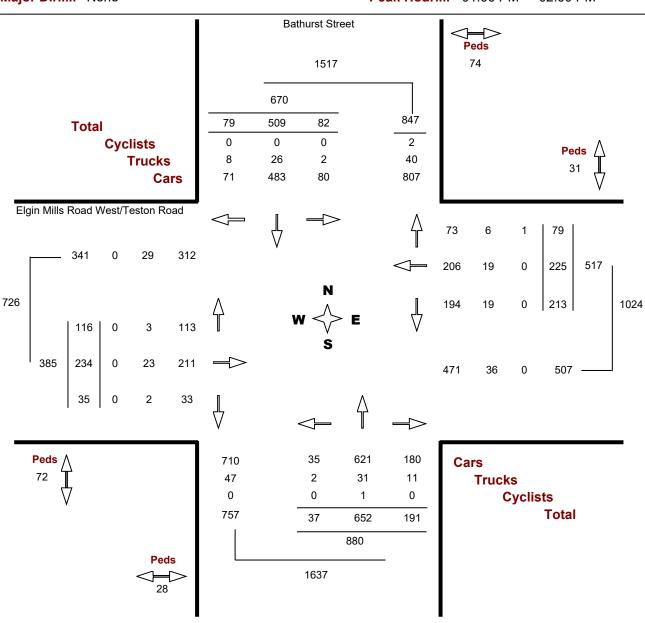
Major Dir..... None

GeolD...... DA6AE471

Count Date. Tuesday, 15 September, 2015

Count Period. 11:00 AM — 02:00 PM

Peak Hour.... 01:00 PM — 02:00 PM





Location...... Bathurst Street & Elgin Mills Road

West/Teston Road

Municipality. Vaughan

Traffic Cont. Traffic signal

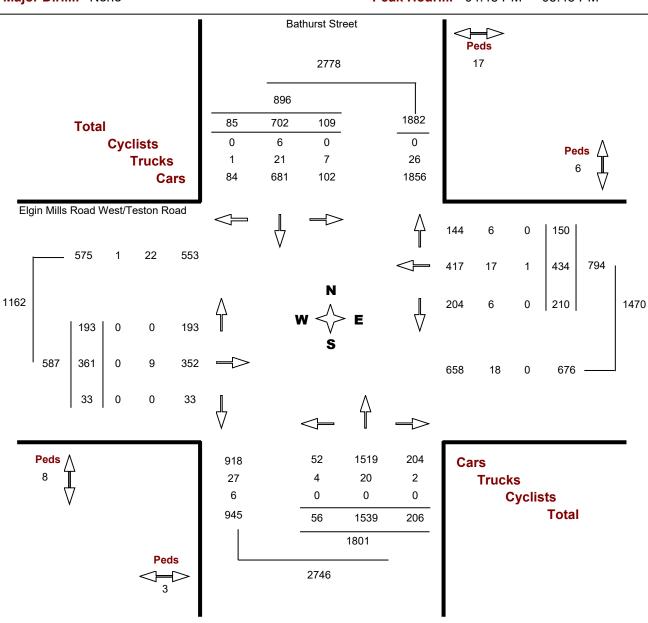
Major Dir..... None

GeolD...... DA6AE471

Count Date. Tuesday, 15 September, 2015

Count Period. 03:00 PM — 06:00 PM

Peak Hour.... 04:45 PM — 05:45 PM





Location...... Jane Street & Kirby Road

Municipality. Vaughan

Traffic Cont. Traffic signal

Major Dir..... None

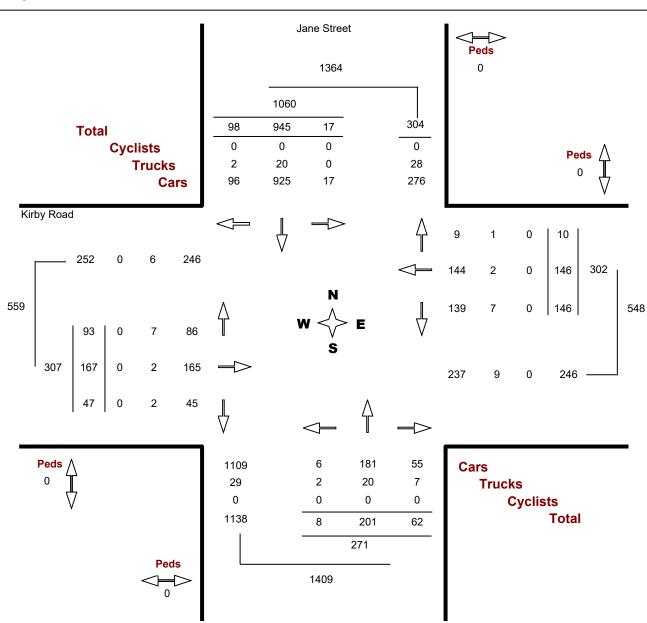
GeoID...... 9674ADF5

Count Date. Thursday, 12 September,

2019

Count Period. 07:00 AM — 09:00 AM

Peak Hour.... 07:30 AM — 08:30 AM





Location...... Jane Street & Kirby Road

Municipality. Vaughan

Traffic Cont. Traffic signal

Major Dir..... None

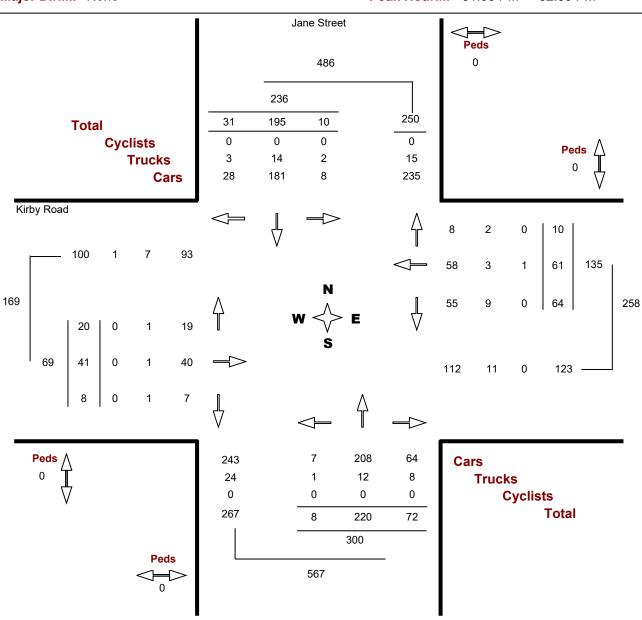
GeoID...... 9674ADF5

Count Date. Thursday, 12 September,

2019

Count Period. 11:00 AM — 02:00 PM

Peak Hour.... 01:00 PM — 02:00 PM





Location...... Jane Street & Kirby Road

Municipality. Vaughan

Traffic Cont. Traffic signal

Major Dir..... None

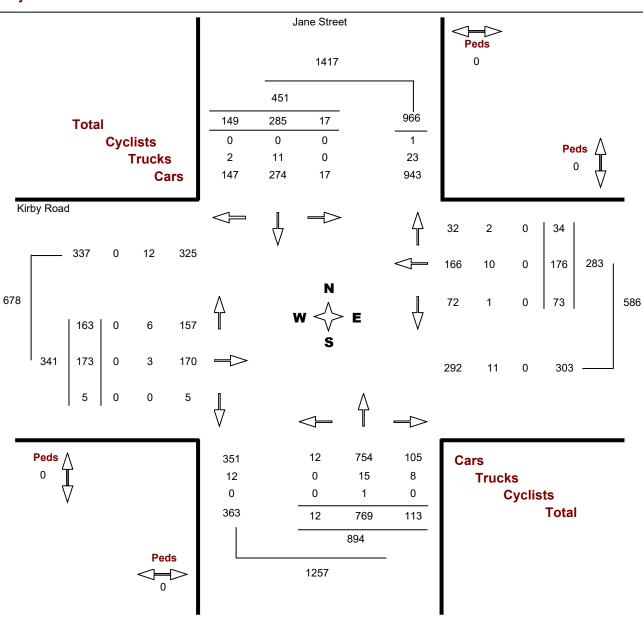
GeoID...... 9674ADF5

Count Date. Thursday, 12 September,

2019

Count Period. 03:00 PM — 06:00 PM

Peak Hour.... 05:00 PM — 06:00 PM





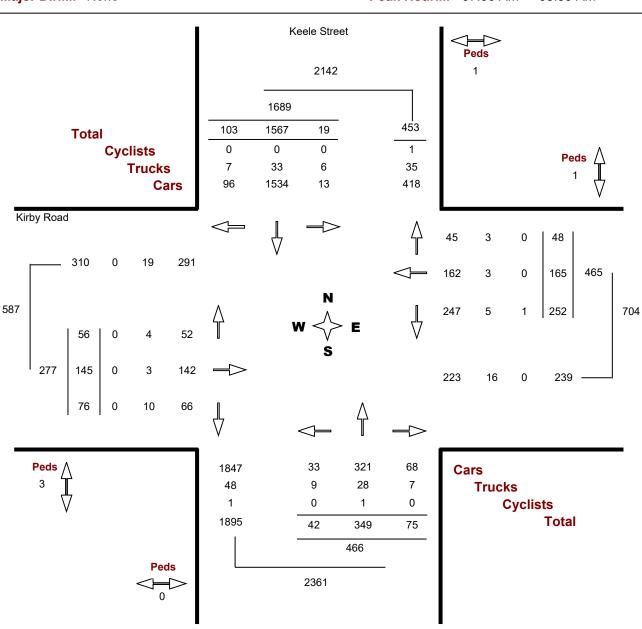
Location...... Keele Street & Kirby Road GeolD...... D1243207

Municipality. Vaughan Count Date. Thursday, 13 September,

2018

Traffic Cont. Traffic signal **Count Period.** 07:00 AM — 09:00 AM

Major Dir.... None **Peak Hour....** 07:30 AM — 08:30 AM





Location...... Keele Street & Kirby Road

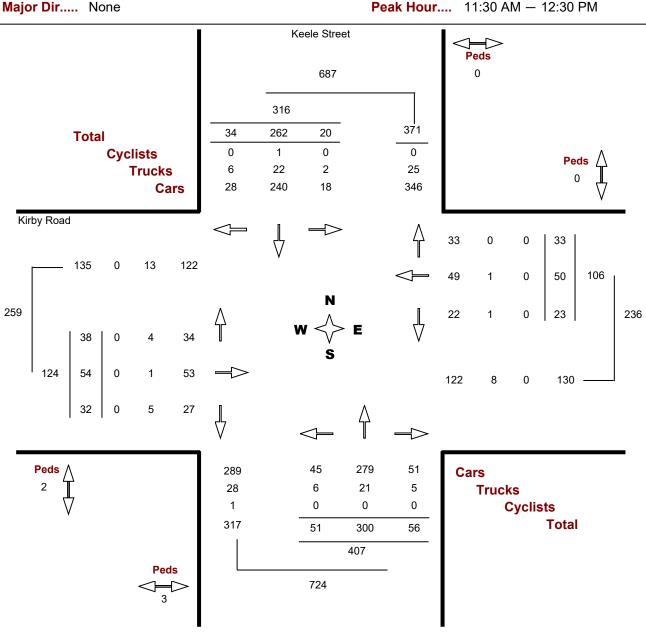
Municipality. Vaughan **Count Date.** Thursday, 13 September,

2018

D1243207

GeoID.....

Count Period. 11:00 AM — 02:00 PM Traffic Cont. Traffic signal





Location...... Keele Street & Kirby Road

Municipality. Vaughan

Traffic Cont. Traffic signal

Major Dir.... None

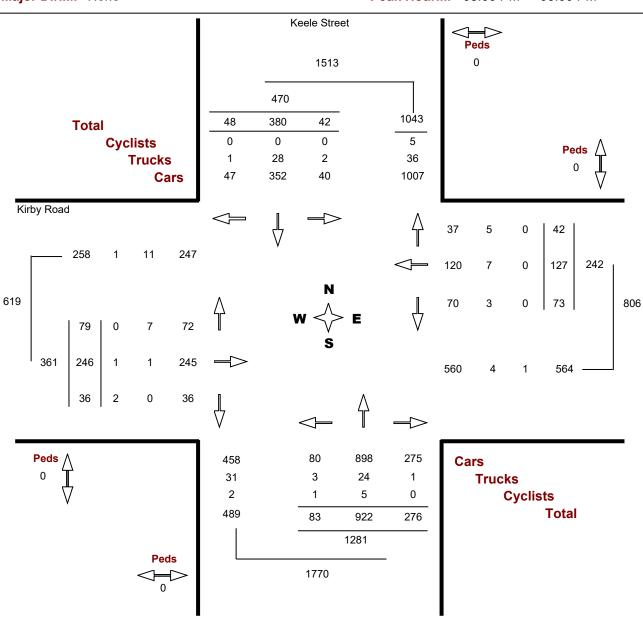
GeolD...... D1243207

Count Date. Thursday, 13 September,

2018

Count Period. 03:00 PM — 06:00 PM

Peak Hour.... 05:00 PM — 06:00 PM



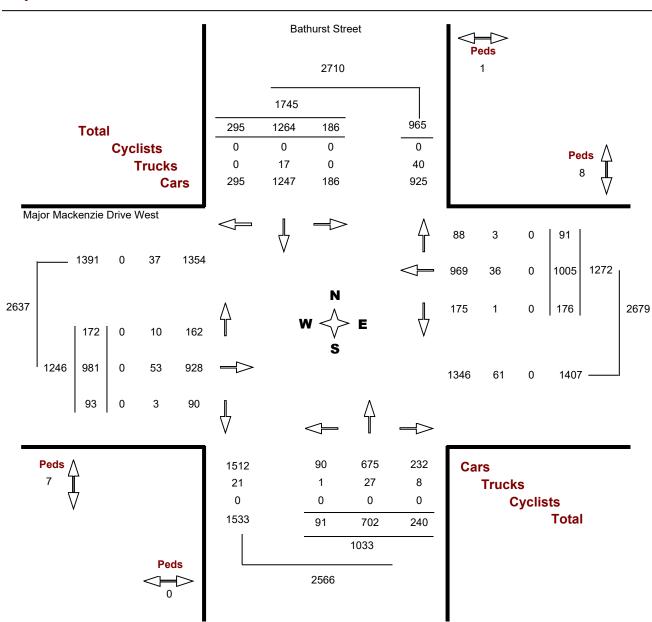


Location...... Major Mackenzie Drive West & Bathurst Street GeolD...... 09601327

Municipality. Vaughan Count Date. Tuesday, 10 May, 2016

Traffic Cont. Traffic signal **Count Period.** 07:00 AM — 09:00 AM

Major Dir.... None **Peak Hour...** 07:45 AM — 08:45 AM



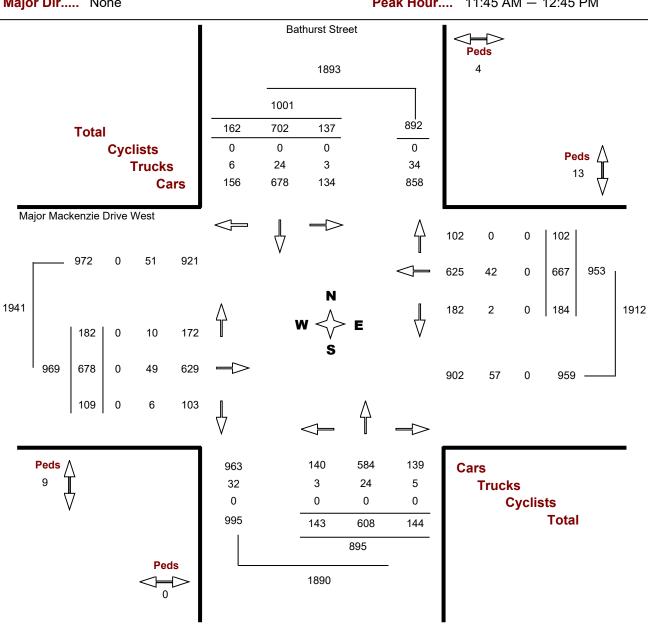


Location...... Major Mackenzie Drive West & Bathurst Street GeolD...... 09601327

Municipality. Vaughan **Count Date.** Tuesday, 10 May, 2016

Traffic Cont. Traffic signal **Count Period.** 11:00 AM — 02:00 PM

Major Dir..... None **Peak Hour....** 11:45 AM — 12:45 PM



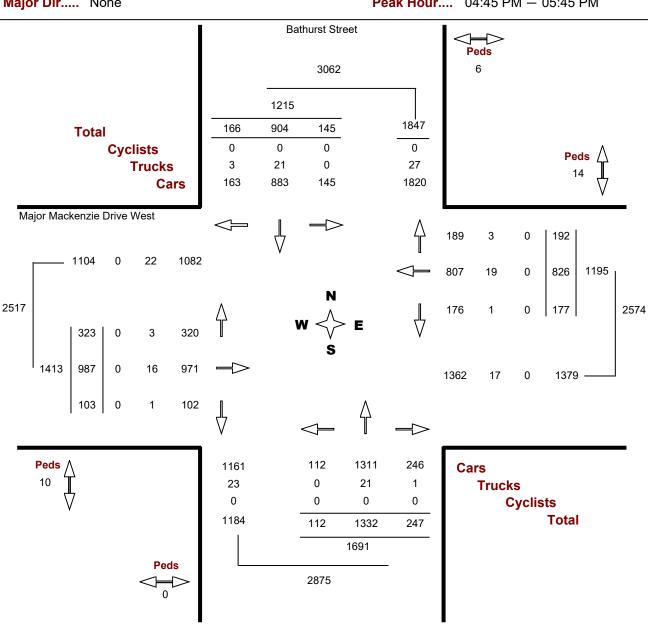


Location...... Major Mackenzie Drive West & Bathurst Street GeolD...... 09601327

Municipality. Vaughan **Count Date.** Tuesday, 10 May, 2016

Traffic Cont. Traffic signal **Count Period.** 03:00 PM — 06:00 PM

Major Dir..... None **Peak Hour....** 04:45 PM — 05:45 PM



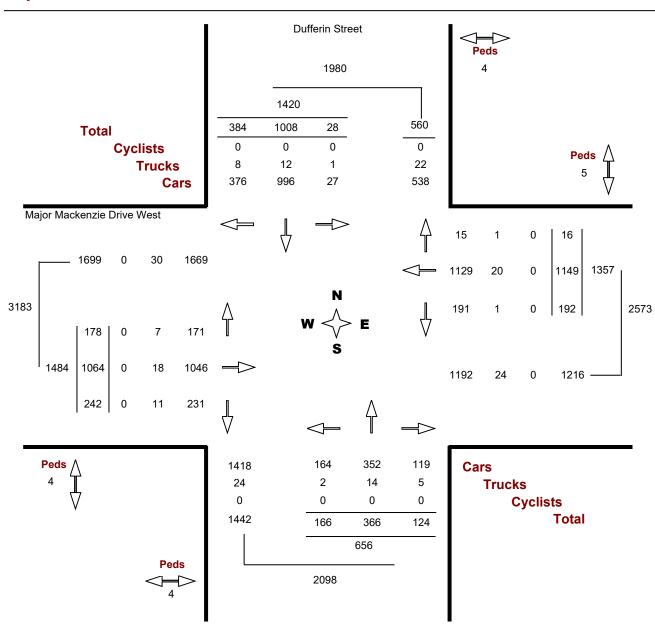


Location...... Major Mackenzie Drive West & Dufferin Street GeolD...... 88C4B88E

Municipality. Vaughan Count Date. Tuesday, 07 March, 2017

Traffic Cont. Traffic signal **Count Period.** 07:00 AM — 09:00 AM

Major Dir.... None **Peak Hour...** 07:45 AM — 08:45 AM



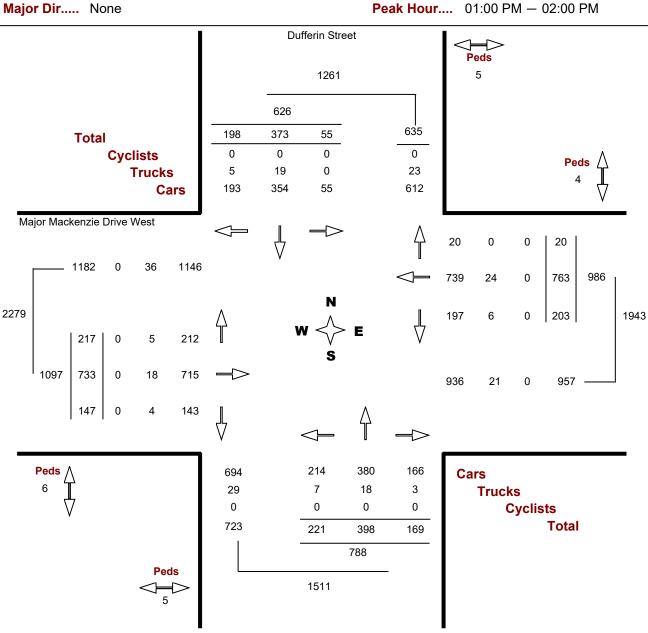


Location...... Major Mackenzie Drive West & Dufferin Street GeolD...... 88C4B88E

Municipality. Vaughan Count Date. Tuesday, 07 March, 2017

Traffic Cont. Traffic signal **Count Period.** 11:00 AM — 02:00 PM

Peak Hour.... 01:00 PM — 02:00 PM



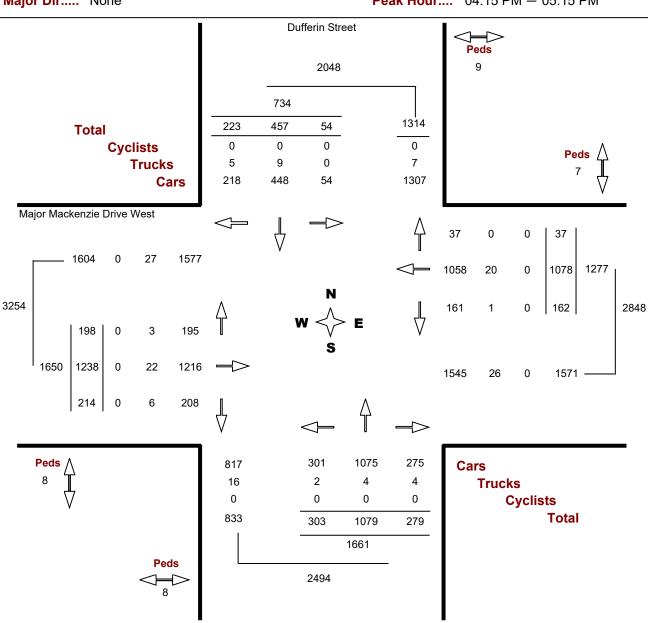


Location...... Major Mackenzie Drive West & Dufferin Street GeolD...... 88C4B88E

Municipality. Vaughan Count Date. Tuesday, 07 March, 2017

Traffic Cont. Traffic signal **Count Period.** 03:00 PM — 06:00 PM

Major Dir.... None **Peak Hour....** 04:15 PM — 05:15 PM





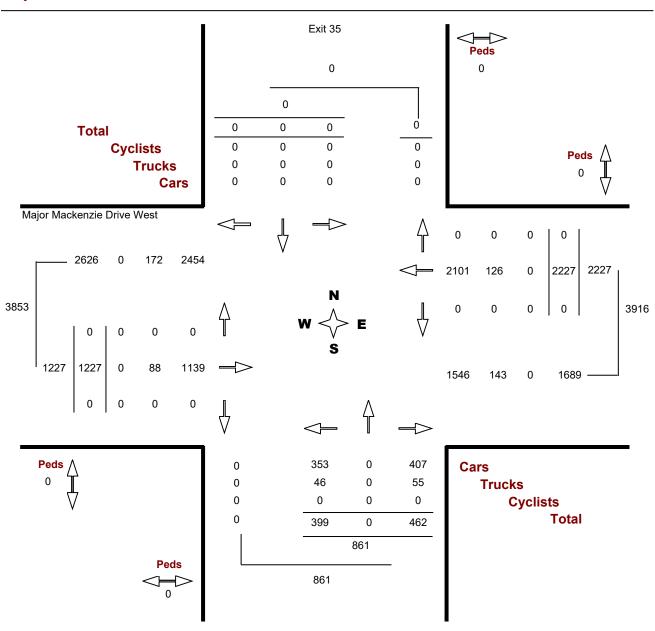
EBF36208

Location...... Major Mackenzie Drive West & Exit 35 GeolD......

Municipality. Vaughan Count Date. Monday, 04 March, 2019

Traffic Cont. Traffic signal Count Period. 07:00 AM — 09:00 AM

Major Dir.... None **Peak Hour...** 07:30 AM — 08:30 AM



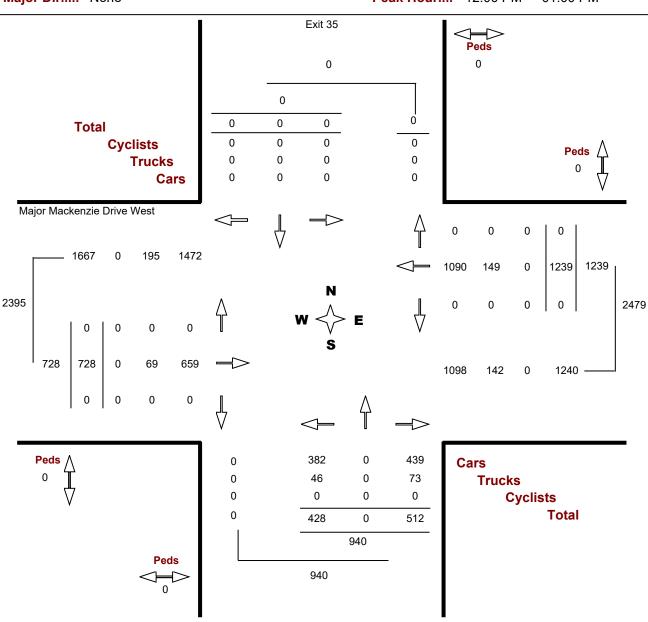


Location...... Major Mackenzie Drive West & Exit 35 GeolD...... EBF36208

Municipality. Vaughan Count Date. Monday, 04 March, 2019

Traffic Cont. Traffic signal Count Period. 11:00 AM — 02:00 PM

Major Dir.... None **Peak Hour...** 12:00 PM — 01:00 PM





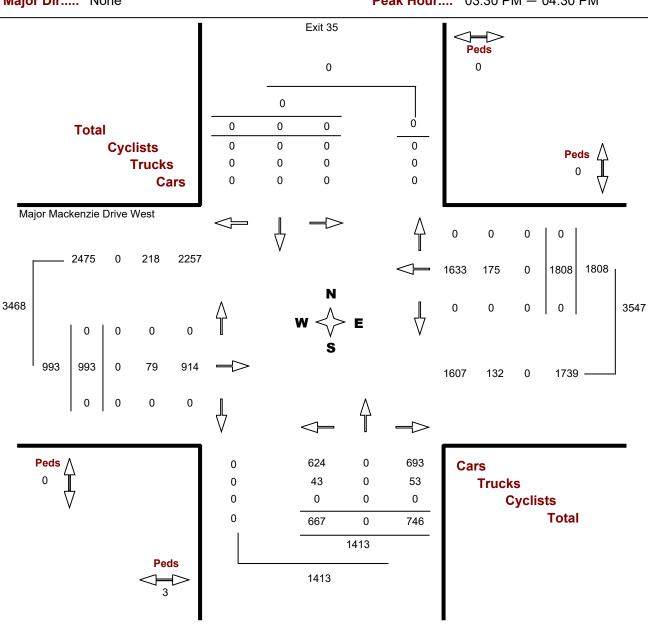
EBF36208

Location...... Major Mackenzie Drive West & Exit 35 GeolD......

Municipality. Vaughan Count Date. Monday, 04 March, 2019

Traffic Cont. Traffic signal Count Period. 03:00 PM — 06:00 PM

Major Dir.... None **Peak Hour...** 03:30 PM — 04:30 PM





Location...... Major Mackenzie Drive West & Exit 35/GO

Carpool Lot - Hwy 400 & Major Mackenzie

Drive West

Municipality. Vaughan

Traffic Cont. Traffic signal

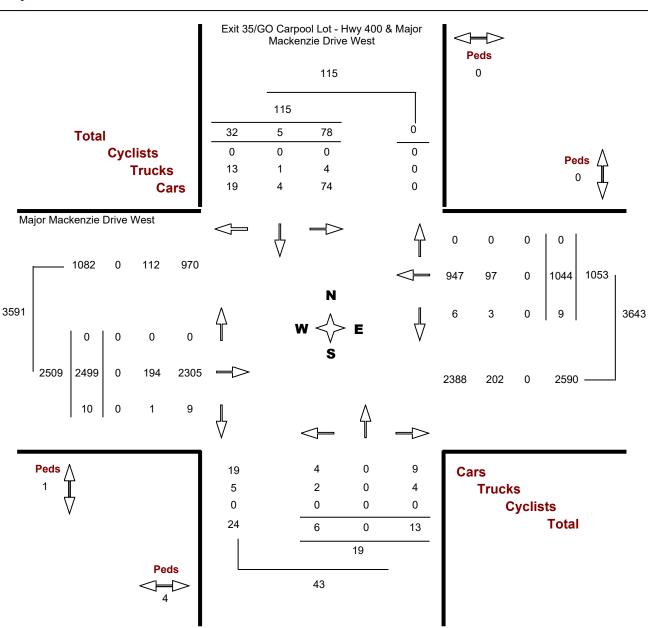
Major Dir..... None

GeoID...... CB10E2BE

Count Date. Thursday, 21 November, 2019

Count Period. 07:00 AM — 09:00 AM

Peak Hour.... 07:45 AM — 08:45 AM





Location...... Major Mackenzie Drive West & Exit 35/GO

Carpool Lot - Hwy 400 & Major Mackenzie

Drive West

Municipality. Vaughan

Traffic Cont. Traffic signal

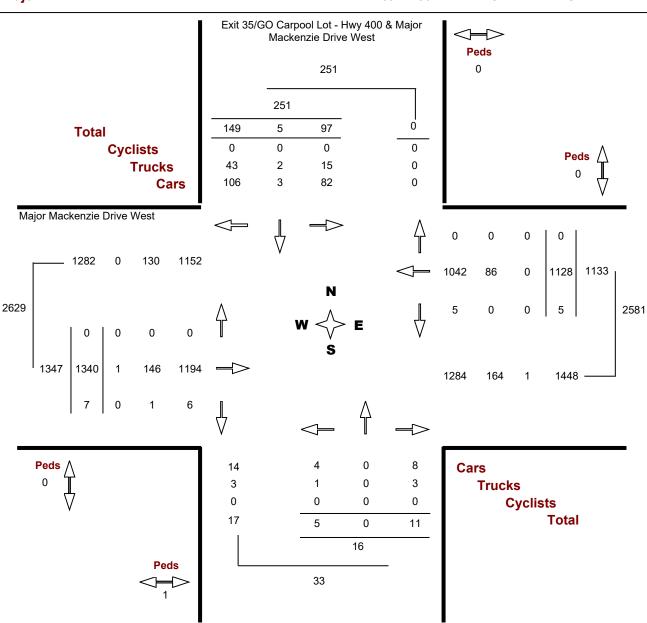
Major Dir..... None

GeoID...... CB10E2BE

Count Date. Thursday, 21 November, 2019

Count Period. 11:00 AM — 02:00 PM

Peak Hour.... 11:45 AM — 12:45 PM





Location...... Major Mackenzie Drive West & Exit 35/GO

Carpool Lot - Hwy 400 & Major Mackenzie

Drive West

Municipality. Vaughan

Traffic Cont. Traffic signal

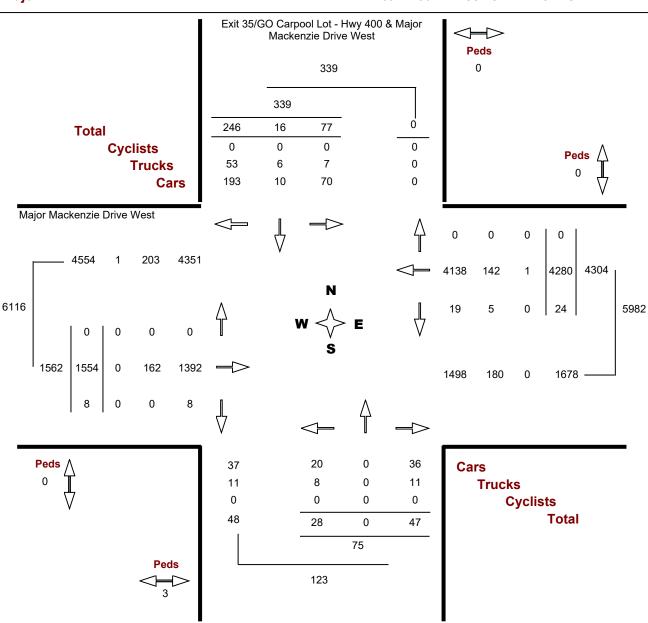
Major Dir..... None

GeoID...... CB10E2BE

Count Date. Thursday, 21 November, 2019

Count Period. 03:00 PM — 06:00 PM

Peak Hour.... 03:15 PM — 04:15 PM





Location...... Major Mackenzie Drive West & Jane Street

Municipality. Vaughan

Traffic Cont. Traffic signal

Major Dir..... None

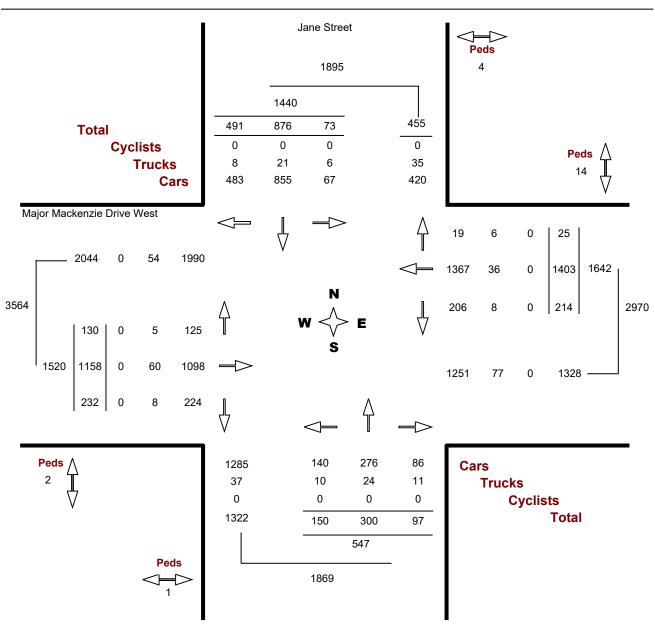
GeoID...... 9C39868B

Count Date. Wednesday, 23 November,

2016

Count Period. 07:00 AM — 09:00 AM

Peak Hour.... 07:45 AM — 08:45 AM





Location...... Major Mackenzie Drive West & Jane Street

Municipality. Vaughan

Traffic Cont. Traffic signal

Major Dir..... None

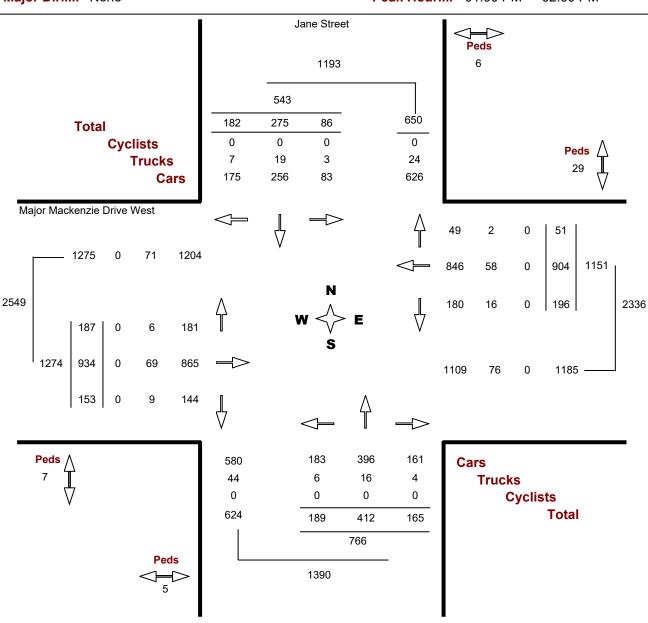
GeoID...... 9C39868B

Count Date. Wednesday, 23 November,

2016

Count Period. 11:00 AM — 02:00 PM

Peak Hour.... 01:00 PM — 02:00 PM





Location...... Major Mackenzie Drive West & Jane Street

Municipality. Vaughan

Traffic Cont. Traffic signal

Major Dir..... None

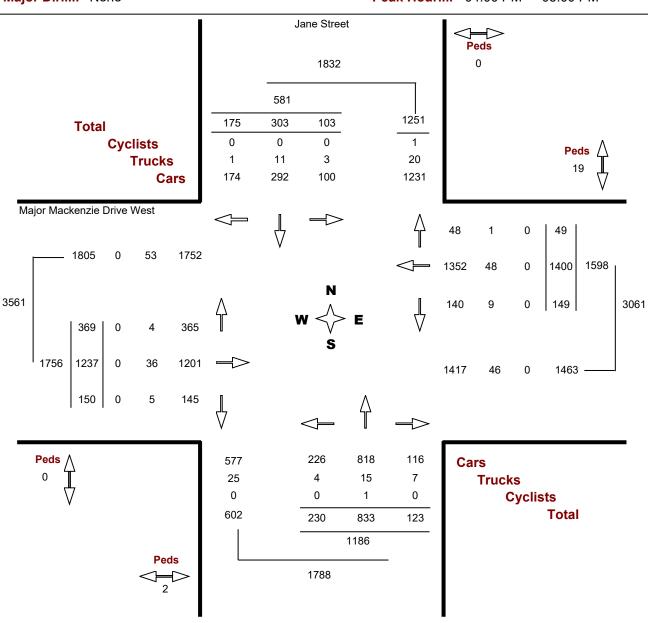
GeoID...... 9C39868B

Count Date. Wednesday, 23 November,

2016

Count Period. 03:00 PM — 06:00 PM

Peak Hour.... 04:00 PM — 05:00 PM



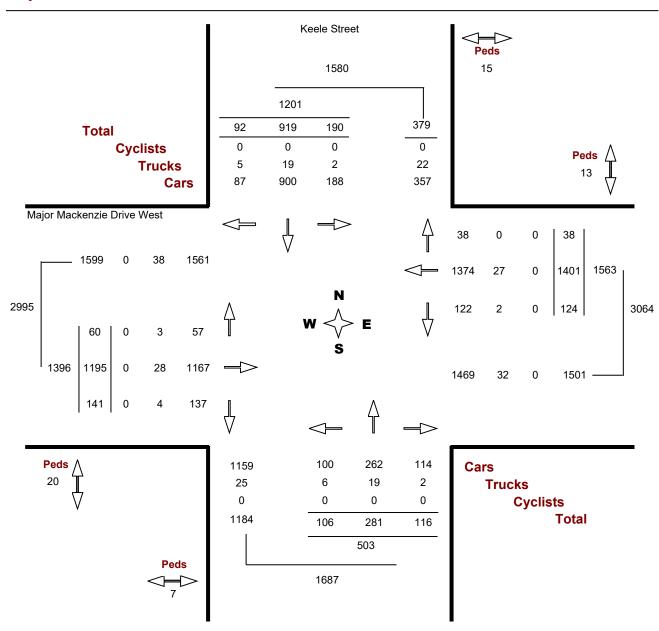


Location...... Keele Street & Major Mackenzie Drive West GeolD...... 54568594

Municipality. Vaughan Count Date. Tuesday, 24 March, 2015

Traffic Cont. Traffic signal **Count Period.** 07:00 AM — 09:00 AM

Major Dir.... None **Peak Hour....** 07:30 AM — 08:30 AM



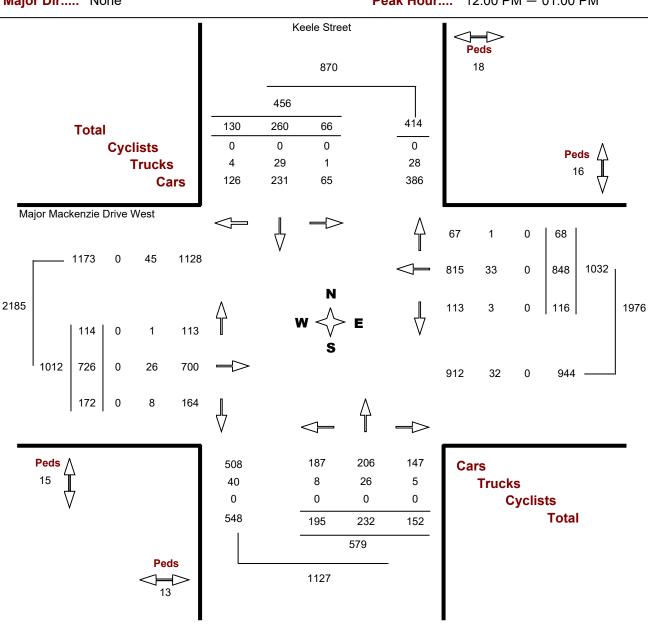


Location...... Keele Street & Major Mackenzie Drive West GeolD...... 54568594

Municipality. Vaughan Count Date. Tuesday, 24 March, 2015

Traffic Cont. Traffic signal **Count Period.** 11:00 AM — 02:00 PM

Major Dir.... None **Peak Hour...** 12:00 PM — 01:00 PM



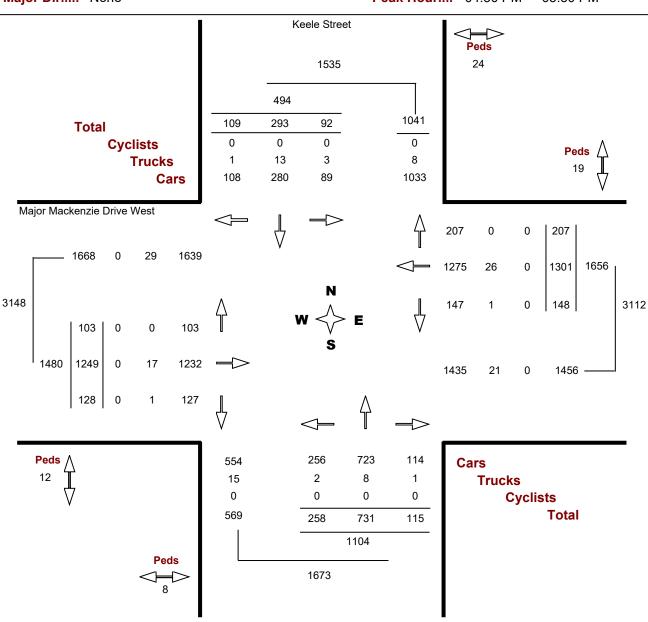


Location...... Keele Street & Major Mackenzie Drive West GeolD...... 54568594

Municipality. Vaughan Count Date. Tuesday, 24 March, 2015

Traffic Cont. Traffic signal **Count Period.** 03:00 PM — 06:00 PM

Major Dir.... None **Peak Hour...** 04:30 PM — 05:30 PM



LOCATION: Hwy 400 NB & Teston Rd MUNICIPALITY: Vaughan 753 (MTO Signal) Ņ CTCS: COMPUTER SYSTEM: Centracs Econolite Cobalt / TS2T1 MODE/COMMENT: SA CONTROLLER/CABINET TYPE: PREPARED/CHECKED BY: MQL CONFLICT FLASH: Red & Red PREPARATION DATE: April 10, 2019 DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s) IMPLEMENTATION DATE: June 27, 2019 CHANNEL/DROP: ΡМ Free Normal 16:30-18:30, **Phase Mode** All Other Times Remarks NEMA Phase (MTO) M-F (Fixed/Demanded/Callable) Time Pattern 98 Pattern 99 Plan 98 Plan 99 1. W/B Left Turn Arrow Pedestrian Minimums: EWWK = 7 sec., EWFD = 13 sec. NSWK = 7 sec., NSFD = 22 sec. WLK FDW MIN Emergency vehicle pre-emption 3/4: EXT NOT USED MAX1 Serve EWG/EWDW min 20 secs and up to MAX2 100 secs if there are continuous AMB emergency calls in EW direction. ALR SPLIT NB phase is callable by vehicle or 2. Eastbound pedestrian actuation. If a vehicle call is WLK received, the minimum NBG is 15 FDW 13 Ped Recall, Veh Max Recall seconds. If ongoing vehicle demand exists MIN 20 on the stopbar loop, the NBG is capable of EXT 4 providing vehicle extensions up to the MAX1 47 maximum green. If a pedestrian call is Use MAX2 MAX2 37 received, the pedestrian minimum will be AMB 4.5 served. AI R 3.0 Teston Rd SPLIT 0 0 Please see reverse page for Pretime. 3. S/B Left Turn Arrow WLK FDW MIN EXT NOT USED MAX1 MAX2 AMB ALR SPLIT 4 Northbound WLK Callable by stopbar loop and/or FDW pushbutton MIN 15 Extendable by stopbar loop EXT 3 MAX1 31 MAX2 41 Use MAX2 AMB 4.5 ALR 3.0 Hwy 400 NB SPLIT 0 0 5. N/B Left Turn Arrow WLK lfDW MIN EXT NOT USED MAX1 MAX2 AMB ALR SPLIT 6. Westbound WLK FDW 0 Veh Max Recall MIN 20 EXT MAX1 47 MAX2 37 Use MAX2 AMB 4.5 ALR 3.0 Teston Rd SPLIT 0 0 LEGEND: WLK SA - Semi-Actuated signal FDW WLK - Walk time MIN FDW - Flashing Don't Walk time EXT NOT USED MIN - Minimum green time MAX1 MAX2 EXT - Extension time AMB MAX1 - Maximum green time 1 ALR MAX2 - Maximum green time 2 SPLIT AMB - Amber ALR -All Red WLK CL - Cycle Length FDW OF - Offset MIN VP - Vehicle Permissive EXT NSWK - North/South Walk NOT USED MAX1 EWWK - East/West Walk MAX2 NSG - North/South Green AMB EWG - East/West Green ALR NSFD - North/South Flashing Don't Walk SPLIT EWFD - East/West Flashing Don't Walk TSP - Transit Priority CL 0 (FREE) 0 (FREE) APS - Audible Pedestrian Signal OF 0 (FREE) 0 (FREE) RLC - Red Light Camera VΡ 0 (FREE) 0 (FREE)

| LOCATION: CTCS: | Teston Road 747 | (YR 49) at Cit | yview Blvd. | | MUNICIPALITY: COMPUTER SYSTEM: | | |
|--|---|------------------|---------------|----------------------------------|---|--|--|
| MODE/COMMENT: PREPARED/CHECKED BY: PREPARATION DATE: | SA M.L. | | | | CONTROLLER/CABINET TYPE: CONFLICT FLASH: DESIGN WALK SPEED: | I | |
| IMPLEMENTATION DATE: | June 26, 201 | 9 AM | | Free | CHANNEL/DROP: | | |
| | | 6:00-10:0 M-F | | | Phase Mode | | |
| NEMA Phase (York) | | | | | | Remarks | |
| | Local Plan System Plan | Pattern 1 Plan 1 | | Pattern 99 Plan 99 | (Fixed/Demanded/Callable) | | |
| 1. | WLK FDW | i idii i | | 1 1411 33 | | Pedestrian Minimums: EWWK = 7 sec., EWFD = 20 sec. NSWK = 7 sec., NSFD = 25 sec. | |
| | MIN EXT | | | | | Emergency vehicle pre-emption 3: | |
| NOT USED | MAX1 MAX2 AMB ALR | | | | | Serve EWG/EWDW min 20 secs and up to 100 secs if there are continuous emergency calls in EW direction. | |
| 2. Westbound | SPLIT | | | | | Emergency vehicle pre-emption 4: | |
| ← | WLK 7 FDW 20 MIN 30 EXT 0 MAX1 50 MAX2 120 AMB 5.0 | USE MAX 2 | | | Fixed | Serve NBG/NBDW min 20 secs and up to 100 secs if there are continuous emergency calls in NS direction. NS phase is callable by vehicle or | |
| Teston Road | ALR 2.0 SPLIT | | | | | pedestrian actuation. If a vehicle call is received, the minimum NSG is 10 seconds. | |
| NOT USED | WLK FDW MIN EXT MAX1 MAX2 AMB ALR SPLIT | | | | | If ongoing vehicle demand exists on the stopbar loop, the NSG is capable of providing vehicle extensions up to the maximum green split during coordinated operation or 19 secs during Free operation. If a pedestrian call is received, the pedestrian minimum will be served. The NSWK & NSFD are only displayed on the pedestrian signal heads if a pedestrian call is received. Extension time is based on vehicle demand. Unused extension time is | |
| NOT USED | WLK FDW MIN EXT MAX1 MAX2 AMB ALR SPLIT | | | | | During coordinated operation, the signal constantly cycles through main street FDW to improve response time to side street vehicle and pedestrian demand. | |
| 5. W/B Left Turn Arrow | WLK | 0 | | | | During free plan, signal rests in EWWK and does not cycle through EWFD unless there | |
| • | FDW MIN 7 EXT 0 MAX1 50 MAX2 90 AMB 3 ALR 1 SPLIT | USE MAX 2 | | | Callable/Extendable by Setback Loop | is side street vehicle or pedestrian demand. EWFD reverts to EWWK if there is no side street demand at the end of the EWFD. | |
| 6. Eastbound Teston Road | WLK 7 FDW 20 MIN 30 EXT 0 MAX1 50 MAX2 30 AMB 5.0 ALR 2.0 SPLIT | USE MAX 2 | | | Fixed | | |
| 7. Southbound Split Phase | WLK | | | | | LEGEND: | |
| | MIN 7 EXT 3 MAX1 7 MAX2 10 AMB 3 ALR 2 SPLIT | USE MAX 2 | | | Callable by stopbar loop | SA - Semi-Actuated signal WLK - Walk time FDW - Flashing Don't Walk time MIN - Minimum green time EXT - Extension time MAX1 - Maximum green time 1 MAX2 - Maximum green time 2 AMB - Amber | |
| 8. Northbound Split Phase Cityview Blvd. | WLK 7 FDW 25 MIN 10 EXT 3 MAX1 25 MAX2 20 AMB 4.0 ALR 2.0 SPLIT | USE MAX 2 | | | Callable by stopbar loop and/or pushbutton; Extendable by stopbar loop. | ALR -All Red CL - Cycle Length OF - Offset VP - Vehicle Permissive NSWK - North/South Walk EWWK - East/West Walk NSG - North/South Green EWG - East/West Green NSFD - North/South Flashing Don't Walk EWFD - East/West Flashing Don't Walk | |
| NOTES: | CL OF VP | 0 | 0 0 | 0 (FREE) 0 (FREE) 0 (FREE) | | TSP - Transit Priority APS - Audible Pedestrian Signal RLC - Red Light Camera | |

LOCATION: Major Mackenzie Dr (YR 25) & Jane St (YR 55) MUNICIPALITY: Vaughan 124 COMPUTER SYSTEM: Centracs CTCS MODE/COMMENT: CONTROLLER/CABINET TYPE: Econolite ASC/3-1000 / TS2T1 PREPARED/CHECKED BY: ML CONFLICT FLASH: Red & Red PREPARATION DATE: DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s) IMPLEMENTATION DATE: Sep. 22,2020 CHANNEL/DROP: AM РМ Free off Phase Mode 22:00-06:00 M-F: 15:00-20:00 10:00-15:00, 20:00-20:00-08:00 Sat. 8 06:00-10:00 22:00 M-F; 08:00-M-F Remarks Sun. M-F 20:00 Sat & Sun **NEMA Phase (York)** (Fixed/Demanded/Callable) Local Plan Pattern 1 Pattern 2 Pattern 3 Pattern 99 System Plan Plan 1 Plan 2 Plan 3 Plan 99 . E/B Left Turn Arrow Fully Protected Fully Prot. WIK FDW Callable/Extendable MIN by Stopbar Loop Emergency vehicle pre-emption 1: EXT MAX1 20 Serve EBG/EBLT min 20 secs and up to MAX2 0 100 secs if there are continuous AMR 3 emergency calls in EB direction. 2 AI R SPLIT 15 20 0 Emergency vehicle pre-emption 2: 2. Westbound WLK Serve WBG/WBLT min 20 secs and up to FDW 30 Veh Ext. Recall 100 secs if there are continuous MIN 37 emergency calls in WB direction. **EXT** 0 40 0 MAX1 Emergency vehicle pre-emption 3: MAX2 AMB 4.0 Serve NSG/NSDW min 20 secs and up to ALR 4.0 100 secs if there are continuous Major Mackenzie Dr 80 emergency calls in NS direction. 3. N/B Left Turn Arrow MIK Callable/Extendable NS phase is callable by vehicle or **FDW** by Setback Loop pedestrian actuation. If a vehicle call is MIN 3 received, the minimum NSG is 10 EXT MAX1 seconds. If ongoing vehicle demand 20 0 MAX2 exists on the stopbar loop, the NSG is AMB capable of providing vehicle extensions up to the maximum green split during 15 19 SPLI1 coordinated operation or 50 secs during Southbound Free operation. If a pedestrian call is WLK received, the pedestrian minimum will be FDW 30 Callable by stopbar loop served. The NSWK & NSFD are only MIN 10 and/or pushbutton; EXT Extendable by stopbar loop. displayed on the pedestrian signal heads MAX1 40 if a pedestrian call is received. Extension MAX2 0 time is based on vehicle demand. Unused AMB 4.5 extension time is given to the EWG ALR 3.5 during coordinated operation. Jane St SPLIT 50 46 5. W/B Left Turn Arrow During coordinated operation, the signal WLK constantly cycles through main street FDW Callable/Extendable FDW to improve response time to side MIN by Stopbar Loop street vehicle and pedestrian demand. FXT 3 20 MAX1 During free plan, signal rests in EWWK MAX2 0 and does not cycle through EWFD unless AMB there is side street vehicle or pedestrian ALR demand SPLIT 20 12 Eastbound EWFD reverts to EWWK if there is no WIK 7 side street demand at the end of the 30 37 0 FDW Veh Ext. Recall EWFD. MIN **EXT** MAX1 40 MAX2 0 AMB 4.0 ALR 4.0 SPLIT 75 83 Major Mackenzie Dr 66 0 7. S/B Left Turn Arrow LEGEND: WLK Callable/Extendable FDW by Setback Loop SA - Semi-Actuated signal MIN WLK - Walk time 3 EXT FDW - Flashing Don't Walk time MAX1 20 MIN - Minimum green time MAX2 0 EXT - Extension time AMB 3 MAX1 - Maximum green time 1 ALR MAX2 - Maximum green time 2 SPLIT 15 AMB - Amber 8. Northbound ALR -All Red WLK CL - Cycle Length FDW 30 Callable by stopbar loop MIN 10 and/or pushbutton; OF - Offset Extendable by stopbar loop. VP - Vehicle Permissive FXT 3 40 MAX1 NSWK - North/South Walk MAX2 0 EWWK - East/West Walk AMB 4.5 NSG - North/South Green 3.5 EWG - East/West Green Jane St 50 50 NSFD - North/South Flashing Don't Walk EWFD - East/West Flashing Don't Walk 160 160 140 0 (FREE) TSP - Transit Priority APS - Audible Pedestrian Signal OF 0 0 (FREE) 0 0 VP 30 30 0 (FREE) 30 RLC - Red Light Camera

Hwy 400 NB Offramp & Major Mackenzie Dr (YR 25) MUNICIPALITY: Vaughan LOCATION: 441 (MTO Signal) CTCS COMPUTER SYSTEM: Centracs **Fully Actuated** MODE/COMMENT: CONTROLLER/CABINET TYPE: Econolite Cobalt / TS2T1 PREPARED/CHECKED BY: M.L. CONFLICT FLASH: Red & Red PREPARATION DATE: DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s) June 19,2020 IMPLEMENTATION DATE CHANNEL/DROP: AΜ ΡМ OFF Free Phase Mode 10:00-15:00, 22:00-06:00 M-F 15:00-20:00 06:00-10:00 20:00-22:00 M-F; M-F 20:00-08:00 Remarks NEMA Phase (MTO) M-F 08:00-20:00 Sat. Sat&Sun & Sun. Fixed/Demanded/Callable Local Plan Pattern 2 Pattern 3 Pattern 99 Pattern 1 System Plan Plan 1 Plan 2 Plan 3 Plan 99 Pedestrian Minimums: WLK EWWK = 7 sec., EWFD = 22 sec. FDW MIN Emergency vehicle pre-emption 3/4: FXT NOT USED MAX1 Serve EWG/EWDW min 20 secs and up MAX2 to 100 secs if there are continuous AMB emergency calls in EW direction. ALR Pre time SPLIT 2. Eastbound WIK EW phase is callable by vehicle or FDW 22 22 Callable by stopbar loop pedestrian actuation. If a vehicle call is MIN 40 29 and/or pushbutton; received, the minimum EWG is 20 EXT 4 4 Extendable by stopbar loop seconds. If ongoing vehicle demand MAX1 60 40 exists on the stopbar loop, the EWG is MAX2 0 50 capable of providing vehicle extensions 4.5 AMB 4.5 up to the maximum green split during ALR 3.0 3.0 coordinated operation or 60 secs during 110 SPLI Major Mackenzie D Free operation. If a pedestrian call is received, the pedestrian minimum will be WLK served. The EWWK & EWFD are only FDW displayed on the pedestrian signal heads MIN if a pedestrian call is received. Extension EXT NOT USED time is based on vehicle demand. MAX1 MAX2 AMB AI R During coordinated operation, the signal SPLIT constantly cycles through main street DW to improve response time to side WIK street vehicle and pedestrian demand. FDW MIN During free plan, signal rests in EWWK EXT NOT USED and does not cycle through EWFD unless MAX1 there is side street vehicle or pedestrian MAX2 demand. AMB ALR EWFD reverts to EWWK if there is no SPLIT side street demand at the end of the EWFD. WLK FDW MIN EXT NOT USED MAX1 MAX2 AMB ALR SPLIT Westbound WIK 22 FDW 22 Callable by stopbar loop MIN 29 40 4 FXT 4 Extendable by stopbar loop MAX1 60 40 MAX2 0 50 AMB 4.5 4.5 ALR 3.0 3.0 110 110 Major Mackenzie Dr SPLI1 LEGEND: WLK SA - Semi-Actuated signal FDW WIK - Walk time MIN FDW - Flashing Don't Walk time EXT NOT USED MIN - Minimum green time MAX1 EXT - Extension time MAX2 MAX1 - Maximum green time 1 AMB MAX2 - Maximum green time 2

LOCATION Keele St (YR 6) & Major Mackenzie Dr W (YR 25) MUNICIPALITY: Vaughan CTCS: 27 COMPUTER SYSTEM: Centracs FXT CONTROLLER/CABINET TYPE: Econolite Cobalt / TS2T1 MODE/COMMENT: PREPARED/CHECKED BY: M.L. CONFLICT FLASH: Red & Red PREPARATION DATE: DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s Feb. 10, 2019 IMPLEMENTATION DATE CHANNEL/DROP. AM OFF Free 10:00-15:00 Phase Mode 22:00-6:00 M-F & 22:00-08:00 20:00-22:00 6:00-10:00 15:00-20:00 M-F 08:00-Remarks M-F **NEMA Phase (York)** 20:00 Sat. & Sat&Sun (Fixed/Demanded/Callable) Sun. Local Plan Pattern 2 Pattern 99 Pattern 1 System Plan Plan 1 Plan 2 Plan 3 Plan 99 1. E/B Left Turn Arrow Pedestrian Minimums EWWK = 7 sec., EWFD = 26 sec. WLK FDW Callable/Extendable NSWK = 7 sec., NSFD = 25 sec MIN by Setback Loop Emergency vehicle pre-emption 3: FXT 3 7 MAX1 Serve EWG/EWDW min 20 secs and up 0 MAX2 to 100 secs if there are continuous AMB 3 emergency calls in EW direction. ALR 20 SPLIT Emergency vehicle pre-emption 4: 2. Westbound WLK Serve NSG/NSDW min 20 secs and up to FDW 26 Fixed 100 secs if there are continuous MIN 28 emergency calls in NS direction. EXT MAX1 28 MAX2 0 AMB 4.0 ALR 3.0 73 68 50 0 Major Mackenzie Dr SPLIT 3. N/B Left Turn Arrow WLK Callable/Extendable FDW by Setback Loop MIN EXT 3 MAX1 MAX2 0 AMB 3 ALR SPLIT 12 20 12 0 Southbound WLK FDW Fixed MIN EXT 27 3 MAX1 27 MAX2 0 AMR 4 0 ALR 3.0 W/B Left Turn Arrow WLK FDW Callable/Extendable MIN by Setback Loop EXT MAX1 7 MAX2 0 AMB ALR 15 20 12 0 SPLIT 6. Eastbound WLK FDW 26 Fixed MIN 28 EXT MAX1 28 MAX2 0 AMB 4.0 ALR 3.0 Major Mackenzie Dr SPI IT 73 68 LEGEND: 7. S/B Left Turn Arrow WLK Callable/Extendable SA - Semi-Actuated signal FDW by Setback Loop WLK - Walk time MIN FDW - Flashing Don't Walk time EXT MIN - Minimum green time MAX1 7 EXT - Extension time MAX2 0 MAX1 - Maximum green time 1 AMB 3 MAX2 - Maximum green time 2 ALR AMB - Amber 27 12 12 0 ALR -All Red 8. Northbound CL - Cycle Length OF - Offset WLK FDW VP - Vehicle Permissive 25 Fixed NSWK - North/South Walk MIN 27 EWWK - East/West Walk EXT 3 NSG - North/South Green MAX1 27 EWG - East/West Green MAX2 0 NSFD - North/South Flashing Don't Walk EWFD - East/West Flashing Don't Walk AMB 4.0 TSP - Transit Priority APS - Audible Pedestrian Signal RLC - Red Light Camera ALR 3.0 SPLIT 46 Keele St 60 CI 0 (FRFF) 160 160 120 OF 0 (FREE) 0 0 0 VP 26 26 26 0 (FREE)

LOCATION: Major Mackenzie Dr (YR 25) & Bathurst ST (YR 38)
CTCS: 117
MODE/COMMENT: SA

SA MQL March 23, 2015 December 6, 2017

PREPARED/CHECKED BY:

IMPLEMENTATION DATE:

PREPARATION DATE:

MUNICIPALITY: Vaughan
COMPUTER SYSTEM: Centracs
CONTROLLER/CABINET TYPE: Econolite Cobalt / TS2T1
CONFLICT FLASH: Red & Red

DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s) CHANNEL/DROP:

| | | AM | PM | OFF 10:00-16:00, | AM 2 | PM 2 | Free | Dhara Mada | |
|--|--------------------|-----------------|----------------|-----------------------|-----------------|----------------|-----------------------------|---|--|
| | | 8:00- | 17:30- | 19:00-22:00 M | 6:00-8:00 | 16:00- | 22:00-6:00 M-F | Phase Mode | |
| NEMA Phase (York) | | 10:00 M-F | 19:00 M-F | F & 9:00-22:00 | M-F | 17:30 M-F | & 22:00-9:00 Sat& Sun | | Remarks |
| | Local Plan | Pattern 1 | Pattern 2 | Sat& Sun Pattern 3 | Pattern 4 | Pattern 5 | Pattern 99 | (Fixed/Demanded/Callable) | |
| 1. E/B Left Turn Arrow | System Plan | | Plan 2 | Plan 3 | Plan 4 | Plan 5 | Plan 99 | | Pedestrian Minimums: |
| | WLK FDW | | | | | | | Callable/Extendable | EWWK = 7 sec., EWFD = 24 sec. NSWK = 7 sec., NSFD = 27 sec. |
| | MIN 7 EXT 3 | | | | | | | by Setback Loop | Emergency vehicle pre-emption 3: |
| | MAX1 20 MAX2 0 | | | | | | | | Serve EWG/EWDW min 20 secs and up to 100 secs if there are continuous |
| | AMB 3 ALR 1 | | | | | | | | emergency calls in EW direction. |
| 2. Waathawad | SPLIT | 13 | 19 | 13 | 13 | 19 | 0 | | Emergency vehicle pre-emption 4: |
| 2. Westbound | WLK 7 | | | | | | | | Serve NSG/EWDW min 20 secs and up to 100 secs if there are continuous |
| | FDW 24 MIN 31 | | | | | | | Fixed | emergency calls in NS direction. |
| (←) | EXT 0 MAX1 31 | | | | | | | | NS phase is callable by vehicle or |
| | MAX2 0 AMB 4.5 | | | | | | | | pedestrian actuation. If a vehicle call is |
| | ALR 2.5 | | | | | | _ | | received, the minimum NSG is 30 seconds. If ongoing vehicle demand |
| Major Mackenzie Dr 3. N/B Left Turn Arrow | SPLIT | 50 | 47 | 42 | 43 | 40 | 0 | | exists on the stopbar loop, the NSG is |
| | WLK FDW | | | | | | | Callable/Extendable by Setback Loop | capable of providing vehicle extensions up to the maximum green split during |
| | MIN 7 EXT 3 | | | | | | | | coordinated operation or 30 secs during |
| | MAX1 20 | | | | | | | | Free operation. If a pedestrian call is received, the pedestrian minimum will be |
| | MAX2 0 AMB 3 | | | | | | | | served. The NSWK & NSFD are only |
| | ALR 1 SPLIT | 12 | 12 | 12 | 12 | 12 | 0 | | displayed on the pedestrian signal heads if a pedestrian call is received. Extension |
| 4. Southbound | WLK 7 | | | | | | | | time is based on vehicle demand. Unused extension time is given to the EWG. |
| A | FDW 27 MIN 30 | | | | | | | Callable by stopbar loop and/or pushbutton; | |
| | EXT 3 | | | | | | | Extendable by stopbar loop. | During coordinated operation, the signal constantly cycles through main street |
| | MAX1 30 MAX2 0 | | | | | | | | FDW to improve response time to side |
| | AMB 4.5 ALR 2.5 | | | | | | | | street vehicle and pedestrian demand. |
| Bathurst St 5. W/B Left Turn Arrow | SPLIT | 65 | 62 | 53 | 72 | 69 | 0 | | During free plan, signal rests in EWWK and does not cycle through EWFD unless |
| O. W/B Left Tuff/Mow | WLK FDW | | | | | | | Callable/Extendable | there is side street vehicle or pedestrian demand. |
| | MIN 7 | | | | | | | by Setback Loop | |
| | EXT 3 MAX1 20 | | | | | | | | EWFD reverts to EWWK if there is no side street demand at the end of the EWFD. |
| | MAX2 0 AMB 3 | | | | | | | | |
| | ALR 1 SPLIT | 13 | 16 | 13 | 13 | 12 | 0 | | |
| 6. Eastbound | | | | | | 12 | | | |
| | WLK 7 FDW 24 | | | | | | | Fixed | |
| | MIN 31 EXT 0 | | | | | | | | |
| \ \ | MAX1 31 MAX2 0 | | | | | | | | |
| | AMB 4.5 ALR 2.5 | | | | | | | | |
| Major Mackenzie Dr 7. S/B Left Turn Arrow | SPLIT 2.5 | 50 | 50 | 42 | 43 | 47 | 0 | | LEGEND: |
| 7. S/D Leit Tulli Allow | WLK | | | | | | | Callable/Extendable | |
| | FDW MIN 7 | | | | | | | by Setback Loop | SA - Semi-Actuated signal WLK - Walk time |
| | EXT 3 MAX1 20 | | | | | | | | FDW - Flashing Don't Walk time MIN - Minimum green time |
| | MAX2 0 AMB 3 | | | | | | | | EXT - Extension time |
| | ALR 1 SPLIT | 12 | 12 | 12 | 12 | 12 | 0 | | MAX1 - Maximum green time 1 MAX2 - Maximum green time 2 |
| 8. Northbound | | 12 | 12 | 12 | 14 | 12 | U | | AMB - Amber |
| | WLK 7 FDW 27 | | | | | | | Callable by stopbar loop | ALR -All Red CL - Cycle Length |
| | MIN 30 EXT 3 | | | | | | | and/or pushbutton; Extendable by stopbar loop. | OF - Offset VP - Vehicle Permissive |
| | MAX1 30 MAX2 0 | | | | | | | | NSWK - North/South Walk |
| | AMB 4.5 ALR 2.5 | | | | | | | | EWWK - East/West Walk NSG - North/South Green |
| Bathurst St | SPLIT 2.5 | 65 | 62 | 53 | 72 | 69 | 0 | | EWG - East/West Green NSFD - North/South Flashing Don't Walk |
| | CL | 140 | 140 | 120 | 140 | 140 | 0 (FREE) | | EWFD - East/West Flashing Don't Walk TSP - Transit Priority |
| | OF VP | 45 24 | 0 24 | 0 24 | 45 24 | 0 24 | 0 (FREE) 0 (FREE) | | APS - Audible Pedestrian Signal |
| II | ĺ | İ | İ | ĺ | i | | l | İ | i |

NOTES:

LOCATION: Jane Street (YR 55) & Kirby Road MUNICIPALITY: Vaughan CTCS: 887 COMPUTER SYSTEM: Centracs MODE/COMMENT: CONTROLLER/CABINET TYPE: Econolite Cobalt / TS2T1 PREPARED/CHECKED BY: M.L. CONFLICT FLASH: Red & Red PREPARATION DATE: DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s) IMPLEMENTATION DATE: July 13,2020 CHANNEL/DROP Free Phase Mode 24 Hrs Daily Remarks NEMA Phase (York) (Fixed/Demanded/Callable) Local Plan Pattern 99 System Plan Plan 99 WLK FDW NOT USED MIN Emergency vehicle pre-emption 3: EXT NOT USED MAX1 Serve NSG/NSDW min 20 secs and up to 100 MAX2 secs if there are continuous emergency calls in AMB NS direction. ALR SPLIT 2. Southbound WLK FDW Fixed MIN 40 EXT 0 EB and WB phases are callable and skippable but not switchable. If EB and WB detectors are MAX1 40 MAX2 120 both active at the end of the NS phase, the WB AMB 5.0 phase is served first followed by the EB phase. ALR 3.5 If only the EB detector is active at the end of Jane Street SPLIT the NS phase, only the EB phase is served (and any late WB demand will only be served the following cycle). EB and WB phases are 3. Westbound WLK only permitted once per cycle. FDW MIN 10 EXT MAX1 40 MAX2 40 AMB 4.5 ALR Kirby Road SPLIT 4. Eastbound WLK FDW Callable by stopbar loop MIN 10 and/or pushbutton; EXT Extendable by stopbar loop. MAX1 40 MAX2 40 AMB 4.5 ALR 2.0 Kirby Road SPLIT WLK FDW MIN EXT NOT USED MAX1 NOT USED MAX2 AMB ALR SPLIT 6. Northbound WLK FDW Fixed MIN 40 EXT Ω MAX1 40 MAX2 120 AMB 5.0 ALR Jane Street SPLIT LEGEND: WLK SA - Semi-Actuated signal FDW WLK - Walk time MIN FDW - Flashing Don't Walk time MIN - Minimum green time EXT Not Used NOT USED MAX1 EXT - Extension time MAX2 MAX1 - Maximum green time 1 MAX2 - Maximum green time 2 AMB AMB - Amber ALR SPLIT ALR -All Red CL - Cycle Length OF - Offset WLK VP - Vehicle Permissive FDW NSWK - North/South Walk EWWK - East/West Walk MIN FXT Not Used NOT USED NSG - North/South Green MAX1 EWG - East/West Green MAX2 NSFD - North/South Flashing Don't Walk EWFD - East/West Flashing Don't Walk AMB TSP - Transit Priority APS - Audible Pedestrian Signal ALR SPLIT RLC - Red Light Camera CL 0 (FREE) OF 0 (FREE) VΡ 0 (FREE)

LOCATION: Hwy 400 SB Offramp & Major Mackenzie Dr (YR25) 442 (MTO Signal) CTCS: MODE/COMMENT: SA PREPARED/CHECKED BY: ML

June 19,2020

PREPARATION DATE:

IMPLEMENTATION DATE:

MUNICIPALITY: Vaughan COMPUTER SYSTEM: Centracs CONTROLLER/CABINET TYPE: Econolite Cobalt / TS2T1

CONFLICT FLASH: Red & Red

DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s)

CHANNEL/DROP:

| IMPLEMENTATION DATE: | June 19,2020 | | | | | | CHANNEL/DROP: | |
|-------------------------------------|---|---|--------------------------------------|--|--|--|--|---|
| NEMA Phase (MTO) | Normal Time | | AM 6:00-10:00 M-F Pattern 1 | PM 16:00- 19:00 M-F Pattern 2 | OFF 10:00-16:00, 19:00- 22:00 M-F,10:00- 22:00 Sat & Sun Pattern 3 | Free 22:00-6:00 M-F, 22:00-10:00 Sat &Sun Pattern 99 | Phase Mode (Fixed/Demanded/Callable) | Remarks |
| 1. W/B Left Turn Arrow | | | Plan 1 | Plan 2 | Plan 3 | Plan 99 | | Pedestrian Minimums: |
| I. W/B Left Yulli/Willow | WLK FDW MIN 7 | 7 | | | | | Callable/Extendable during | EWWK = 7 sec., EWFD = 21sec. |
| | EXT 3 MAX1 10 | 3 10 | | | | | Normal Time & Veh Min Recall during Pre-Time | Emergency vehicle pre-emption 3/4: |
| | MAX2 0 AMB 3 ALR 1 | 0 3 1 | | | | | Recall during Pre-Time | Serve EWG/EWDW min 20 secs and up to 100 secs if there are continuous emergency calls in EW direction. |
| 2. Eastbound | SPLIT | | 12 | 12 | 12 | 0 | | |
| | WLK 7 FDW 21 MIN 20 EXT 4 MAX1 60 MAX2 0 AMB 4.5 ALR 2.5 | 7 21 45 4 50 0 4.5 2.5 | | | | | Callable/Extendable during Normal Time & Veh Max Recall during Pre-Time | SB phase is callable by vehicle or pedestrian actuation. If a vehicle call is received, the minimum SBG is 10 seconds. If ongoing vehicle demand exists on the stopbar loop, the SBG is capable of providing vehicle extensions up to the maximum green. If a pedestrian call |
| Major Mackenzie Dr 3. Northbound | SPLIT | | 78 | 68 | 48 | 0 | | is received, the pedestrian minimum will be served. The NSWK & NSFD are only |
| 3. Northbound | WLK FDW MIN 10 EXT 2 MAX1 25 MAX2 0 AMB 4.5 ALR 3 | 10 2 25 0 4.5 3 | | | | | Callable/Extendable during Normal Time & Veh Min Recall during Pre-Time | displayed on the pedestrian signal heads if a pedestrian call is received. Extension time is based on vehicle demand. During coordinated operation, the signal constantly cycles through main street |
| | SPLIT | Ů | 19 | 19 | 19 | 0 | | FDW to improve response time to side |
| 4. Southbound | WLK 7 FDW 25 MIN 10 EXT 2 MAX1 25 MAX2 0 | 7 25 15 2 30 0 | | | | | Callable/Extendable during Normal Time & Veh Min Recall during Pre-Time 10 secs delay | street vehicle and pedestrian demand. During free plan, signal rests in EWWK and does not cycle through EWFD unless there is side street vehicle or pedestrian demand. |
| Hwy 400 SB Offramp | AMB 4.0 ALR 3.0 SPLIT | 4.5 3.0 | 41 | 41 | 41 | 0 | | EWFD reverts to EWWK if there is no side street demand at the end of the EWFD. |
| NOT USED | WLK FDW MIN EXT MAX1 MAX2 AMB ALR SPLIT | | | | | | | |
| 6. Westbound | WLK 7 FDW 21 MIN 20 EXT 4 MAX1 60 MAX2 0 AMB 4.5 ALR 2.5 | 7 21 45 4 50 0 4.5 2.5 | | | | | Callable/Extendable during Normal Time & Veh Max Recall during Pre-Time | |
| Major Mackenzie Dr 7. | SPLIT | | 90 | 80 | 60 | 0 | | LEGEND: |
| NOT USED 8. Northbound | WLK FDW MIN EXT MAX1 MAX2 AMB ALR SPLIT | | | | | | | SA - Semi-Actuated signal WLK - Walk time FDW - Flashing Don't Walk time MIN - Minimum green time EXT - Extension time MAX1 - Maximum green time 1 MAX2 - Maximum green time 2 AMB - Amber |
| o. INOLUIDOUNA | WLK | | | | | | | ALR -All Red |
| NOT USED | FDW MIN EXT MAX1 MAX2 AMB ALR SPLIT | | | | | 0 | | CL - Cycle Length OF - Offset VP - Vehicle Permissive NSWK - North/South Walk EWWK - East/West Walk NSG - North/South Green EWG - East/West Green NSFD - North/South Flashing Don't Walk |
| | CL | | 150 | 140 | 120 | 0 (FREE) | | EWFD - East/West Flashing Don't Walk |
| | OF VP | | 20 21 | 20 21 | 0 21 | 0 (FREE) 0 (FREE) | | TSP - Transit Priority APS - Audible Pedestrian Signal |

Teston Rd (YR 49) & Jane St. (YR 55) LOCATION MUNICIPALITY: Vaughan COMPUTER SYSTEM: Centracs MODE/COMMENT: SΑ CONTROLLER/CABINET TYPE: Econolite ASC/3-1000 / TS2T1 PREPARED/CHECKED BY: M.L. CONFLICT FLASH: Red & Red PREPARATION DATE: DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s IMPLEMENTATION DATE June 18, 2019 CHANNEL/DROP: OFF 10:00-15:00, Phase Mode 22:00-6:00 M-F 6:00-10:00 5:00-20:00 20:00-22:00 & 22:00-9:00 Remarks M-F M-F; & 9:00-NEMA Phase (York) Fixed/Demanded/Callable) 2:00 Sat & Sur Local Plan Changes were made due to closure at Major Mackeinzie Drive and McNaughtor System Plan Plan 1 Plan 2 Plan 99 Plan 3 Road 1. N/B Left Turn Arrow Pedestrian Minimums: NSWK = 7 sec., NSFD = 27 sec. WLK FDW Permissive/Protected EWWK = 7 sec., EWFD = 25 sec. MIN Callable/Extendable Emergency vehicle pre-emption 3: EXT by Setback Loop MAX1 20 Serve NSG/NSDW min 20 secs and up to MAX2 0 100 secs if there are continuous AMB 3 emergency calls in NS direction. ALR SPLIT 12 12 12 0 Emergency vehicle pre-emption 4: Southbound WLK Serve EWG/EWDW min 20 secs and up FDW 27 Fixed to 100 secs if there are continuous emergency calls in EW direction. MIN 35 EXT 0 MAX1 35 MAX2 0 AMB 4.5 EW phase is callable by vehicle or pedestrian actuation. If a vehicle call is ALR 3.0 Jane St. SPLIT 50 received, the minimum EWG is 10 3. W/B Left Turn Arrow seconds. If ongoing vehicle demand exists on the stopbar loop, the EWG is wı ĸ Permissive/Protected capable of providing vehicle extensions up to the maximum green Free operation FDW MIN Callable/Extendable by Setback Loop EXT If a pedestrian call is received, the MAX1 MAX2 nedestrian minimum will be served. The 7 EWWK & EWFD are only displayed on 0 AMB the pedestrian signal heads if a 3 AI R nedestrian call is received. Extension time is based on vehicle demand. SPLIT 25 20 12 0 Unused extension time is given to the 4. Eastbound NSG. FDW 25 Callable by stopbar loop 10 MIN and/or pushbutton: EXT Extendable by stopbar loop 3 During coordinated operation, the signal MAX1 35 constantly cycles through main street MAX2 0 FDW to improve response time to side AMB 5.5 street vehicle and pedestrian demand. ALR 3.0 55 68 53 0 Teston Rd During free plan, signal rests in NSWK 5. S/B Left Turn Arrow and does not cycle through NSFD unless WLK there is side street vehicle or pedestrian FDW demand. MIN FXT NOT USED MAX1 NSFD reverts to NSWK if there is no side MAX2 street demand at the end of the NSFD. AMB ALR SPLI 6. Northbound WI K FDW 27 Fixed MIN 35 EXT 0 MAX1 35 MAX2 0 AMB 4.5 AI R 3.0 70 62 65 0 SPLIT Jane St. LEGEND: Eastbound Left Turn Arro WLK SA - Semi-Actuated signal FDW WLK - Walk time MIN Permissive/Protected FDW - Flashing Don't Walk time EXT Callable/Extendable MIN - Minimum green time MAX1 20 by Setback Loop EXT - Extension time MAX2 0 MAX1 - Maximum green time 1 AMB 3 MAX2 - Maximum green time 2 ALR AMB - Amber SPLIT 12 20 12 0 ALR -All Red CL - Cycle Length 8. Westbound OF - Offset WLK VP - Vehicle Permissive Callable by stopbar loop FDW 25 NSWK - North/South Walk EWWK - East/West Walk MIN 10 and/or pushbutton: EXT Extendable by stopbar loop 3 NSG - North/South Green MAX1 35 EWG - East/West Green MAX2 ٥ NSFD - North/South Flashing Don't Walk EWFD - East/West Flashing Don't Walk AMB 5.5 ALR 3.0 TSP - Transit Priority Teston Rd SPLI 53 APS - Audible Pedestrian Signal RLC - Red Light Camera 150 CL 150 130 0 (FREE) OF 0 (FREE) 35 VΡ 27 27 27 0 (FREE)

Major Mackenzie Drive (YR 25) & Dufferin St (YR 55)

CTCS: MODE/COMMENT: SA PREPARED/CHECKED BY: PREPARATION DATE:

LOCATION

118 M.L.

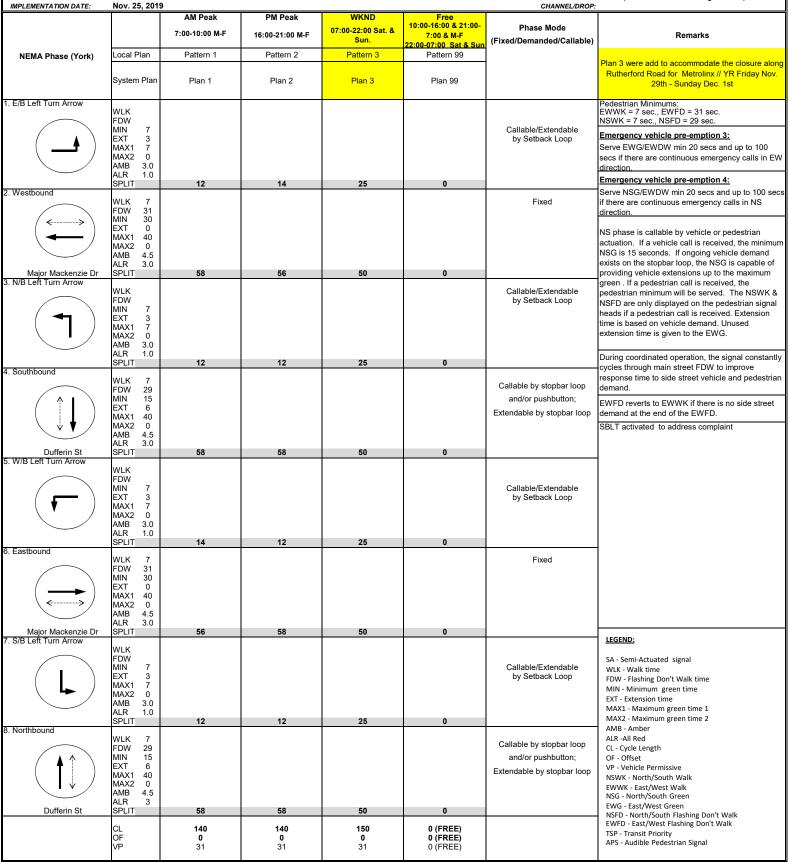
MUNICIPALITY: Richmond Hill COMPUTER SYSTEM: Centracs

CONTROLLER/CABINET TYPE: Econolite Cobalt / TS2T1 CONFLICT FLASH: Red & Red

DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s)

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CHANNEL/DROP



| LOCATION: CTCS: | Keele St (YR 490 | (6) & Testo | n Road (Y | R 49) | | MUNICIPALITY: COMPUTER SYSTEM: | Centracs | |
|---|--|---------------------|---------------------|--|---|--|---|--|
| MODE/COMMENT: PREPARED/CHECKED BY: PREPARATION DATE: IMPLEMENTATION DATE: | SA M.L. June 26,201 | 9 | | | | CONTROLLER/CABINET TYPE: CONFLICT FLASH: DESIGN WALK SPEED: CHANNEL/DROP: | | |
| IIII EEIIENTATION DATE. | 04.10 20,20 1 | AM | PM | OFF | Free | Phase Mode | | |
| NEMA Phase (York) | | 6:00-10:00 M-F | 15:00- 20:00 M-F | 10:00-15:00, 20:00-22:00 M-F; & 9:00- 22:00 Sat & | 22:00-6:00 M-F & 22:00-9:00 Sat&Sun | | Remarks | |
| | Local Plan System Plan | Pattern 1 Plan 1 | Pattern 2 Plan 2 | Sun Pattern 3 Plan 3 | Pattern 99 Plan 99 | (Fixed/Demanded/Callable) | Changes were made due to closure at Major Mackeinzie Drive and McNaughton Road | |
| 1. N/B Left Turn Arrow | WLK | i idii i | Tiuitz | 1 Idii 0 | 1 1011 00 | | Pedestrian Minimums: NSWK = 7 sec., NSFD = 21 sec. | |
| | FDW | | | | | Callable/Extendable | EWWK = 7 sec., NSPD = 21 sec. | |
| | MIN 7 EXT 3 | | | | | by Setback Loop | Emergency vehicle pre-emption 3: | |
| | MAX1 7 MAX2 0 AMB 3 ALR 1 | | | | | | Serve NSG/NSDW min 20 secs and up to 100 secs if there are continuous emergency calls in NS direction. | |
| 2. Southbound | SPLIT | 20 | 37 | 20 | 0 | | Emergency vehicle pre-emption 4: | |
| | WLK 7 FDW 21 MIN 30 EXT 0 MAX1 30 MAX2 0 | | | | | Fixed | Serve EWG/EWDW min 20 secs and up to 100 secs if there are continuous emergency calls in EW direction. | |
| | AMB 4.0 ALR 3.5 | | | | | | | |
| Keele Street 3.W/B Left Turn Arrow | SPLIT | 73 | 38 | 47 | 0 | | | |
| | WLK FDW MIN 7 EXT 3 MAX1 7 MAX2 0 | | | | | Callable/Extendable by Setback Loop | | |
| | AMB 3 ALR 1 SPLIT | 12 | 14 | 12 | 0 | | | |
| 4. Eastbound | WLK 7 | | | | | | | |
| | FDW 22 MIN 10 EXT 3 MAX1 40 MAX2 0 AMB 4.5 ALR 3.0 | | | | | Fixed | | |
| Teston Road | SPLIT | 45 | 61 | 51 | 0 | | | |
| NOT USED | WLK FDW MIN EXT MAX1 MAX2 AMB ALR SPLIT | 0 | 0 | 0 | 0 | | | |
| 6. Northbound | WLK 7 | | | | | | | |
| | FDW 21 MIN 30 EXT 0 MAX1 30 MAX2 0 AMB 4.0 ALR 3.5 | | | | | Fixed | | |
| Keele Street 7. E/B Left Turn Arrow | SPLIT | 93 | 75 | 67 | 0 | 0 11 (5) 1 11 | LEGEND: | |
| | WLK FDW MIN 7 EXT 3 MAX1 7 MAX2 0 AMB 3 ALR 1 | | | | | Callable/Extendable by Setback Loop | SA - Semi-Actuated signal WLK - Walk time FDW - Flashing Don't Walk time MIN - Minimum green time EXT - Extension time MAX1 - Maximum green time 1 MAX2 - Maximum green time 2 AMB - Amber | |
| 8. Westbound | SPLIT | 17 | 37 | 20 | 0 | | ALR -All Red CL - Cycle Length | |
| Teston Road | WLK 7 FDW 22 MIN 10 EXT 3 MAX1 40 MAX2 0 AMB 4.5 ALR 3.0 SPLIT | 40 | 38 | 43 | 0 | Fixed | CL - Cycle Lengtn OF - Offset VP - Vehicle Permissive NSWK - North/South Walk EWWK - East/West Walk NSG - North/South Green EWG - East/West Green NSFD - North/South Flashing Don't Walk EWFD - East/West Flashing Don't Walk TSP - Transit Priority APS - Audible Pedestrian Signal RLC - Red Light Camera | |
| 103ion Road | CL | 150 | 150 | 130 | 0 (FREE) | | | |
| | OF VP | 0 21 | 120 21 | 0 21 | 0 (FREE) 0 (FREE) 0 (FREE) | | | |

LOCATION Teston Road (YR 49) & Dufferin Street (YR 53) MUNICIPALITY: Vaughan CTCS 706 COMPUTER SYSTEM: Centracs MODE/COMMENT: SA with APS CONTROLLER/CABINET TYPE: Econolite Cobalt / TS2T1 PREPARED/CHECKED BY: AM CONFLICT FLASH: Red & Red PREPARATION DATE: DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s) IMPLEMENTATION DATE: October 22, 2019 CHANNEL/DROP AM ΡМ Free **Phase Mode** 10:00- 16:00; & 7:00-10:00 16:00-20:00 20:00-7:00 M-F Remarks **NEMA Phase (York)** M-F M-F ; Free Sat. & Sun (Fixed/Demanded/Callable) Local Plan Local Plan Pattern 1
System Plan Plan 1 Pattern 2 Pattern 99 Plan 2 Plan 99 Pedestrian Minimums NSWK=7 sec, NSDW= 19sec WLK FDW EWWK=7 sec, EWDW= 19sec MIN Emergency vehicle pre-emption 3: EXT NOT USED MAX1 Serve NSG/NSDW min 20 secs and up to 100 MAX2 secs if there are continuous emergency calls in AMB NS direction ALR 0 0 **SPLIT** 0 Emergency vehicle pre-emption 4: Southbound WLK Serve EWG/EWDW min 20 secs and up to 100 FDW 19 Fixed secs if there are continuous emergency calls in MIN 30 EW direction. EXT MAX1 6 50 APS Extended Push Activation = 3 sec When MAX2 60 activated, APS is on for 7 seconds. AMB 4.5 M modified due to complaint ALR 2.5 70 104 **Dufferin Street** SPLIT 0 3.W/B Left Turn Arrow WLK Callable/Extendable FDW by Stopbar Loop MIN EXT 30 45 MAX1 MAX2 AMB 3 ALR SPLIT 36 12 0 4. Eastbound WLK FDW MIN 19 Callable by stopbar loop 10 and/or pushbutton; Extendable by stopbar loop. FXT 3 40 MAX1 MAX2 65 4.5 AMB ALR 2.5 Teston Road SPLIT 34 34 0 S/B Left Turn Arrow WLK Callable/Extendable FDW MIN by Setback Loop **EXT** 3 MAX1 12 MAX2 20 AMB 3 AI R SPLIT 12 12 6. Northbound WLK FDW 19 Fixed MIN 30 EXT 6 MAX1 MAX2 50 60 AMB 4.5 ALR 2.5 **Dufferin Street** SPLIT 58 92 0 LEGEND: '. E/B Left Turn Arrow WLK Callable/Extendable FDW MIN by Stopbar Loop SA - Semi-Actuated signal 7 WLK - Walk time EXT FDW - Flashing Don't Walk time MAX1 30 MIN - Minimum green time MAX2 45 EXT - Extension time AMB MAX1 - Maximum green time 1 ALR MAX2 - Maximum green time 2 12 SPLIT 36 0 AMB - Amber 8. Westbound ALR -All Red WLK FDW 19 Callable by stopbar loop CL - Cycle Length MIN 10 and/or pushbutton; OF - Offset EXT 3 Extendable by stopbar loop. VP - Vehicle Permissive MAX1 40 NSWK - North/South Walk MAX2 65 EWWK - East/West Walk AMB 4.5 NSG - North/South Green ALR 2.5 EWG - East/West Green SPLIT Teston Road 34 34 NSFD - North/South Flashing Don't Walk EWFD - East/West Flashing Don't Walk 0 (FREE) 140 150 TSP - Transit Priority OF 120 0 (FREE) APS - Audible Pedestrian Signal VΡ 19 19 0 (FREE)

NOTES

Bathurst Street (YR 38) & Elgin Mills Road/Teston Rd (R49) LOCATION MUNICIPALITY: Vaughan 168 COMPUTER SYSTEM: Centracs CTCS: MODE/COMMENT: CONTROLLER/CABINET TYPE: Econolite ASC3 / TS2T1 PREPARED/CHECKED BY: AM CONFLICT FLASH: Red & Red PREPARATION DATE November 26, 2019 DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s) November 26, 2019 IMPLEMENTATION DATE: Phase Mode 10:00-16:00: 22:00-6:00 M-F. and 6:00-10:00 9:00-22:00 M-F; 22:00-9:00Sat. & Sun Remarks NEMA Phase (York) M-F 09:00-22:00 Sat (Fixed/Callable) Local Plan Pattern 1 Pattern 2 Pattern 3 Pattern 99 Plan 2 Plan 3 System Plan Plan 1 Plan 99 Pedestrian Minimums WLK NSWK= 7sec, NSFD= 25sec EWWK= 7 sec, EWFD= 28 sec FDW Emergency vehicle pre-emption 3: EXT NOT USED MAX1 Serve NSG/NSFD min 20 secs and up to 100 secs MAX2 there are continuous emergency calls in NS AMB direction. ALR SPLIT Emergency vehicle pre-emption 4: 2. Southbound WLK Serve EWG/EWFD min 20 secs and up to 100 sec FDW Fixed if there are continuous emergency calls in EW MIN 30 EXT MAX1 30 EW phase is callable by vehicle or pedestrian MAX2 actuation. If a vehicle call is received, the minimun EWG will be served. If ongoing vehicle demand exists on the stopbar loop, the EWG is capable of AMB 5.0 ALR 3.0 providing vehicle extensions up to the maximum 78 Bathurst Stree green split. If a pedestrian call is received, the W/B Left Turn Arrow pedestrian minimum will be served. The EWWK & WLK Callable/Extendable EWFD are only displayed on the pedestrian signal heads if a pedestrian call is received. Extension time FDW MIN by Stopbar Loop is based on vehicle demand. Unused extension time EXT is given to the NSG. MAX1 MAX2 AMB 3.0 AI R 12 12 12 SPLIT During coordinated operation, the signal constantly . Eastbound cycles through main street FDW to improve WLK response time to side street vehicle and pedestrian FDW 28 Callable by stopbar loop MIN 10 and/or pushbutton; EXT Extendable by stopbar loop MAX1 25 During free plan, signal rests in NSWK and does not MAX2 cycle through NSFD unless there is side street 0 AMB 4.5 vehicle or pedestrian demand. AI R 3.5 Teston Rd SPLIT 5. S/B Left Turn Arrow NSFD reverts to NSWK if there is no side street WLK lemand at the end of the NSFD. FDW Callable/Extendable MIN by Setback Loop EXT MAX1 MAX2 0 AMB 3 SPLI 12 12 12 6. Northbound WLK FDW 25 Fixed MIN 30 EXT 0 MAX1 30 MAX2 AMB 5 ALR 3 Bathurst Street SPLIT 82 66 LEGEND: . E/B Left Turn Arrow WIK SA - Semi-Actuated signal FDW FA - Fully Actuated signal MIN Callable/Extendable WLK - Walk time EXT by Setback Loop FDW - Flashing Don't Walk time MAX1 7 MIN - Minimum green time MAX2 0 EXT - Extension time AMB MAX1 - Maximum green time 1 AI R MAX2 - Maximum green time 2 AMB - Amber 12 12 SPLIT Westbound ALR -All Red CL - Cycle Length WLK OF - Offset FDW 28 Callable by stopbar loop VP - Vehicle Permissive MIN 10 and/or pushbutton: NSWK - North/South Walk EXT Extendable by stopbar loop EWWK - East/West Walk MAX1 25 NSG - North/South Green MAX2 0 EWG - East/West Green AMB 4.5 NSFD - North/South Flashing Don't Walk ALR 3.5 EWFD - East/West Flashing Don't Walk Elgin Mills Road SPLIT TSP - Transit Signal Priority APS - Audible Pedestrian Signal CL 150 0 (FREE) 140 120 RLC - Red Light Camera OF VP 60 0 (FREE) 25 25 25 0 (FREE)

LOCATION: Dufferin St (YR 53) & Kirby Rd
CTCS: 697

MODE/COMMENT: SA with APS
PREPARED/CHECKED BY: AM/JL
PREPARATION DATE: August 19, 2019
IMPLEMENTATION DATE: November 4, 2019

MUNICIPALITY: Vaughan
COMPUTER SYSTEM: Centracs
CONTROLLER/CABINET TYPE: Econolite Cobalt / TS2T1
CONFLICT FLASH: Red & Red
DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s)

| IMPLEMENTATION DATE: | November 4 | | | | | |
|------------------------------|---|----------------------------------|---------------------------------------|---|--|---|
| NEMA Phase (York) | Local Plan | 07:00- 10:00 M-F Pattern 1 | PM 16:00-20:00 M-F Pattern 2 | Free 10:00-16:00, 20:00 7:00 M-F & Sat-Sun Pattern 99 | Phase Mode (Fixed/Demanded/Callable) | Remarks |
| 1. N/B Left Turn Arrow | System Plan | | Plan 2 | Plan 99 | | Pedestrian Minimums: |
| | WLK FDW | | | | Permissive/Protected Callable/Extendable | NSWK = 7 sec., NSFD = 15 sec. EWWK = 7 sec., EWFD = 15 sec. |
| | MIN 7 EXT 3 | | | | by Setback Loop | Emergency vehicle pre-emption 3: |
| | MAX1 7 MAX2 0 AMB 3 ALR 1 | | | | | Serve NSG/NSFD min 20 secs and up to 100 secs if there are continuous emergency calls in NS direction. |
| 2. Southbound | SPLIT | 0 | 0 | 0 | | Emergency vehicle pre-emption 4: |
| | WLK 7 FDW 15 MIN 30 EXT 0 MAX1 30 | | | | Fixed | Serve EWG/EWFD min 20 secs and up to 100 secs if there are continuous emergency calls in NS direction. |
| Dufforin St | MAX2 0 AMB 5.0 ALR 3.0 SPLIT | 100 | 00 | 0 | | EW phase is callable by vehicle or pedestrian actuation. If a vehicle call is received, the minimum EWG will be |
| Dufferin St 3. | WLK | 100 | 90 | U | | serviced. If ongoing vehicle demand exists on the stopbar loop, the EWG is |
| NOT USED | FDW MIN EXT MAX1 MAX2 AMB ALR SPLIT | | | | | capable of providing vehicle extensions up to the maximum green split. If a pedestrian call is received, the pedestrian minimum will be served. The EWWK & EWFD are only displayed on the pedestrian signal heads if a pedestrian call is received. Extension time is based |
| 4. Eastbound | WLK 7 | | | | | on vehicle demand. Unused extension time is given to the NSG during |
| | FDW 15 MIN 10 | | | | Callable by stopbar loop and/or pushbutton; | coordinated opeation. |
| | EXT 3 MAX1 30 MAX2 0 AMB 4.5 ALR 2.0 | | | | Extendable by stopbar loop. | During coordinated operation, the signal constantly cycles through main street FDW to improve response time to side street vehicle and pedestrian demand. |
| Kirby Rd 5. | SPLIT | 40 | 50 | 0 | | During free plan, signal rests in NSWK |
| NOT USED | WLK FDW MIN EXT MAX1 MAX2 AMB ALR | | | | | and does not cycle through NSFD unless there is side street vehicle or pedestrian demand. NSFD reverts to NSWK if there is no side street demand at the end of the NSFD. APS Extended Push Activation = 3 |
| 6 Northhound | SPLIT | | | | | sec When activated, APS is on for 7 |
| Dufferin St | WLK FDW MIN 30 EXT 0 MAX1 30 MAX2 0 AMB 5.0 ALR 3.0 SPLIT | 100 | 90 | 0 | Fixed | seconds. |
| 7. | WLK | | | | | LEGEND: SA - Semi-Actuated signal |
| NOT USED | FDW MIN EXT MAX1 MAX2 AMB ALR SPLIT | | | | | FA - Fully-Actuated signal WLK - Walk time FDW - Flashing Don't Walk time MIN - Minimum green time EXT - Extension time MAX1 - Maximum green time 1 MAX2 - Maximum green time 2 |
| Westbound(ped only) | WLK 7 | | | | | AMB - Amber ALR -All Red |
| * | FDW 15 MIN 10 EXT 3 MAX1 30 MAX2 0 AMB 4.5 ALR 2.0 SPLIT | | | | Callable by pushbutton | CL - Cycle Length OF - Offset VP - Vehicle Permissive NSWK - North/South Walk EWWK - East/West Walk NSG - North/South Green EWG - East/West Green NSED - North/South Flashing Don't Walk |
| | CL OF VP | 140 0 15 | 140 0 15 | 0 (FREE) 0 (FREE) 0 (FREE) | | NSFD - North/South Flashing Don't Walk EWFD - East/West Flashing Don't Walk TSP - Transit Signal Priority APS - Audible Pedestrian Signal RLC - Red Light Camera |
| NOTES: T Intersection (No Ea | 1 | 1 | l | l | l | |

NOTES: T Intersection (No East Leg)

Bathurst Street (YR 38) & Gamble Road / LOCATION: Kirby Road (YR 29) MUNICIPALITY: Vaughan CTCS: 534 COMPUTER SYSTEM: Centracs MODE/COMMENT: SA CONTROLLER/CABINET TYPE: Econolite ASC3 / TS2T1 PREPARED/CHECKED BY: M.L./J.L. CONFLICT FLASH: Red & Red Aug 20, 2019 September 17, 2019 PREPARATION DATE: DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s) IMPLEMENTATION DATE: Free Phase Mode Remarks 24 Hrs Daily **NEMA Phase (York)** (Fixed/Callable) Local Plan Pattern 99 System Plan Plan 99 Pedestrian Minimums WLK NSWK= 7sec, NWFD= 28sec FDW EWWK=7sec, NSFD= 24sec Emergency vehicle pre-emption 3: EXT NOT USED MAX1 Serve NSG/NSFD min 20 secs and up to 100 secs MAX2 if there are continuous emergency calls in NS AMB direction. ALR SPLIT Emergency vehicle pre-emption 4: 2. Southbound WLK Serve EWG/EWFD min 20 secs and up to 100 FDW 28 Fixed secs if there are continuous emergency calls in MIN 50 EW direction. EXT 0 MAX1 50 MAX2 0 AMB 5.0 ALR 2.5 **Bathurst Street** SPLIT WIK FDW MIN EW phase is callable by vehicle or pedestrian EXT MAX1 NOT USED actuation. If a vehicle call is received, the ninimum EWG will be served. If ongoing vehicle MAX2 demand exists on the stopbar loop, the EWG is AMB capable of providing vehicle extensions up to the maximum green split. If a pedestrian call is received, the pedestrian minimum will be served. ALR SPLIT 4. Eastbound The EWWK & EWFD are only displayed on the WLK pedestrian signal heads if a pedestrian call is received. Extension time is based on vehicle FDW 24 Callable by stopbar loop MIN 10 demand. Unused extension time is given to the and/or pushbutton: EXT Extendable by stopbar loop NSG during coordinated operation. MAX1 40 MAX2 Ω Split Phase During coordinated operation, the signal constantly AMB 4.5 cycles through main street FDW to improve ALR response time to side street vehicle and pedestriar Kirby Road SPLIT 5. S/B Left Turn Arrow WLK FDW Callable/Extendable MIN by Stopbar Loop During free plan, signal rests in NSWK and does EXT not cycle through NSFD unless there is side street 3 7 MAX1 vehicle or pedestrian demand. MAX2 0 AMB ALR NSFD reverts to NSWK if there is no side street SPLIT demand at the end of the NSFD. 6. Northbound WLK FDW 28 Fixed MIN 50 EXT 0 MAX1 50 MAX2 0 AMB ALR 2.5 Bathurst Street SPLIT LEGEND: WLK FDW SA - Semi-Actuated signal MIN FA - Fully -Actuated signal WLK - Walk time EXT NOT USED MAX1 FDW - Flashing Don't Walk time MIN - Minimum green time MAX2 AMB EXT - Extension time ALR MAX1 - Maximum green time 1 SPLIT 0 MAX2 - Maximum green time 2 8. Westbound AMB - Amber WLK ALR -All Red FDW MIN 24 10 Callable by stopbar loop CL - Cycle Length OF - Offset and/or pushbutton: VP - Vehicle Permissive EXT Extendable by stopbar loop NSWK - North/South Walk MAX1 40 FWWK - Fast/West Walk Split Phase MAX2 0 NSG - North/South Green AMB 4.5 EWG - East/West Green ALR NSFD - North/South Flashing Don't Walk Gamble Road SPLIT EWFD - East/West Flashing Don't Walk TSP - Transit Signal Priority 0 (FREE) APS - Audible Pedestrian Signal OF 0 (FREE) RLC - Red Light Camera VΡ 0 (FREE)

LOCATION Keele St (YR 6) & Kirby Road MUNICIPALITY: Vaughan CTCS: 633 COMPUTER SYSTEM: Centracs CONTROLLER/CABINET TYPE: Econolite Cobalt / TS2T1 MODE/COMMENT: SA PREPARED/CHECKED BY: CONFLICT FLASH: Red & Red M.L. PREPARATION DATE: DESIGN WALK SPEED: 1.0 m/s (FDW based on full crossing at 1.2 m/s March 24, 2020 IMPLEMENTATION DATE: CHANNEL/DROP: AM PM Free Phase Mode 19:00-6:30 M-F 6:30-09:30, M-F 16:00-19:00 Remarks & all day NEMA Phase (York) Sat&Sun (Fixed/Demanded/Callable) Local Plan Pattern 99 Pattern 1 System Pla Plan 1 Plan 2 Plan 99 edestrian Minimums: WLK NSWK=7 sec, NSFD=18sec FDW EWWK=7sec, EWFD=21sec MIN Emergency vehicle pre-emption 3: EXT NOT USED MAX1 Serve EWG/EWDW min 20 secs and up MAX2 to 100 secs if there are continuous AMB emergency calls in EW direction. ALR SPLIT 2. Southbound WI K FDW 18 Fixed MIN 30 EXT MAX1 30 MAX2 0 AMB 5.0 ALR 2.5 80 Keele St SPLIT 80 WLK FDW MIN EXT NOT USED MAX1 MAX2 AMB ALR SPLIT 4. Eastbound WLK FDW 21 MIN 10 Callable by stobarloop and or EXT 3 push button ;Extendable by MAX1 19 stopbar loop MAX2 0 AMB 4.5 ALR 2.5 SPLIT Kirby WLK FDW MIN EXT NOT USED MAX1 MAX2 AMB ALR SPLIT 0 0 6. Northbound WLK FDW 18 Fixed MIN 30 EXT 0 MAX1 30 0 MAX2 AMB 5.0 ALR 2.5 Keele St SPLIT 80 LEGEND: WLK SA - Semi-Actuated signal FDW WLK - Walk time FDW - Flashing Don't Walk time MIN - Minimum green time MIN EXT NOT USED MAX1 EXT - Extension time MAX2 MAX1 - Maximum green time 1 AMB MAX2 - Maximum green time 2 AMB - Amber ALR ALR -All Red CL - Cycle Length SPLI 8. Westbound OF - Offset VP - Vehicle Permissive WI K FDW 21 NSWK - North/South Walk MIN 10 EWWK - East/West Walk EXT MAX1 3 19 Callable by stobarloop and or NSG - North/South Green EWG - East/West Green push button ;Extendable by MAX2 0 NSFD - North/South Flashing Don't Walk EWFD - East/West Flashing Don't Walk stopbar loop AMB 4.5 TSP - Transit Priority APS - Audible Pedestrian Signal AI R 2.5 Kirby SPLIT 40 40 RLC - Red Light Camera 0 (FREE) 120 120 OF **0** 18 0 (FREE) 0 VP 18 0 (FREE) NOTES:

Appendix C: Synchro Results for Existing Conditions (2020)

| | ۶ | → | * | • | + | • | 4 | 1 | ~ | - | ↓ | 4 |
|-----------------------------------|-------|----------|-------|-------|-------------|------------|---------|------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ¥ | 44 | 7 | * | * 1> | | 44 | | 7 | | 4 | |
| Traffic Volume (vph) | 0 | 739 | 444 | 701 | 634 | 3 | 56 | 0 | 343 | 0 | 3 | 1 |
| Future Volume (vph) | 0 | 739 | 444 | 701 | 634 | 3 | 56 | 0 | 343 | 0 | 3 | 1 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | 1.0 | 5.0 | | 5.0 | | 5.0 | | 1.0 | |
| Lane Util. Factor | | 0.95 | 1.00 | 1.00 | 0.95 | | 0.97 | | 1.00 | | 1.00 | |
| Frpb, ped/bikes | | 1.00 | 0.99 | 1.00 | 1.00 | | 1.00 | | 1.00 | | 1.00 | |
| Flpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | | 1.00 | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | | 0.85 | | 0.97 | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 3318 | 1463 | 1630 | 3258 | | 2603 | | 1420 | | 1856 | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | | 1.00 | |
| Satd. Flow (perm) | | 3318 | 1463 | 1630 | 3258 | | 2603 | | 1420 | | 1856 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 0 | 762 | 458 | 723 | 654 | 3 | 58 | 0 | 354 | 0 | 3 | 1 |
| RTOR Reduction (vph) | 0 | 0 | 222 | 0 | 0 | 0 | 0 | 0 | 323 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 0 | 762 | 236 | 723 | 657 | 0 | 58 | 0 | 31 | 0 | 3 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | | | | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Heavy Vehicles (%) | 0% | 10% | 10% | 12% | 12% | 0% | 36% | 0% | 15% | 0% | 0% | 0% |
| Turn Type | Perm | NA | Perm | Prot | NA | | Prot | | Perm | | NA | |
| Protected Phases | | 6 | | 5 | 2 | | 8 | | | | 7 | |
| Permitted Phases | 6 | | 6 | | | | | | 8 | 7 | | |
| Actuated Green, G (s) | | 53.1 | 53.1 | 64.2 | 121.3 | | 12.5 | | 12.5 | | 1.2 | |
| Effective Green, g (s) | | 55.1 | 55.1 | 67.2 | 123.3 | | 13.5 | | 13.5 | | 5.2 | |
| Actuated g/C Ratio | | 0.36 | 0.36 | 0.44 | 0.81 | | 0.09 | | 0.09 | | 0.03 | |
| Clearance Time (s) | | 7.0 | 7.0 | 4.0 | 7.0 | | 6.0 | | 6.0 | | 5.0 | |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 1194 | 526 | 715 | 2625 | | 229 | | 125 | | 63 | |
| v/s Ratio Prot | | c0.23 | 020 | c0.44 | 0.20 | | c0.02 | | .20 | | c0.00 | |
| v/s Ratio Perm | | 00.20 | 0.16 | • | 0.20 | | 00.02 | | 0.02 | | 00.00 | |
| v/c Ratio | | 0.64 | 0.45 | 1.01 | 0.25 | | 0.25 | | 0.25 | | 0.05 | |
| Uniform Delay, d1 | | 40.7 | 37.4 | 42.9 | 3.6 | | 65.0 | | 65.0 | | 71.5 | |
| Progression Factor | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 2.6 | 2.8 | 36.5 | 0.2 | | 0.6 | | 1.1 | | 0.3 | |
| Delay (s) | | 43.3 | 40.1 | 79.4 | 3.8 | | 65.6 | | 66.1 | | 71.8 | |
| Level of Service | | D | D | E | A | | E | | E | | E | |
| Approach Delay (s) | | 42.1 | | _ | 43.4 | | _ | 66.0 | _ | | 71.8 | |
| Approach LOS | | D | | | D | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 46.0 | H | CM 2000 | Level of S | Service | | D | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.75 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 153.0 | S | um of lost | time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | 1 | | 83.1% | IC | CU Level of | of Service | | | Е | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Synchro 10 Report Baseline Page 1

| | - | * | 1 | • | 1 | - | | |
|-------------------------------|------------|-------|-------|----------|------------|------------------|---|--|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | | |
| Lane Configurations | ^ | 7 | | ^ | 74 | 7 | | |
| Traffic Volume (vph) | 826 | 268 | 0 | 1282 | 70 | 309 | | |
| Future Volume (vph) | 826 | 268 | 0 | 1282 | 70 | 309 | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | |
| Total Lost time (s) | 5.0 | 4.0 | | 5.0 | 5.0 | 5.0 | | |
| Lane Util. Factor | 0.95 | 1.00 | | 0.95 | 0.97 | 0.91 | | |
| Frt | 1.00 | 0.85 | | 1.00 | 0.90 | 0.85 | | |
| Flt Protected | 1.00 | 1.00 | | 1.00 | 0.98 | 1.00 | | |
| Satd. Flow (prot) | 3411 | 1526 | | 3411 | 3075 | 1389 | | |
| Flt Permitted | 1.00 | 1.00 | | 1.00 | 0.98 | 1.00 | | |
| Satd. Flow (perm) | 3411 | 1526 | | 3411 | 3075 | 1389 | | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | | |
| Adj. Flow (vph) | 852 | 276 | 0 | 1322 | 72 | 319 | | |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 102 | 102 | | |
| Lane Group Flow (vph) | 852 | 276 | 0 | 1322 | 130 | 57 | | |
| Heavy Vehicles (%) | 7% | 7% | 0% | 7% | 7% | 7% | | |
| Turn Type | NA | Free | | NA | Prot | Perm | | |
| Protected Phases | 2 | | | 6 | 8 | | | |
| Permitted Phases | | Free | | | | 8 | | |
| Actuated Green, G (s) | 47.0 | 77.0 | | 47.0 | 15.0 | 15.0 | | |
| Effective Green, g (s) | 49.5 | 77.0 | | 49.5 | 17.5 | 17.5 | | |
| Actuated g/C Ratio | 0.64 | 1.00 | | 0.64 | 0.23 | 0.23 | | |
| Clearance Time (s) | 7.5 | | | 7.5 | 7.5 | 7.5 | | |
| Vehicle Extension (s) | 4.0 | | | 4.0 | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 2192 | 1526 | | 2192 | 698 | 315 | | |
| v/s Ratio Prot | 0.25 | | | c0.39 | 0.04 | | | |
| v/s Ratio Perm | | c0.18 | | | | 0.04 | | |
| v/c Ratio | 0.39 | 0.18 | | 0.60 | 0.19 | 0.18 | | |
| Uniform Delay, d1 | 6.5 | 0.0 | | 8.0 | 24.0 | 24.0 | | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 0.5 | 0.3 | | 1.2 | 0.1 | 0.3 | | |
| Delay (s) | 7.1 | 0.3 | | 9.3 | 24.1 | 24.3 | | |
| Level of Service | Α | Α | | Α | С | С | | |
| Approach Delay (s) | 5.4 | | | 9.3 | 24.2 | | | |
| Approach LOS | Α | | | Α | С | | | |
| Intersection Summary | | | | | | | | |
| HCM 2000 Control Delay | | | 9.8 | H | CM 2000 | Level of Service | е | |
| HCM 2000 Volume to Capa | city ratio | | 0.51 | | | | | |
| Actuated Cycle Length (s) | | | 77.0 | | ım of lost | ٠, | | |
| Intersection Capacity Utiliza | ition | | 56.3% | IC | U Level o | of Service | | |
| Analysis Period (min) | | | 15 | | | | | |
| c Critical Lane Group | | | | | | | | |

Baseline Synchro 10 Report Page 2

| | ٠ | → | • | • | • | • | 4 | 1 | - | - | ţ | 1 |
|-------------------------------|-------------------------------|----------|-------|-------|-------------|------------|----------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | * | ^ | 7 | 7 | ^ | 7 | * | ^ | 7 |
| Traffic Volume (vph) | 92 | 688 | 230 | 248 | 979 | 11 | 190 | 101 | 96 | 101 | 657 | 308 |
| Future Volume (vph) | 92 | 688 | 230 | 248 | 979 | 11 | 190 | 101 | 96 | 101 | 657 | 308 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1772 | 3544 | 1547 | 1807 | 3510 | 1126 | 1825 | 3288 | 1555 | 1772 | 3614 | 1596 |
| Flt Permitted | 0.13 | 1.00 | 1.00 | 0.19 | 1.00 | 1.00 | 0.27 | 1.00 | 1.00 | 0.69 | 1.00 | 1.00 |
| Satd. Flow (perm) | 238 | 3544 | 1547 | 359 | 3510 | 1126 | 526 | 3288 | 1555 | 1280 | 3614 | 1596 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 95 | 709 | 237 | 256 | 1009 | 11 | 196 | 104 | 99 | 104 | 677 | 318 |
| RTOR Reduction (vph) | 0 | 0 | 162 | 0 | 0 | 7 | 0 | 0 | 52 | 0 | 0 | 114 |
| Lane Group Flow (vph) | 95 | 709 | 75 | 256 | 1009 | 4 | 196 | 104 | 47 | 104 | 677 | 204 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | | | | | | |
| Confl. Bikes (#/hr) | | | | | | | | | | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 4% | 1% | 4% | 45% | 0% | 11% | 5% | 3% | 1% | 1% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |
| Protected Phases | 7 | 4 | . 0 | 3 | 8 | . 0 | 1 | 6 | . 0 | . 0 | 2 | |
| Permitted Phases | 4 | • | 4 | 8 | | 8 | 6 | • | 6 | 2 | _ | 2 |
| Actuated Green, G (s) | 45.6 | 37.8 | 37.8 | 58.6 | 46.8 | 46.8 | 62.8 | 62.8 | 62.8 | 50.8 | 50.8 | 50.8 |
| Effective Green, g (s) | 51.6 | 41.3 | 41.3 | 61.6 | 50.3 | 50.3 | 65.8 | 65.3 | 65.3 | 53.3 | 53.3 | 53.3 |
| Actuated g/C Ratio | 0.38 | 0.30 | 0.30 | 0.45 | 0.37 | 0.37 | 0.48 | 0.48 | 0.48 | 0.39 | 0.39 | 0.39 |
| Clearance Time (s) | 4.0 | 8.5 | 8.5 | 4.0 | 8.5 | 8.5 | 4.0 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 209 | 1065 | 465 | 369 | 1284 | 412 | 355 | 1562 | 739 | 496 | 1401 | 619 |
| v/s Ratio Prot | 0.04 | 0.20 | 700 | c0.10 | c0.29 | 712 | c0.04 | 0.03 | 700 | 450 | c0.19 | 013 |
| v/s Ratio Perm | 0.13 | 0.20 | 0.05 | 0.21 | 00.20 | 0.00 | 0.22 | 0.00 | 0.03 | 0.08 | 00.10 | 0.13 |
| v/c Ratio | 0.45 | 0.67 | 0.16 | 0.69 | 0.79 | 0.01 | 0.55 | 0.07 | 0.06 | 0.21 | 0.48 | 0.33 |
| Uniform Delay, d1 | 30.5 | 42.0 | 35.3 | 26.9 | 38.8 | 27.7 | 22.3 | 19.5 | 19.5 | 28.0 | 31.7 | 29.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.6 | 1.6 | 0.2 | 5.6 | 3.2 | 0.0 | 1.9 | 0.1 | 0.2 | 1.0 | 1.2 | 1.4 |
| Delay (s) | 32.1 | 43.6 | 35.5 | 32.4 | 42.0 | 27.7 | 24.1 | 19.6 | 19.7 | 29.0 | 32.9 | 30.9 |
| Level of Service | C | D | D | C | D | C | C | В | В | C | C | C |
| Approach Delay (s) | | 40.7 | | | 40.0 | | <u> </u> | 21.9 | | | 31.9 | |
| Approach LOS | | D | | | D | | | C | | | C | |
| • • | | | | | | | | | | | | |
| Intersection Summary | | | | | | | <u> </u> | | _ | | | |
| HCM 2000 Control Delay | | | 36.0 | Н | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Capa | icity ratio | | 0.62 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 137.4 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliza | on Capacity Utilization 107.4 | | | | CU Level of | of Service | 9 | | G | | | |
| Analysis Period (min) | eriod (min) | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Synchro 10 Report Page 3 Baseline

| | - | • | 1 | • | 1 | 1 | |
|--------------------------------|------------|------|-------|----------|------------|------------------|---|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | |
| Lane Configurations | † † | 7 | * | ^ | 7 | 7 | |
| Traffic Volume (vph) | 726 | 68 | 38 | 944 | 173 | 69 | |
| Future Volume (vph) | 726 | 68 | 38 | 944 | 173 | 69 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 | |
| Flt Protected | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 3444 | 1541 | 1772 | 3510 | 1807 | 1526 | |
| FIt Permitted | 1.00 | 1.00 | 0.35 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 3444 | 1541 | 661 | 3510 | 1807 | 1526 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | |
| Adj. Flow (vph) | 748 | 70 | 39 | 973 | 178 | 71 | |
| RTOR Reduction (vph) | 0 | 20 | 0 | 0 | 0 | 59 | |
| Lane Group Flow (vph) | 748 | 50 | 39 | 973 | 178 | 12 | |
| Heavy Vehicles (%) | 6% | 6% | 3% | 4% | 1% | 7% | |
| Turn Type | NA | Perm | Perm | NA | Prot | Perm | |
| Protected Phases | 6 | | | 2 | 8 | | |
| Permitted Phases | | 6 | 2 | | | 8 | |
| Actuated Green, G (s) | 64.7 | 64.7 | 64.7 | 64.7 | 14.4 | 14.4 | |
| Effective Green, g (s) | 67.2 | 67.2 | 67.2 | 67.2 | 16.4 | 16.4 | |
| Actuated g/C Ratio | 0.72 | 0.72 | 0.72 | 0.72 | 0.18 | 0.18 | |
| Clearance Time (s) | 7.5 | 7.5 | 7.5 | 7.5 | 7.0 | 7.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 2472 | 1106 | 474 | 2520 | 316 | 267 | |
| v/s Ratio Prot | 0.22 | | | c0.28 | c0.10 | | |
| v/s Ratio Perm | | 0.03 | 0.06 | | | 0.01 | |
| v/c Ratio | 0.30 | 0.05 | 0.08 | 0.39 | 0.56 | 0.05 | |
| Uniform Delay, d1 | 4.8 | 3.8 | 4.0 | 5.2 | 35.3 | 32.1 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | 0.1 | 0.3 | 0.4 | 2.3 | 0.1 | |
| Delay (s) | 5.1 | 3.9 | 4.3 | 5.6 | 37.6 | 32.2 | |
| Level of Service | Α | Α | Α | Α | D | С | |
| Approach Delay (s) | 5.0 | | | 5.5 | 36.1 | | |
| Approach LOS | Α | | | Α | D | | |
| Intersection Summary | | | | | | | |
| HCM 2000 Control Delay | | | 9.0 | H | CM 2000 | Level of Service | е |
| HCM 2000 Volume to Capac | city ratio | | 0.42 | | | | |
| Actuated Cycle Length (s) | | | 93.6 | | um of lost | | |
| Intersection Capacity Utilizat | ion | | 58.3% | IC | U Level o | of Service | |
| Analysis Period (min) | | | 15 | | | | |
| c Critical Lane Group | | | | | | | |

Synchro 10 Report Page 4 Baseline

| | ۶ | - | * | 1 | — | 1 | 1 | † | ~ | - | Ţ | 1 |
|------------------------------|-------------|----------|-------|-------|------------|------------|---------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ↑ | 7 | 7 | 1→ | | 7 | 1 | | 7 | ^ | 7 |
| Traffic Volume (vph) | 187 | 84 | 406 | 47 | 34 | 5 | 161 | 203 | 60 | 31 | 1031 | 699 |
| Future Volume (vph) | 187 | 84 | 406 | 47 | 34 | 5 | 161 | 203 | 60 | 31 | 1031 | 699 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | | 1.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.99 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1738 | 1731 | 1532 | 1206 | 1560 | | 1601 | 3047 | | 1759 | 3544 | 1601 |
| Flt Permitted | 0.71 | 1.00 | 1.00 | 0.70 | 1.00 | | 0.15 | 1.00 | | 0.58 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1302 | 1731 | 1532 | 890 | 1560 | | 258 | 3047 | | 1083 | 3544 | 1601 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 193 | 87 | 419 | 48 | 35 | 5 | 166 | 209 | 62 | 32 | 1063 | 721 |
| RTOR Reduction (vph) | 0 | 0 | 221 | 0 | 3 | 0 | 0 | 18 | 0 | 0 | 0 | 342 |
| Lane Group Flow (vph) | 193 | 87 | 198 | 48 | 37 | 0 | 166 | 253 | 0 | 32 | 1063 | 379 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | | | 4 | 4 | | |
| Heavy Vehicles (%) | 5% | 11% | 5% | 51% | 21% | 20% | 14% | 8% | 38% | 3% | 3% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | | pm+pt | NA | | Perm | NA | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | 1 | 6 | | | 2 | |
| Permitted Phases | 4 | | 4 | 8 | | | 6 | | | 2 | | 2 |
| Actuated Green, G (s) | 50.2 | 39.8 | 39.8 | 39.8 | 33.4 | | 85.5 | 85.5 | | 69.3 | 69.3 | 69.3 |
| Effective Green, g (s) | 53.2 | 42.3 | 42.3 | 45.8 | 35.9 | | 88.5 | 88.0 | | 71.8 | 71.8 | 71.8 |
| Actuated g/C Ratio | 0.35 | 0.28 | 0.28 | 0.30 | 0.24 | | 0.59 | 0.58 | | 0.48 | 0.48 | 0.48 |
| Clearance Time (s) | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | | 4.0 | 7.5 | | 7.5 | 7.5 | 7.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 505 | 485 | 430 | 290 | 371 | | 286 | 1779 | | 515 | 1688 | 762 |
| v/s Ratio Prot | c0.04 | 0.05 | | 0.01 | 0.02 | | c0.06 | 0.08 | | | c0.30 | |
| v/s Ratio Perm | 0.09 | | c0.13 | 0.04 | | | 0.28 | | | 0.03 | | 0.24 |
| v/c Ratio | 0.38 | 0.18 | 0.46 | 0.17 | 0.10 | | 0.58 | 0.14 | | 0.06 | 0.63 | 0.50 |
| Uniform Delay, d1 | 35.5 | 41.1 | 44.8 | 38.0 | 44.8 | | 19.5 | 14.2 | | 21.3 | 29.5 | 27.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.5 | 0.8 | 3.5 | 0.3 | 0.5 | | 3.0 | 0.2 | | 0.2 | 1.8 | 2.3 |
| Delay (s) | 36.0 | 41.9 | 48.3 | 38.3 | 45.3 | | 22.5 | 14.4 | | 21.5 | 31.3 | 29.4 |
| Level of Service | D | D | D | D | D | | С | В | | С | С | С |
| Approach Delay (s) | | 44.1 | | | 41.5 | | | 17.5 | | | 30.4 | |
| Approach LOS | | D | | | D | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 32.0 | H | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.55 | | | | | | 10.5 | | | |
| Actuated Cycle Length (s) | | | 150.7 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliz | ation | | 86.7% | IC | U Level o | of Service | 9 | | Е | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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| | ٠ | → | * | • | ← | • | 1 | 1 | ~ | 1 | Ţ | ✓ |
|------------------------------|----------------------------------|----------|-------|-------|------------|------------|---------|----------|-------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | 1→ | | 7 | 7 | | * | ↑ | 7 | * | 1 | |
| Traffic Volume (vph) | 1 | 2 | 14 | 792 | 10 | 247 | 5 | 302 | 249 | 251 | 773 | 3 |
| Future Volume (vph) | 1 | 2 | 14 | 792 | 10 | 247 | 5 | 302 | 249 | 251 | 773 | 3 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | | 1.0 | 5.0 | | 5.0 | 5.0 | 1.0 | 1.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.87 | | 1.00 | 0.86 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1825 | 1669 | | 1755 | 1461 | | 1825 | 1715 | 1440 | 1659 | 1762 | |
| Flt Permitted | 0.60 | 1.00 | | 0.73 | 1.00 | | 0.08 | 1.00 | 1.00 | 0.42 | 1.00 | |
| Satd. Flow (perm) | 1145 | 1669 | | 1340 | 1461 | | 145 | 1715 | 1440 | 728 | 1762 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 1 | 2 | 14 | 792 | 10 | 255 | 5 | 311 | 257 | 259 | 797 | 3 |
| RTOR Reduction (vph) | 0 | 11 | 0 | 0 | 143 | 0 | 0 | 0 | 97 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 1 | 5 | 0 | 792 | 122 | 0 | 5 | 311 | 160 | 259 | 800 | 0 |
| Confl. Bikes (#/hr) | | | | | | | | | 1 | | | 1 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 4% | 0% | 13% | 0% | 12% | 12% | 10% | 9% | 0% |
| Turn Type | pm+pt | NA | | pm+pt | NA | | Perm | NA | pm+ov | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | | 6 | 3 | 5 | 2 | |
| Permitted Phases | 4 | | | 8 | | | 6 | | 6 | 2 | | |
| Actuated Green, G (s) | 31.6 | 30.2 | | 66.2 | 60.8 | | 51.0 | 51.0 | 83.0 | 63.0 | 63.0 | |
| Effective Green, g (s) | 37.6 | 32.2 | | 69.2 | 62.8 | | 53.0 | 53.0 | 89.0 | 66.0 | 65.0 | |
| Actuated g/C Ratio | 0.26 | 0.22 | | 0.48 | 0.44 | | 0.37 | 0.37 | 0.62 | 0.46 | 0.45 | |
| Clearance Time (s) | 4.0 | 7.0 | | 4.0 | 7.0 | | 7.0 | 7.0 | 4.0 | 4.0 | 7.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 6.0 | 6.0 | 3.0 | 6.0 | 3.0 | |
| Lane Grp Cap (vph) | 321 | 375 | | 748 | 640 | | 53 | 634 | 894 | 407 | 799 | |
| v/s Ratio Prot | 0.00 | 0.00 | | c0.26 | 0.08 | | | 0.18 | 0.04 | 0.05 | c0.45 | |
| v/s Ratio Perm | 0.00 | | | 0.25 | | | 0.03 | | 0.07 | 0.24 | | |
| v/c Ratio | 0.00 | 0.01 | | 1.06 | 0.19 | | 0.09 | 0.49 | 0.18 | 0.64 | 1.00 | |
| Uniform Delay, d1 | 39.0 | 43.2 | | 34.9 | 24.6 | | 29.4 | 34.7 | 11.5 | 28.4 | 39.1 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 0.1 | | 49.6 | 0.7 | | 3.5 | 2.7 | 0.1 | 5.4 | 32.1 | |
| Delay (s) | 39.0 | 43.2 | | 84.4 | 25.3 | | 32.9 | 37.4 | 11.6 | 33.7 | 71.2 | |
| Level of Service | D | D | | F | С | | С | D | В | С | Е | |
| Approach Delay (s) | | 43.0 | | | 69.6 | | | 25.8 | | | 62.1 | |
| Approach LOS | | D | | | Е | | | С | | | Е | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 57.2 | H | CM 2000 | Level of S | Service | | Е | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.99 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 143.2 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliz | tion Capacity Utilization 128.9% | | | IC | U Level c | f Service | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Synchro 10 Report Page 6 Baseline

| | - | * | 1 | • | 1 | - | | |
|-------------------------------|-------------|---------|---------|----------|------------|------------------|---|--|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | | |
| Lane Configurations | * | 7 | ሻ | <u> </u> | ሻ | 7 | | |
| Traffic Volume (vph) | 418 | 101 | 86 | 1086 | 130 | 129 | | |
| Future Volume (vph) | 418 | 101 | 86 | 1086 | 130 | 129 | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | |
| Total Lost time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Frpb, ped/bikes | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 0.98 | | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Frt | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 | | |
| Flt Protected | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1812 | 1480 | 1788 | 1883 | 1738 | 1567 | | |
| Flt Permitted | 1.00 | 1.00 | 0.48 | 1.00 | 0.95 | 1.00 | | |
| Satd. Flow (perm) | 1812 | 1480 | 910 | 1883 | 1738 | 1567 | | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | | |
| Adj. Flow (vph) | 431 | 104 | 89 | 1120 | 134 | 133 | | |
| RTOR Reduction (vph) | 0 | 41 | 0 | 0 | 0 | 105 | | |
| Lane Group Flow (vph) | 431 | 63 | 89 | 1120 | 134 | 28 | | |
| Confl. Peds. (#/hr) | 101 | 1 | 1 | 1120 | 1 | 1 | | |
| Heavy Vehicles (%) | 6% | 8% | 2% | 2% | 5% | 2% | | |
| Turn Type | NA | Perm | Perm | NA | Prot | Perm | | |
| Protected Phases | 6 | 1 01111 | 1 01111 | 2 | 8 | 1 01111 | | |
| Permitted Phases | | 6 | 2 | | | 8 | | |
| Actuated Green, G (s) | 30.3 | 30.3 | 30.3 | 30.3 | 10.6 | 10.6 | | |
| Effective Green, g (s) | 32.8 | 32.8 | 32.8 | 32.8 | 11.6 | 11.6 | | |
| Actuated g/C Ratio | 0.60 | 0.60 | 0.60 | 0.60 | 0.21 | 0.21 | | |
| Clearance Time (s) | 7.5 | 7.5 | 7.5 | 7.5 | 6.0 | 6.0 | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 1092 | 892 | 548 | 1135 | 370 | 334 | | |
| v/s Ratio Prot | 0.24 | 302 | | c0.59 | c0.08 | | | |
| v/s Ratio Perm | V.E 1 | 0.04 | 0.10 | 33.00 | 22.00 | 0.02 | | |
| v/c Ratio | 0.39 | 0.07 | 0.16 | 0.99 | 0.36 | 0.08 | | |
| Uniform Delay, d1 | 5.6 | 4.5 | 4.8 | 10.6 | 18.2 | 17.1 | | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 1.1 | 0.2 | 0.6 | 23.7 | 0.6 | 0.1 | | |
| Delay (s) | 6.7 | 4.6 | 5.4 | 34.3 | 18.9 | 17.3 | | |
| Level of Service | Α | A | Α | С | В | В | | |
| Approach Delay (s) | 6.3 | | | 32.2 | 18.1 | | | |
| Approach LOS | A | | | С | В | | | |
| Intersection Summary | | | | | | | | |
| HCM 2000 Control Delay | | | 23.4 | Н | CM 2000 | Level of Service |) | |
| HCM 2000 Volume to Capa | acity ratio | | 0.82 | | | | | |
| Actuated Cycle Length (s) | ., | | 54.4 | S | um of lost | t time (s) | | |
| Intersection Capacity Utiliza | ation | | 74.2% | | | of Service | | |
| Analysis Period (min) | | | 15 | | | | | |
| c Critical Lane Group | | | | | | | | |

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|-------------------------------|------------|----------|--------|-------|------------|------------|---------|----------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | * | 7 | * | ^ | 7 | * | ^ | 1 | * | ^ | 7 |
| Traffic Volume (vph) | 166 | 379 | 33 | 245 | 488 | 71 | 35 | 919 | 132 | 181 | 1682 | 284 |
| Future Volume (vph) | 166 | 379 | 33 | 245 | 488 | 71 | 35 | 919 | 132 | 181 | 1682 | 284 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1738 | 1865 | 1330 | 1772 | 1847 | 1385 | 1644 | 3476 | 1487 | 1770 | 3579 | 1585 |
| Flt Permitted | 0.10 | 1.00 | 1.00 | 0.18 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.21 | 1.00 | 1.00 |
| Satd. Flow (perm) | 188 | 1865 | 1330 | 335 | 1847 | 1385 | 96 | 3476 | 1487 | 390 | 3579 | 1585 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 1.00 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 171 | 391 | 34 | 245 | 488 | 73 | 36 | 947 | 136 | 187 | 1734 | 293 |
| RTOR Reduction (vph) | 0 | 0 | 25 | 0 | 0 | 54 | 0 | 0 | 66 | 0 | 0 | 89 |
| Lane Group Flow (vph) | 171 | 391 | 9 | 245 | 488 | 19 | 36 | 947 | 70 | 187 | 1734 | 204 |
| Confl. Peds. (#/hr) | 16 | | 1 | 1 | | 16 | 5 | | 14 | 14 | | 5 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 2 |
| Heavy Vehicles (%) | 5% | 3% | 21% | 3% | 4% | 14% | 11% | 5% | 4% | 3% | 2% | 1% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 6 | | 6 | 2 | | 2 |
| Actuated Green, G (s) | 44.0 | 36.0 | 36.0 | 44.0 | 36.0 | 36.0 | 74.0 | 74.0 | 74.0 | 86.0 | 86.0 | 86.0 |
| Effective Green, g (s) | 50.0 | 39.0 | 39.0 | 50.0 | 39.0 | 39.0 | 77.0 | 77.0 | 77.0 | 89.0 | 89.0 | 89.0 |
| Actuated g/C Ratio | 0.33 | 0.26 | 0.26 | 0.33 | 0.26 | 0.26 | 0.51 | 0.51 | 0.51 | 0.59 | 0.59 | 0.59 |
| Clearance Time (s) | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 176 | 484 | 345 | 217 | 480 | 360 | 49 | 1784 | 763 | 332 | 2123 | 940 |
| v/s Ratio Prot | 0.07 | 0.21 | | c0.08 | c0.26 | | | 0.27 | | 0.04 | c0.48 | |
| v/s Ratio Perm | 0.25 | | 0.01 | 0.29 | | 0.01 | 0.38 | | 0.05 | 0.29 | | 0.13 |
| v/c Ratio | 0.97 | 0.81 | 0.03 | 1.13 | 1.02 | 0.05 | 0.73 | 0.53 | 0.09 | 0.56 | 0.82 | 0.22 |
| Uniform Delay, d1 | 41.5 | 52.0 | 41.3 | 45.7 | 55.5 | 41.6 | 28.5 | 24.4 | 18.6 | 16.7 | 24.1 | 14.2 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 59.2 | 9.6 | 0.0 | 100.1 | 45.3 | 0.2 | 65.6 | 1.1 | 0.2 | 2.2 | 3.6 | 0.5 |
| Delay (s) | 100.6 | 61.6 | 41.4 | 145.9 | 100.8 | 41.8 | 94.2 | 25.6 | 18.9 | 18.9 | 27.7 | 14.8 |
| Level of Service | F | E | D | F | F | D | F | С | В | В | С | В |
| Approach Delay (s) | | 71.6 | | | 109.2 | | | 26.9 | | | 25.2 | |
| Approach LOS | | Е | | | F | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 45.8 | Н | CM 2000 | Level of S | Service | | D | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.89 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 150.0 | | um of lost | ٠, | | | 12.0 | | | |
| Intersection Capacity Utiliza | ation | | 123.6% | IC | CU Level | of Service | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|---------------------------------|-----------|-----------|-------|--------------|--------------|------------|--------------|-----------|--------------|--------------|--------------|--------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ተተ1> | | 7 | ^ | 7 | 7 | | 7 | 7 | 4 | 7 |
| Traffic Volume (vph) | 0 | 2524 | 10 | 9 | 1054 | 0 | 6 | 0 | 13 | 79 | 5 | 32 |
| Future Volume (vph) | 0 | 2524 | 10 | 9 | 1054 | 0 | 6 | 0 | 13 | 79 | 5 | 32 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | | 1.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 0.91 | | 1.00 | 0.95 | | 1.00 | | 1.00 | 0.95 | 0.91 | 0.95 |
| Frpb, ped/bikes | | 1.00 | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | | 1.00 | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt Flt Protected | | 1.00 | | 1.00 0.95 | 1.00 1.00 | | 1.00 | | 0.85 1.00 | 1.00 0.95 | 0.99 0.96 | 0.85 |
| Satd. Flow (prot) | | 4852 | | 1372 | 3349 | | 0.95 1371 | | 1247 | 1651 | 1521 | 1.00 1085 |
| Flt Permitted | | 1.00 | | 0.04 | 1.00 | | 0.45 | | 1.00 | 0.95 | 0.96 | 1.00 |
| Satd. Flow (perm) | | 4852 | | 52 | 3349 | | 656 | | 1247 | 1651 | 1521 | 1085 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 0.97 | 2602 | 10 | 9 | 1087 | 0.97 | 6 | 0.97 | 13 | 81 | 5 | 33 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 2 | 28 |
| Lane Group Flow (vph) | 0 | 2612 | 0 | 9 | 1087 | 0 | 6 | 0 | 1 | 45 | 42 | 2 |
| Confl. Peds. (#/hr) | | 2012 | 4 | 4 | 1007 | | 1 | | | 10 | 12 | 1 |
| Heavy Vehicles (%) | 0% | 8% | 10% | 33% | 9% | 0% | 33% | 0% | 31% | 5% | 20% | 41% |
| Turn Type | | NA | | pm+pt | NA | Perm | Perm | | Perm | Perm | NA | Perm |
| Protected Phases | | 2 | | 1 | 6 | | | | | | 4 | |
| Permitted Phases | | | | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | | 107.8 | | 113.2 | 113.2 | | 6.3 | | 6.3 | 9.0 | 9.0 | 9.0 |
| Effective Green, g (s) | | 109.8 | | 116.2 | 115.2 | | 8.8 | | 8.8 | 11.0 | 11.0 | 11.0 |
| Actuated g/C Ratio | | 0.73 | | 0.77 | 0.77 | | 0.06 | | 0.06 | 0.07 | 0.07 | 0.07 |
| Clearance Time (s) | | 7.0 | | 4.0 | 7.0 | | 7.5 | | 7.5 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 3551 | | 79 | 2572 | | 38 | | 73 | 121 | 111 | 79 |
| v/s Ratio Prot | | c0.54 | | 0.00 | c0.32 | | | | | | | |
| v/s Ratio Perm | | | | 0.09 | | | c0.01 | | 0.00 | 0.03 | 0.03 | 0.00 |
| v/c Ratio | | 0.74 | | 0.11 | 0.42 | | 0.16 | | 0.01 | 0.37 | 0.38 | 0.03 |
| Uniform Delay, d1 | | 11.7 | | 10.3 | 6.0 | | 67.1 | | 66.5 | 66.2 | 66.2 | 64.5 |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 1.4 | | 0.6 | 0.5 | | 1.9 | | 0.1 | 1.9 | 2.2 | 0.1 |
| Delay (s) | | 13.1 B | | 11.0 | 6.5 | | 69.0 E | | 66.6 E | 68.1 E | 68.4 E | 64.7 E |
| Level of Service | | 13.1 | | В | A 6.5 | | Е | 67.3 | | Е | 67.4 | |
| Approach Delay (s) Approach LOS | | 13.1 B | | | 0.5 A | | | 67.3 E | | | 67.4 E | |
| • • | | Ь | | | Α | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 13.1 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.67 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 150.0 | | um of lost | | | | 18.5 | | | |
| Intersection Capacity Utilizati | ion | | 78.8% | IC | CU Level | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-----------------------------------|-------|----------|-------|------|-------------|------------|---------|------|-------|----------|---------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ^ | 7 | | ^ | 7 | 44 | | 77 | | | |
| Traffic Volume (vph) | 0 | 1239 | 0 | 0 | 2249 | 0 | 403 | 0 | 467 | 0 | 0 | 0 |
| Future Volume (vph) | 0 | 1239 | 0 | 0 | 2249 | 0 | 403 | 0 | 467 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | | | 5.0 | | 5.0 | | 5.0 | | | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 0.97 | | 0.88 | | | |
| Frt | | 1.00 | | | 1.00 | | 1.00 | | 0.85 | | | |
| FIt Protected | | 1.00 | | | 1.00 | | 0.95 | | 1.00 | | | |
| Satd. Flow (prot) | | 3411 | | | 3444 | | 3190 | | 2566 | | | |
| FIt Permitted | | 1.00 | | | 1.00 | | 0.95 | | 1.00 | | | |
| Satd. Flow (perm) | | 3411 | | | 3444 | | 3190 | | 2566 | | | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 0 | 1277 | 0 | 0 | 2319 | 0 | 415 | 0 | 481 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 117 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1277 | 0 | 0 | 2319 | 0 | 415 | 0 | 364 | 0 | 0 | 0 |
| Heavy Vehicles (%) | 0% | 7% | 0% | 0% | 6% | 0% | 11% | 0% | 12% | 0% | 0% | 0% |
| Turn Type | | NA | Perm | | NA | Perm | Perm | | Perm | | | |
| Protected Phases | | 2 | | | 6 | | | | | | | |
| Permitted Phases | | | 2 | | | 6 | 8 | | 8 | | | |
| Actuated Green, G (s) | | 117.4 | | | 117.4 | | 28.6 | | 28.6 | | | |
| Effective Green, g (s) | | 119.9 | | | 119.9 | | 30.1 | | 30.1 | | | |
| Actuated g/C Ratio | | 0.75 | | | 0.75 | | 0.19 | | 0.19 | | | |
| Clearance Time (s) | | 7.5 | | | 7.5 | | 6.5 | | 6.5 | | | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | 3.0 | | 3.0 | | | |
| Lane Grp Cap (vph) | | 2556 | | | 2580 | | 600 | | 482 | | | |
| v/s Ratio Prot | | 0.37 | | | c0.67 | | | | | | | |
| v/s Ratio Perm | | | | | | | 0.13 | | c0.14 | | | |
| v/c Ratio | | 0.50 | | | 0.90 | | 0.69 | | 0.76 | | | |
| Uniform Delay, d1 | | 8.0 | | | 15.4 | | 60.6 | | 61.5 | | | |
| Progression Factor | | 1.00 | | | 0.70 | | 1.00 | | 1.00 | | | |
| Incremental Delay, d2 | | 0.7 | | | 2.9 | | 3.4 | | 6.6 | | | |
| Delay (s) | | 8.7 | | | 13.7 | | 64.1 | | 68.1 | | | |
| Level of Service | | Α | | | В | | E | | E | | | |
| Approach Delay (s) | | 8.7 | | | 13.7 | | | 66.2 | | | 0.0 | |
| Approach LOS | | Α | | | В | | | Е | | | Α | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 22.8 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.88 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 160.0 | | um of lost | | | | 11.5 | | | |
| Intersection Capacity Utilization | | | 81.2% | IC | CU Level of | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|------------|----------|------|-------|------------|------------|---------|----------|------|----------|----------|-------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 44 | ^ | 7 | * | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 135 | 1205 | 241 | 223 | 1460 | 26 | 156 | 312 | 101 | 76 | 912 | 511 |
| Future Volume (vph) | 135 | 1205 | 241 | 223 | 1460 | 26 | 156 | 312 | 101 | 76 | 912 | 511 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 0.97 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3404 | 3476 | 1564 | 1755 | 3579 | 1305 | 1722 | 3380 | 1427 | 1681 | 3579 | 1578 |
| FIt Permitted | 0.95 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 | 0.49 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3404 | 3476 | 1564 | 139 | 3579 | 1305 | 158 | 3380 | 1427 | 874 | 3579 | 1578 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 139 | 1242 | 248 | 230 | 1505 | 27 | 161 | 322 | 104 | 78 | 940 | 527 |
| RTOR Reduction (vph) | 0 | 0 | 124 | 0 | 0 | 0 | 0 | 0 | 74 | 0 | 0 | 111 |
| Lane Group Flow (vph) | 139 | 1242 | 124 | 230 | 1505 | 27 | 161 | 322 | 30 | 78 | 940 | 416 |
| Confl. Peds. (#/hr) | 4 | | 1 | 1 | | 4 | 2 | | 14 | 14 | | 2 |
| Heavy Vehicles (%) | 4% | 5% | 3% | 4% | 2% | 23% | 6% | 8% | 11% | 8% | 2% | 2% |
| Turn Type | Prot | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 9.7 | 67.1 | 67.1 | 86.7 | 72.0 | 72.0 | 55.0 | 43.7 | 43.7 | 51.6 | 42.0 | 42.0 |
| Effective Green, g (s) | 13.7 | 70.1 | 70.1 | 89.7 | 75.0 | 75.0 | 60.3 | 46.7 | 46.7 | 57.6 | 45.0 | 45.0 |
| Actuated g/C Ratio | 0.09 | 0.44 | 0.44 | 0.56 | 0.47 | 0.47 | 0.38 | 0.29 | 0.29 | 0.36 | 0.28 | 0.28 |
| Clearance Time (s) | 5.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 291 | 1522 | 685 | 265 | 1677 | 611 | 199 | 986 | 416 | 378 | 1006 | 443 |
| v/s Ratio Prot | 0.04 | 0.36 | | c0.10 | c0.42 | | c0.07 | 0.10 | | 0.02 | 0.26 | |
| v/s Ratio Perm | | | 0.08 | 0.38 | | 0.02 | 0.23 | | 0.02 | 0.06 | | c0.26 |
| v/c Ratio | 0.48 | 0.82 | 0.18 | 0.87 | 0.90 | 0.04 | 0.81 | 0.33 | 0.07 | 0.21 | 0.93 | 0.94 |
| Uniform Delay, d1 | 69.7 | 39.3 | 27.4 | 44.9 | 39.0 | 23.1 | 40.6 | 44.3 | 41.0 | 34.4 | 56.1 | 56.2 |
| Progression Factor | 0.96 | 1.14 | 2.50 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.1 | 4.3 | 0.5 | 24.5 | 8.0 | 0.1 | 21.0 | 0.2 | 0.1 | 0.3 | 15.0 | 27.8 |
| Delay (s) | 68.1 | 49.3 | 69.1 | 69.4 | 47.0 | 23.2 | 61.6 | 44.5 | 41.1 | 34.7 | 71.1 | 84.0 |
| Level of Service | E | D | Е | E | D | С | Е | D | D | С | Е | F |
| Approach Delay (s) | | 53.9 | | | 49.5 | | | 48.6 | | | 73.6 | |
| Approach LOS | | D | | | D | | | D | | | Е | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 57.5 | Н | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.90 | | | | | | | | | |
| Actuated Cycle Length (s) | | | | | um of lost | t time (s) | | | 12.0 | | | |
| Intersection Capacity Utiliza | • | | | | CU Level | of Service |) | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| o Critical Lana Croup | | | | | | | | | | | | |

Synchro 10 Report Page 11 Baseline

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|------------------------------|-------|----------|--------|-------|-------------|------------|---------|-------------|------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | 1 | | * | ↑ ↑ | | 7 | ↑ ↑→ | | 7 | 1 | |
| Traffic Volume (vph) | 63 | 1256 | 148 | 130 | 1472 | 40 | 111 | 295 | 122 | 200 | 966 | 97 |
| Future Volume (vph) | 63 | 1256 | 148 | 130 | 1472 | 40 | 111 | 295 | 122 | 200 | 966 | 97 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | | 1.0 | 5.0 | | 1.0 | 5.0 | | 1.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 1.00 | | 1.00 | 0.96 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1738 | 3510 | | 1789 | 3563 | | 1738 | 3299 | | 1802 | 3507 | |
| Flt Permitted | 0.06 | 1.00 | | 0.06 | 1.00 | | 0.09 | 1.00 | | 0.37 | 1.00 | |
| Satd. Flow (perm) | 105 | 3510 | | 106 | 3563 | | 156 | 3299 | | 705 | 3507 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 65 | 1295 | 153 | 134 | 1518 | 41 | 114 | 304 | 126 | 206 | 996 | 100 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 1 | 0 | 0 | 27 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 65 | 1442 | 0 | 134 | 1558 | 0 | 114 | 403 | 0 | 206 | 1091 | 0 |
| Confl. Peds. (#/hr) | 15 | | 7 | 7 | | 15 | 20 | | 13 | 13 | | 20 |
| Heavy Vehicles (%) | 5% | 2% | 3% | 2% | 2% | 0% | 5% | 6% | 2% | 1% | 2% | 5% |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 74.0 | 66.8 | | 80.2 | 69.9 | | 52.0 | 44.0 | | 65.0 | 53.0 | |
| Effective Green, g (s) | 80.0 | 68.8 | | 84.1 | 71.9 | | 58.0 | 46.0 | | 68.0 | 55.0 | |
| Actuated g/C Ratio | 0.50 | 0.43 | | 0.53 | 0.45 | | 0.36 | 0.29 | | 0.42 | 0.34 | |
| Clearance Time (s) | 4.0 | 7.0 | | 4.0 | 7.0 | | 4.0 | 7.0 | | 4.0 | 7.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 156 | 1508 | | 195 | 1600 | | 165 | 947 | | 436 | 1204 | |
| v/s Ratio Prot | 0.03 | 0.41 | | c0.06 | c0.44 | | c0.05 | 0.12 | | 0.06 | c0.31 | |
| v/s Ratio Perm | 0.18 | | | 0.30 | | | 0.20 | | | 0.14 | | |
| v/c Ratio | 0.42 | 0.96 | | 0.69 | 0.97 | | 0.69 | 0.43 | | 0.47 | 0.91 | |
| Uniform Delay, d1 | 34.8 | 44.2 | | 41.3 | 43.2 | | 39.6 | 46.3 | | 30.5 | 50.1 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.8 | 14.9 | | 9.6 | 17.1 | | 11.8 | 1.4 | | 0.8 | 11.4 | |
| Delay (s) | 36.6 | 59.1 | | 51.0 | 60.2 | | 51.4 | 47.7 | | 31.3 | 61.5 | |
| Level of Service | D | Е | | D | Е | | D | D | | С | E | |
| Approach Delay (s) | | 58.1 | | | 59.5 | | | 48.5 | | | 56.7 | |
| Approach LOS | | E | | | Е | | | D | | | Е | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 57.2 | Н | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Cap | | | 0.90 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 160.1 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliz | ation | | 100.6% | IC | CU Level of | of Service | 9 | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| o Critical Lana Croup | | | | | | | | | | | | |

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|------------------------------|-------|----------|-------|-------|-----------|------------|---------|----------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | * | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 183 | 1096 | 249 | 198 | 1184 | 16 | 171 | 377 | 128 | 29 | 1039 | 396 |
| Future Volume (vph) | 183 | 1096 | 249 | 198 | 1184 | 16 | 171 | 377 | 128 | 29 | 1039 | 396 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1755 | 3579 | 1545 | 1807 | 3579 | 1517 | 1807 | 3510 | 1543 | 1769 | 3614 | 1575 |
| Flt Permitted | 0.08 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.50 | 1.00 | 1.00 |
| Satd. Flow (perm) | 143 | 3579 | 1545 | 145 | 3579 | 1517 | 153 | 3510 | 1543 | 933 | 3614 | 1575 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 189 | 1130 | 257 | 204 | 1221 | 16 | 176 | 389 | 132 | 30 | 1071 | 408 |
| RTOR Reduction (vph) | 0 | 0 | 103 | 0 | 0 | 10 | 0 | 0 | 81 | 0 | 0 | 103 |
| Lane Group Flow (vph) | 189 | 1130 | 154 | 204 | 1221 | 6 | 176 | 389 | 51 | 30 | 1071 | 305 |
| Confl. Peds. (#/hr) | 4 | | 4 | 4 | | 4 | 4 | | 5 | 5 | | 4 |
| Heavy Vehicles (%) | 4% | 2% | 4% | 1% | 2% | 6% | 1% | 4% | 4% | 3% | 1% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 56.6 | 48.6 | 48.6 | 60.6 | 50.6 | 50.6 | 58.8 | 50.8 | 50.8 | 51.4 | 47.1 | 47.1 |
| Effective Green, g (s) | 62.6 | 51.1 | 51.1 | 65.6 | 53.1 | 53.1 | 62.1 | 53.3 | 53.3 | 57.4 | 49.6 | 49.6 |
| Actuated g/C Ratio | 0.46 | 0.37 | 0.37 | 0.48 | 0.39 | 0.39 | 0.45 | 0.39 | 0.39 | 0.42 | 0.36 | 0.36 |
| Clearance Time (s) | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 195 | 1337 | 577 | 227 | 1390 | 589 | 202 | 1368 | 601 | 436 | 1311 | 571 |
| v/s Ratio Prot | c0.08 | 0.32 | | c0.09 | 0.34 | | c0.07 | 0.11 | | 0.00 | c0.30 | |
| v/s Ratio Perm | c0.36 | | 0.10 | 0.35 | | 0.00 | 0.32 | | 0.03 | 0.03 | | 0.19 |
| v/c Ratio | 0.97 | 0.85 | 0.27 | 0.90 | 0.88 | 0.01 | 0.87 | 0.28 | 0.09 | 0.07 | 0.82 | 0.53 |
| Uniform Delay, d1 | 38.2 | 39.2 | 29.8 | 38.1 | 38.8 | 25.7 | 33.7 | 28.6 | 26.3 | 23.4 | 39.4 | 34.4 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 54.9 | 6.7 | 1.1 | 33.4 | 8.1 | 0.0 | 31.1 | 0.1 | 0.1 | 0.1 | 4.1 | 1.0 |
| Delay (s) | 93.0 | 45.9 | 30.9 | 71.5 | 46.9 | 25.7 | 64.8 | 28.7 | 26.4 | 23.5 | 43.5 | 35.4 |
| Level of Service | F | D | С | Е | D | С | Е | С | С | С | D | D |
| Approach Delay (s) | | 49.1 | | | 50.2 | | | 37.4 | | | 40.9 | |
| Approach LOS | | D | | | D | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 45.5 | H | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Cap | | | 0.88 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 136.7 | | um of los | | | | 12.0 | | | |
| Intersection Capacity Utiliz | ation | | 96.2% | IC | U Level | of Service | Э | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| 0.10.110 | | | | | | | | | | | | |

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|-------------------------------|-------------|----------|-------|-------|------------|------------|---------|----------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 179 | 1021 | 97 | 183 | 1046 | 95 | 95 | 731 | 250 | 194 | 1315 | 307 |
| Future Volume (vph) | 179 | 1021 | 97 | 183 | 1046 | 95 | 95 | 731 | 250 | 194 | 1315 | 307 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 4.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1722 | 3476 | 1585 | 1807 | 3544 | 1565 | 1807 | 3510 | 1551 | 1824 | 3614 | 1600 |
| Flt Permitted | 0.09 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 | 0.07 | 1.00 | 1.00 | 0.25 | 1.00 | 1.00 |
| Satd. Flow (perm) | 155 | 3476 | 1585 | 163 | 3544 | 1565 | 128 | 3510 | 1551 | 487 | 3614 | 1600 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 185 | 1053 | 100 | 189 | 1078 | 98 | 98 | 754 | 258 | 200 | 1356 | 316 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 63 | 0 | 0 | 124 | 0 | 0 | 118 |
| Lane Group Flow (vph) | 185 | 1053 | 100 | 189 | 1078 | 35 | 98 | 754 | 134 | 200 | 1356 | 198 |
| Confl. Peds. (#/hr) | 1 | | | | | 1 | 7 | | 8 | 8 | | 7 |
| Heavy Vehicles (%) | 6% | 5% | 3% | 1% | 3% | 3% | 1% | 4% | 3% | 0% | 1% | 0% |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | Free | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 53.8 | 43.9 | 140.0 | 53.4 | 43.7 | 43.7 | 64.2 | 56.4 | 56.4 | 64.6 | 56.6 | 56.6 |
| Effective Green, g (s) | 59.8 | 45.9 | 140.0 | 59.4 | 45.7 | 45.7 | 70.2 | 58.4 | 58.4 | 70.6 | 58.6 | 58.6 |
| Actuated g/C Ratio | 0.43 | 0.33 | 1.00 | 0.42 | 0.33 | 0.33 | 0.50 | 0.42 | 0.42 | 0.50 | 0.42 | 0.42 |
| Clearance Time (s) | 4.0 | 7.0 | | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 210 | 1139 | 1585 | 218 | 1156 | 510 | 193 | 1464 | 646 | 350 | 1512 | 669 |
| v/s Ratio Prot | c0.08 | 0.30 | | 0.08 | c0.30 | | 0.04 | 0.21 | | c0.04 | c0.38 | |
| v/s Ratio Perm | 0.30 | | 0.06 | 0.29 | | 0.02 | 0.21 | | 0.09 | 0.24 | | 0.12 |
| v/c Ratio | 0.88 | 0.92 | 0.06 | 0.87 | 0.93 | 0.07 | 0.51 | 0.52 | 0.21 | 0.57 | 0.90 | 0.30 |
| Uniform Delay, d1 | 37.4 | 45.4 | 0.0 | 36.4 | 45.7 | 32.5 | 28.1 | 30.3 | 26.0 | 21.0 | 37.9 | 27.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 32.1 | 13.8 | 0.1 | 28.3 | 14.5 | 0.3 | 2.1 | 0.3 | 0.2 | 2.3 | 7.4 | 0.2 |
| Delay (s) | 69.5 | 59.1 | 0.1 | 64.8 | 60.2 | 32.7 | 30.2 | 30.6 | 26.2 | 23.2 | 45.2 | 27.3 |
| Level of Service | Е | E | Α | Е | Е | С | С | C | С | С | D | С |
| Approach Delay (s) | | 56.2 | | | 58.9 | | | 29.5 | | | 39.9 | |
| Approach LOS | | Е | | | Е | | | С | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 46.2 | Н | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.86 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 140.0 | | um of lost | . , | | | 12.0 | | | |
| Intersection Capacity Utiliza | ation | | 96.0% | IC | CU Level | of Service |) | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-----------------------------------|------|----------|-------|------|------------|------------|---------|------|------|------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | 4 | | | 4 | |
| Traffic Volume (vph) | 38 | 65 | 18 | 147 | 147 | 10 | 8 | 203 | 63 | 12 | 695 | 72 |
| Future Volume (vph) | 38 | 65 | 18 | 147 | 147 | 10 | 8 | 203 | 63 | 12 | 695 | 72 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | |
| Lane Util. Factor | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | | 0.98 | | | 1.00 | | | 0.97 | | | 0.99 | |
| Flt Protected | | 0.98 | | | 0.98 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | 1748 | | | 1809 | | | 1680 | | | 1841 | |
| FIt Permitted | | 0.78 | | | 0.49 | | | 0.97 | | | 0.99 | |
| Satd. Flow (perm) | | 1388 | | | 901 | | | 1640 | | | 1831 | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 38 | 65 | 18 | 147 | 147 | 10 | 8 | 203 | 63 | 12 | 695 | 72 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 116 | 0 | 0 | 303 | 0 | 0 | 274 | 0 | 0 | 779 | 0 |
| Heavy Vehicles (%) | 13% | 2% | 6% | 5% | 1% | 10% | 25% | 10% | 11% | 0% | 3% | 3% |
| | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | • | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | • | | 8 | | | 2 | _ | | 6 | | |
| Actuated Green, G (s) | • | 11.5 | | | 45.6 | | _ | 59.3 | | • | 59.3 | |
| Effective Green, g (s) | | 13.0 | | | 47.1 | | | 62.8 | | | 62.8 | |
| Actuated g/C Ratio | | 0.09 | | | 0.34 | | | 0.46 | | | 0.46 | |
| Clearance Time (s) | | 6.5 | | | 6.5 | | | 8.5 | | | 8.5 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | | 130 | | | 307 | | | 746 | | | 833 | |
| v/s Ratio Prot | | 100 | | | 001 | | | 7 10 | | | 000 | |
| v/s Ratio Perm | | c0.08 | | | c0.34 | | | 0.17 | | | c0.43 | |
| v/c Ratio | | 0.90 | | | 0.99 | | | 0.37 | | | 0.94 | |
| Uniform Delay, d1 | | 61.8 | | | 45.1 | | | 24.6 | | | 35.6 | |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | 48.3 | | | 47.6 | | | 0.3 | | | 17.4 | |
| Delay (s) | | 110.1 | | | 92.7 | | | 24.9 | | | 53.0 | |
| Level of Service | | F | | | F | | | C | | | D | |
| Approach Delay (s) | | 110.1 | | | 92.7 | | | 24.9 | | | 53.0 | |
| Approach LOS | | F | | | F | | | С | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 60.6 | H | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capacity r | atio | | 0.95 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 137.9 | Sı | um of lost | time (s) | | | 15.0 | | | |
| Intersection Capacity Utilization | | | 77.7% | IC | CU Level o | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-----------------------------------|-------|----------|--------|------|-----------|------------|---------|------|------|------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | ર્ન | 7 | | 414 | 7 | | 414 | 7 |
| Traffic Volume (vph) | 57 | 148 | 78 | 257 | 168 | 49 | 43 | 356 | 77 | 19 | 1598 | 105 |
| Future Volume (vph) | 57 | 148 | 78 | 257 | 168 | 49 | 43 | 356 | 77 | 19 | 1598 | 105 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | | | 5.0 | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 |
| Lane Util. Factor | | 1.00 | | | 1.00 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | 0.99 | | 1.00 | 0.98 | | 1.00 | 0.97 |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | | 0.96 | | | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| FIt Protected | | 0.99 | | | 0.97 | 1.00 | | 0.99 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1727 | | | 1828 | 1519 | | 3319 | 1464 | | 3564 | 1485 |
| FIt Permitted | | 0.69 | | | 0.60 | 1.00 | | 0.60 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (perm) | | 1196 | | | 1134 | 1519 | | 2012 | 1464 | | 3376 | 1485 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 57 | 148 | 78 | 257 | 168 | 49 | 43 | 356 | 77 | 19 | 1598 | 105 |
| RTOR Reduction (vph) | 0 | 10 | 0 | 0 | 0 | 29 | 0 | 0 | 37 | 0 | 0 | 51 |
| Lane Group Flow (vph) | 0 | 273 | 0 | 0 | 425 | 20 | 0 | 399 | 40 | 0 | 1617 | 54 |
| Confl. Peds. (#/hr) | 1 | | | | | 1 | 3 | | 1 | 1 | | 3 |
| Confl. Bikes (#/hr) | | | | | | 1 | | | 1 | | | |
| Heavy Vehicles (%) | 7% | 2% | 13% | 2% | 2% | 6% | 21% | 8% | 9% | 32% | 2% | 7% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 44.2 | | | 44.2 | 44.2 | | 57.2 | 57.2 | | 57.2 | 57.2 |
| Effective Green, g (s) | | 46.2 | | | 46.2 | 46.2 | | 59.7 | 59.7 | | 59.7 | 59.7 |
| Actuated g/C Ratio | | 0.40 | | | 0.40 | 0.40 | | 0.52 | 0.52 | | 0.52 | 0.52 |
| Clearance Time (s) | | 7.0 | | | 7.0 | 7.0 | | 7.5 | 7.5 | | 7.5 | 7.5 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 476 | | | 452 | 605 | | 1036 | 754 | | 1738 | 764 |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | | 0.23 | | | c0.37 | 0.01 | | 0.20 | 0.03 | | c0.48 | 0.04 |
| v/c Ratio | | 0.57 | | | 0.94 | 0.03 | | 0.39 | 0.05 | | 0.93 | 0.07 |
| Uniform Delay, d1 | | 27.2 | | | 33.5 | 21.2 | | 17.0 | 14.0 | | 26.2 | 14.1 |
| Progression Factor | | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | | 1.7 | | | 27.8 | 0.0 | | 0.2 | 0.0 | | 9.4 | 0.0 |
| Delay (s) | | 28.9 | | | 61.4 | 21.3 | | 17.2 | 14.0 | | 35.6 | 14.2 |
| Level of Service | | С | | | E | С | | В | В | | D | В |
| Approach Delay (s) | | 28.9 | | | 57.2 | | | 16.7 | | | 34.3 | |
| Approach LOS | | С | | | Е | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 34.6 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.93 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 115.9 | S | um of los | t time (s) | | | 10.0 | | | |
| Intersection Capacity Utilization | 1 | | 108.8% | | | of Service | | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|------------|----------|-------|------|------------|------------|---------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | | 7 | | | | 7 | ^ | | | † | 7 |
| Traffic Volume (vph) | 109 | 0 | 273 | 0 | 0 | 0 | 290 | 332 | 0 | 0 | 493 | 224 |
| Future Volume (vph) | 109 | 0 | 273 | 0 | 0 | 0 | 290 | 332 | 0 | 0 | 493 | 224 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.0 | | 5.0 | | | | 5.0 | 5.0 | | | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | | 1.00 | | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Frt | 1.00 | | 0.85 | | | | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | 0.95 | | 1.00 | | | | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | 1789 | | 1601 | | | | 1789 | 1883 | | | 1883 | 1601 |
| Flt Permitted | 0.95 | | 1.00 | | | | 0.45 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | 1789 | | 1601 | | | | 854 | 1883 | | | 1883 | 1601 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 112 | 0 | 281 | 0 | 0 | 0 | 299 | 342 | 0 | 0 | 508 | 231 |
| RTOR Reduction (vph) | 0 | 0 | 247 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 48 |
| Lane Group Flow (vph) | 112 | 0 | 34 | 0 | 0 | 0 | 299 | 342 | 0 | 0 | 508 | 183 |
| Heavy Vehicles (%) | 2% | 0% | 2% | 0% | 0% | 0% | 2% | 2% | 0% | 0% | 2% | 2% |
| Turn Type | Perm | | Perm | | | | Perm | NA | | | NA | Perm |
| Protected Phases | | | | | | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | | | | 2 | | | | | 6 |
| Actuated Green, G (s) | 13.1 | | 13.1 | | | | 92.0 | 92.0 | | | 92.0 | 92.0 |
| Effective Green, g (s) | 14.6 | | 14.6 | | | | 95.0 | 95.0 | | | 95.0 | 95.0 |
| Actuated g/C Ratio | 0.12 | | 0.12 | | | | 0.79 | 0.79 | | | 0.79 | 0.79 |
| Clearance Time (s) | 6.5 | | 6.5 | | | | 8.0 | 8.0 | | | 8.0 | 8.0 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | | 3.0 | 3.0 | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 218 | | 195 | | | | 678 | 1495 | | | 1495 | 1271 |
| v/s Ratio Prot | | | | | | | | 0.18 | | | 0.27 | |
| v/s Ratio Perm | c0.06 | | 0.02 | | | | c0.35 | | | | | 0.11 |
| v/c Ratio | 0.51 | | 0.18 | | | | 0.44 | 0.23 | | | 0.34 | 0.14 |
| Uniform Delay, d1 | 49.2 | | 47.1 | | | | 3.9 | 3.1 | | | 3.5 | 2.9 |
| Progression Factor | 1.00 | | 1.00 | | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.0 | | 0.4 | | | | 2.1 | 0.4 | | | 0.6 | 0.2 |
| Delay (s) | 51.2 | | 47.5 | | | | 6.0 | 3.4 | | | 4.1 | 3.1 |
| Level of Service | D | | D | | | | Α | Α | | | Α | Α |
| Approach Delay (s) | | 48.6 | | | 0.0 | | | 4.6 | | | 3.8 | |
| Approach LOS | | D | | | Α | | | Α | | | Α | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 14.0 | H | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.46 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 119.6 | | um of lost | | | | 11.5 | | | |
| Intersection Capacity Utiliza | ation | | 68.7% | IC | U Level o | of Service | | | С | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-----------------------------------|-------|----------|--------|------|------------|------------|---------|----------|------|-------|-------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | × | ર્ન | 7 | * | ^ | 7 | * | * 1> | |
| Traffic Volume (vph) | 0 | 0 | 0 | 595 | 0 | 59 | 0 | 915 | 245 | 139 | 1370 | 0 |
| Future Volume (vph) | 0 | 0 | 0 | 595 | 0 | 59 | 0 | 915 | 245 | 139 | 1370 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 1.0 | 5.0 | |
| Lane Util. Factor | | | | 0.95 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frt | | | | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | |
| Flt Protected | | | | 0.95 | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | | | | 1700 | 1700 | 1601 | | 3579 | 1601 | 1789 | 3579 | |
| FIt Permitted | | | | 0.95 | 0.95 | 1.00 | | 1.00 | 1.00 | 0.19 | 1.00 | |
| Satd. Flow (perm) | | | | 1700 | 1700 | 1601 | | 3579 | 1601 | 360 | 3579 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 0 | 0 | 0 | 613 | 0 | 61 | 0 | 943 | 253 | 143 | 1412 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 39 | 0 | 0 | 87 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 306 | 307 | 22 | 0 | 943 | 166 | 143 | 1412 | 0 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 2% | 0% | 2% | 0% | 2% | 2% | 2% | 2% | 0% |
| Turn Type | | | | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | | | | 40.0 | 40.0 | 40.0 | | 50.0 | 50.0 | 61.0 | 61.0 | |
| Effective Green, g (s) | | | | 42.0 | 42.0 | 42.0 | | 52.5 | 52.5 | 64.0 | 63.5 | |
| Actuated g/C Ratio | | | | 0.36 | 0.36 | 0.36 | | 0.45 | 0.45 | 0.55 | 0.55 | |
| Clearance Time (s) | | | | 7.0 | 7.0 | 7.0 | | 7.5 | 7.5 | 4.0 | 7.5 | |
| Vehicle Extension (s) | | | | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | | | 618 | 618 | 582 | | 1626 | 727 | 323 | 1967 | |
| v/s Ratio Prot | | | | | | | | 0.26 | | 0.04 | c0.39 | |
| v/s Ratio Perm | | | | 0.18 | 0.18 | 0.01 | | | 0.10 | 0.21 | | |
| v/c Ratio | | | | 0.50 | 0.50 | 0.04 | | 0.58 | 0.23 | 0.44 | 0.72 | |
| Uniform Delay, d1 | | | | 28.5 | 28.5 | 23.7 | | 23.3 | 19.2 | 14.8 | 19.3 | |
| Progression Factor | | | | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | | | | 0.6 | 0.6 | 0.0 | | 1.5 | 0.7 | 1.0 | 2.3 | |
| Delay (s) | | | | 29.1 | 29.2 | 23.7 | | 24.8 | 19.9 | 15.8 | 21.6 | |
| Level of Service | | 0.0 | | С | C | С | | C | В | В | C | |
| Approach Delay (s) | | 0.0 | | | 28.7 | | | 23.8 | | | 21.1 | |
| Approach LOS | | Α | | | С | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 23.5 | H | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.67 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 115.5 | | um of lost | | | | 16.0 | | | |
| Intersection Capacity Utilization | 1 | | 112.3% | IC | U Level of | of Service | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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Appendix D: Evaluation of Active Transportation Facilities on Teston Road

TABLE 1: MMLOS INTERSECTION ANALYSIS AT TESTON ROAD AND JANE STREET

| | | | | | Intersection | Approach ² | |
|----------------------------|---|-------------------------------|-------------------|---------------|---------------|-----------------------|---------------|
| | Criteria (Intersection A | naly | sis) ¹ | Jane | Street | Testor | n Road |
| | | | | NB | SB | EB | WB |
| | Automobile | Dela | ay (seconds) | 25 | 33 | 44 | 42 |
| Auto | Performance at the Intersection Approach | | ume to pacity | 0.55 (NBL) | 0.48 (SBT) | 0.67 (EBT) | 0.79 (WBT) |
| | Auto Level of Serv (AL | vice OS) | Target = D | С | С | D | D |
| | Sidewalk / Multi-Use Pa (Dimension) | th Wi | dth | 1.5m | None | 1.5m | None |
| an 3 | Buffer / Boulevard (Dimension) | | 1.0m | None | 1.0m | None | |
| Pedestrian ³ | Signalized Crossing (Ye | ignalized Crossing (Yes / No) | | Yes | Yes | Yes | Yes |
| Ped | Crosswalk (Yes / No) | | | Yes | Yes | Yes | Yes |
| | Pedestrian Leve Service (PL | - | Target = C | В | F | В | F |
| | Separated, Dedicated o | r Sha | red ⁴ | None | Dedicated | None | None |
| o o | Bicycle Facility Width (D | imen | ision) | 1 | 1.25m | 1 | - |
| Bicycle | Buffer (Yes / No) | | | No | No | No | No |
| Θ | Bicycle Treatment (e.g. signal head, etc.) | | box, bicycle | No | No | No | No |
| | Bicycle Level of Serv (BL | vice OS) | Target = C | F | D | F | F |
| | Transit Service Frequen (minutes) ⁷ | ıcy – | Headway | - | - | 12 | - |
| 0 & 6 | Transit Service Leve Service (TSL | - | Target = C | N/A | N/A | С | N/A |
| Transit ^{5 &} | Transit Vehicle Performance at the | Dela | ay (seconds) | - | - | 36 | - |
| Tra | Intersection Approach | I | ume to pacity | - | - | 0.16 (EBR) | - |
| | Transit Performa Level of Service (TPL rall LOS for each mode is ba | OS) | Target = D | N/A | N/A | D | N/A |

¹ Overall LOS for each mode is based on the worst-case criteria.

² All modes evaluated in direction of travel for each intersection approach.

³ Pedestrian facility referenced York Region Transportation Master Plan – Map 5: Sidewalk Gaps on Regional Roads dated May 12th, 2016.

⁴ Bicycle facility type referenced York Region Transportation Master Plan – Map 4: Existing Cycling Network dated May 12, 2016.

⁵ Transit evaluation based on York Region System Map dated September 6, 2020.

⁶ Transit LOS evaluation does not include "Access to Transit Stops, Stations or Transfer Points" since this criterion is development related.

⁷ Transit headway provided by YRT based on October 2019 conditions (pre-COVID).

⁸ Transit Vehicle Performance evaluated based on the transit movement at the intersection.

TABLE 2: MMLOS SEGMENT ANALYSIS ON TESTON ROAD BETWEEN JANE STREET TO KEELE STREET

| | | | | Mid-Block | Segment |
|-----------------------|---|-------------|--------------------------------|---------------|---------------|
| | Criteria (Segment Ana | alysis |) ¹ | Testor | Road |
| | | | | EB | WB |
| | Automobile | Dela 3 | ay (seconds) ² | 49 | 42 |
| Auto | Performance at the Intersection Approach | 1 | ume to pacity ²³ | 0.46 (EBR) | 0.79 (WBT) |
| | Auto Level of Ser (AL | vice OS) | Target = D | D | D |
| 4. | Sidewalk / Multi-Use Pa (Dimension) | ath W | idth | 3.0m | - |
| Pedestr. ⁴ | Buffer / Boulevard (Dim | ensic | on) | 4.0m | - |
| Pe | Pedestrian Leve Service (PL | - | Target = C | A | F |
| | Separated, Dedicated of | or Sha | ared ⁵ | Separated | None |
| Bicycle | Bicycle Facility Width ([| Dimer | nsion) | 3.0m | - |
| Bic | Buffer (Yes / No) | | | Yes | - |
| | Bicycle Level of Ser (BL | vice OS) | Target = C | A | F |
| | Transit Service Freque | ncy (H | Headway) ⁸ | - | - |
| 6.7 | Transit Service Leve Service (TSL | | Target = C | N/A | N/A |
| Fransit ⁶⁷ | Transit Vehicle Performance at the | Dela | ay (seconds) | - | - |
| Tra | Intersection Approach | | ume to acity | - | - |
| | Transit Performa Level of Service (TPL | | Target = D | N/A | N/A |

¹ Overall LOS for each mode is based on the worst-case criteria.

² EB segment delay and v/c ratio are for the EB approach to Keele Street.

³ WB segment delay and v/c ratio are for the WB approach to Jane Street.

⁴ Pedestrian facility referenced York Region Transportation Master Plan – Map 5: Sidewalk Gaps on Regional Roads dated May 12th, 2016.

⁵ Bicycle facility type referenced York Region Transportation Master Plan – Map 4: Existing Cycling Network dated May 12, 2016.

⁶ Transit evaluation based on York Region System Map dated September 6, 2020.

⁷ Transit LOS evaluation does not include "Access to Transit Stops, Stations or Transfer Points" since this criterion is development related or "Boarding Volumes" since it is not available.

⁸ Transit headway provided by YRT based on October 2019 conditions (pre-COVID).

⁹ Transit Vehicle Performance evaluated based on the transit movement at the intersection.

TABLE 3: MMLOS INTERSECTION ANALYSIS AT TESTON ROAD AND KEELE STREET

| | | | | | Intersection | Approach ² | |
|-----------------|--|--------------|-----------------------|--------------------|--------------------|-----------------------|----------------|
| | Criteria (Intersection A | Analy | rsis) ¹ | Keele | Street | Testor | n Road |
| | | | | NB | SB | EB | WB |
| | Automobile | Dela | ay (seconds) | 23 | 32 | 49 | 46 |
| Auto | Performance at the Intersection Approach | 1 | ıme to acity | 0.58 (NBL) | 0.63 (SBT) | 0.46 (EBR) | 0.10 (WBTR) |
| | Auto Level of Ser (AL | vice .OS) | Target = D | C | C | D | D |
| | Sidewalk / Multi-Use Pa (Dimension) | ath W | idth | - | - | 3.0m | - |
| an ³ | Buffer / Boulevard (Dim | ensio | n) | - | - | 5.0m | - |
| Pedestrian | Signalized Crossing (Ye | es / N | o) | Yes | Yes | Yes | Yes |
| Ped | Crosswalk (Yes / No) | | | Yes | Yes | Yes | Yes |
| | Pedestrian Leve Service (PL | | Target = C | F | F | Α | F |
| | Separated, Dedicated o | r Sha | ared ⁴ | None | None | Separated | None |
| o d | Bicycle Facility Width ([| Dimer | nsion) | - | - | 3.0m | - |
| Bicycle | Buffer (Yes / No) | | | No | No | Yes | No |
| Bi | Bicycle Treatment (e.g. signal head, etc.) | | box, bicycle | No | No | No | No |
| | Bicycle Level of Ser (BL | vice .OS) | Target = C | F | F | Α | F |
| | Transit Service Frequer | ncy (H | leadway) ⁷ | 25 – 32 minutes | 25 – 32 minutes | 19 minutes | - |
| 5 & 6 | Transit Service Leve Service (TSL | | Target = C | E/F | E/F | D | N/A |
| Transit | Transit Vehicle Performance at the | Dela | ay (seconds) | 15 | 32 | 49 | - |
| Tra | Intersection Approach | Сар | ıme to acity | 0.14 (NBT) | 0.63 (SBT) | 0.46 (EBR) | - |
| | Transit Performa Level of Service (TPL all LOS for each mode is be | OS) | Target = D | В | С | D | N/A |

¹ Overall LOS for each mode is based on the worst-case criteria.

² All modes evaluated in direction of travel for each intersection approach.

³ Pedestrian facility referenced York Region Transportation Master Plan – Map 5: Sidewalk Gaps on Regional Roads dated May 12th, 2016.

⁴ Bicycle facility type referenced York Region Transportation Master Plan – Map 4: Existing Cycling Network dated May 12, 2016.

⁵ Transit evaluation based on York Region System Map dated September 6, 2020.

⁶ Transit LOS evaluation does not include "Access to Transit Stops, Stations or Transfer Points" since this criterion is development related.

⁷ Transit headway provided by YRT based on October 2019 conditions (pre-COVID).

⁸ Transit Vehicle Performance evaluated based on the transit movement at the intersection.

TABLE 4: MMLOS INTERSECTION ANALYSIS AT TESTON ROAD AND DUFFERIN STREET

| | | | | | Intersection | Approach ² | |
|-------------------------|---|---|-----------------------|---------------|---------------|-----------------------------|---------------|
| | Criteria (Intersection A | Analy | rsis) ¹ | Dufferi | n Street | Testo | n Road |
| | | | | NB | SB | EB | WB |
| | Automobile | Dela | ay (seconds) | 38 | 72 | 44 | 85 |
| Auto | Performance at the Intersection Approach | | ume to acity | 0.49 (NBT) | 1.00 (SBT) | 0.01 (EBTR) | 1.06 (WBL) |
| | Auto Level of Serv (AL | | Target = D | D | E | D | F |
| | Sidewalk / Multi-Use Pa (Dimension) | / Multi-Use Path Width | | - | - | 1.5m | - |
| Pedestrian ³ | Buffer / Boulevard (Dimension) | | | - | - | Varies (>1.0m buffer) | - |
| dest | Signalized Crossing (Ye | alized Crossing (Yes / No) | | Yes | Yes | Yes | Yes |
| Pe | Crosswalk (Yes / No) | | | Yes | Yes | Yes | Yes |
| | Pedestrian Leve Service (PL | | Target = C | F | F | В | F |
| | Separated, Dedicated o | r Sha | ared ⁴ | Dedicated | Dedicated | None | Dedicated |
| Ф | Bicycle Facility Width (| Dimer | nsion) | 2.0m | 2.0m | - | 1.5m |
| Bicycle | Buffer (Yes / No) | | | No | No | No | No |
| B | Bicycle Treatment (e.g. signal head, etc.) | bike | box, bicycle | No | No | No | No |
| | Bicycle Level of Serv (BL | | Target = C | В | В | F | D |
| | Transit Service Frequer | псу (Н | leadway) ⁷ | - | - | - | - |
| 5 & 6 | | ransit Service Level of Service (TSLOS) Target = C | | N/A | N/A | N/A | N/A |
| ısit ⁵ | Transit Vehicle Performance at the | cle e at the Approach Volume to Capacity | | - | - | - | - |
| Transit | Intersection Approach | | | - | - | - | - |
| | Transit Performa Level of Service (TPL | OS) | Target = D | N/A | N/A | N/A | N/A |

Overall LOS for each mode is based on the worst-case criteria.

² All modes evaluated in direction of travel for each intersection approach.

³ Pedestrian facility referenced York Region Transportation Master Plan – Map 5: Sidewalk Gaps on Regional Roads dated May 12th, 2016.

⁴ Bicycle facility type referenced York Region Transportation Master Plan – Map 4: Existing Cycling Network dated May 12, 2016.

⁵ Transit evaluation based on York Region System Map dated September 6, 2020.

⁶ Transit LOS evaluation does not include "Access to Transit Stops, Stations or Transfer Points" since this criterion is development related.

⁷ Transit headway provided by YRT based on October 2019 conditions (pre-COVID).

⁸ Transit Vehicle Performance evaluated based on the transit movement at the intersection.

TABLE 5: MMLOS SEGMENT ANALYSIS ON TESTON ROAD BETWEEN DUFFERIN STREET TO BATHURST STREET

| | | | | Mid-Block | Segment |
|------------------------------|---|-------------|--------------------------------|---------------|---------------|
| | Criteria (Segment Ana | lysis |) ¹ | Testor | n Road |
| | | | | EB | WB |
| | Automobile | Dela 3 | ay (seconds) ² | 101 | 85 |
| Auto | Performance at the Intersection Approach | | ume to acity ^{2 3} | 0.97 (EBL) | 1.06 (WBL) |
| | Auto Level of Ser (AL | vice OS) | Target = D | F | F |
| 4. | Sidewalk / Multi-Use Pa (Dimension) | th W | dth | - | - |
| Pedestr. ⁴ | Buffer / Boulevard (Dim | ensio | n) | - | - |
| Pe | Pedestrian Leve Service (PL | | Target = C | F | F |
| | Separated, Dedicated o | r Sha | red ⁵ | Dedicated | Dedicated |
| /cle | Bicycle Facility Width (D | Dimer | ision) | 1.5m | 1.5m |
| Bicycle | Buffer (Yes / No) | | | No | No |
| | Bicycle Level of Ser (BL | vice OS) | Target = C | D | D |
| | Transit Service Frequer | псу (Н | leadway) ⁸ | - | - |
| 8 7 | Transit Service Leve Service (TSL | | Target = C | N/A | N/A |
| Transit ^{6 & 7} | Transit Vehicle Performance at the | Dela | ay (seconds) | - | - |
| Tra | Intersection Approach | | ume to acity | - | - |
| | Transit Performa | | Target = D | N/A | N/A |

¹ Overall LOS for each mode is based on the worst-case criteria.

² EB segment delay and v/c ratio are for the EB approach to Bathurst Street.

³ WB segment delay and v/c ratio are for the WB approach to Dufferin Street.

⁴ Pedestrian facility referenced York Region Transportation Master Plan – Map 5: Sidewalk Gaps on Regional Roads dated May 12th, 2016.

⁵ Bicycle facility type referenced York Region Transportation Master Plan – Map 4: Existing Cycling Network dated May 12, 2016.

⁶ Transit evaluation based on York Region System Map dated September 6, 2020.

⁷ Transit LOS evaluation does not include "Access to Transit Stops, Stations or Transfer Points" since this criterion is development related or "Boarding Volumes" since it is not available.

⁸ Transit headway provided by YRT based on October 2019 conditions (pre-COVID).

⁹ Transit Vehicle Performance evaluated based on the transit movement at the intersection.

TABLE 6: MMLOS INTERSECTION ANALYSIS AT TESTON ROAD / ELGIN MILLS ROAD WEST AND BATHURST STREET

| | | | Intersection | Approach ² | | | |
|------------------|---|-----------------------|--------------------------|--|---------------|--|---------------|
| | Criteria (Intersection A | analy | sis) ¹ | Bathurs | st Street | Testo | n Road |
| | | | | NB | SB | EB | WB |
| | Automobile | Dela | ay (seconds) | 95 | 28 | 101 | 146 |
| Auto | Performance at the Intersection Approach | Cap | ume to pacity | 0.73 (NBL) | 0.82 (SBT) | 0.97 (EBL) | 1.13 (WBL) |
| | Auto Level of Serv (AL | | Target = D | F | С | F | F |
| | Sidewalk / Multi-Use Pa (Dimension) | th W | idth | 1.5m | 1.5m | 1.5m | 1.5m |
| ian ³ | Buffer / Boulevard (Dim | ensio | n) | 2.5m | 2.0m | 7.0m | 1.5m |
| estri | Signalized Crossing (Ye | s / N | o) | Yes | Yes | Yes | Yes |
| Pedestrian | Crosswalk (Yes / No) | | | Yes | Yes | Yes | Yes |
| | Pedestrian Leve Service (PL | | Target = C | В | В | В | В |
| | Separated, Dedicated o | r Sha | ared ⁴ | None | None | None | None |
| o o | Bicycle Facility Width (D | imer | nsion) | - | - | - | - |
| Bicycle | Buffer (Yes / No) | | | No | No | No | No |
| Bi | Bicycle Treatment (e.g. signal head, etc.) | | box, bicycle | No | No | No | No |
| | Bicycle Level of Serv (BL | vice OS) | Target = C | F | F | F | F |
| | Transit Service Frequer | leadway) ⁷ | 15 minutes (Route 88) | 15 minutes (Route 88) 29 minutes (Route 80) | - | 29 minutes (Route 80) 35 minutes (Route 83) | |
| nsit 5&6 | Transit Service Leve Service (TSL | | Target = C | С | E | N/A | F |
| Transit | Transit Vehicle Performance at the | Dela | ay (seconds) | 26 | 28 | - | 42 |
| - | Intersection Approach | Cap | ume to pacity | 0.53 (NBT) | 0.82 (SBT) | - | 0.05 (WBR) |
| | Transit Performa | OS) | Target = D | С | С | N/A | D |

¹ Overall LOS for each mode is based on the worst-case criteria.

² All modes evaluated in direction of travel for each intersection approach.

³ Pedestrian facility referenced York Region Transportation Master Plan – Map 5: Sidewalk Gaps on Regional Roads dated May 12th, 2016.

⁴ Bicycle facility type referenced York Region Transportation Master Plan – Map 4: Existing Cycling Network dated May 12, 2016.

⁵ Transit evaluation based on York Region System Map dated September 6, 2020.

⁶ Transit LOS evaluation does not include "Access to Transit Stops, Stations or Transfer Points" since this criterion is development related.

⁷ Transit headway provided by YRT based on October 2019 conditions (pre-COVID).

⁸ Transit Vehicle Performance evaluated based on the transit movement at the intersection.

Appendix E: A Summary of All Collisions Involving Pedestrians and Cyclists

Table 1: Summary of Collisions in the Project Study Area involving Cyclists

| # | Date | Location | Vehicle Type | Impact Type | Classification of Collision | Driver Condition / Action | Cyclist Condition / Action | Environmental Condition | Light Condition | Surface Condition |
|---|-----------|--|----------------------|---------------------|-----------------------------|---|---|----------------------------|--------------------|----------------------|
| 1 | 7/24/2018 | Bathurst Street & Regent Street/Lady Nadia Drive | Passenger Vehicle | Angle | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Driving Properly | Clear | Daylight | Dry |
| 2 | 8/1/2015 | Dufferin Street b/w Sir Benson Drive & Teston Road | Passenger Vehicle | Rear End | Fatal | Normal / Driving Properly | Ability Impaired (Drugs) / Failed to Field Right- of-Way | Clear | Dark | Dry |
| 3 | 4/24/2015 | Jane Street & Roseheath Drive/Grand Valley Boulevard | Passenger Vehicle | Turning Movement | P.D. Only | Unknown / Driving Properly | Normal / Failed to Field Right- of-Way | Clear | Daylight | Dry |
| 4 | 5/1/2017 | Jane Street & Roseheath Drive/Grand Valley Boulevard | Pick-up Truck | Angle | Non-Fatal | Unknown / Other | Normal / Driving Properly | Rain | Daylight | Wet |
| 5 | 10/8/2017 | Jane Street btwn Major Mackenzie Drive West & Roseheath Drive/Grand Valley Boulevard | Passenger Vehicle | Angle | Non-Fatal | Normal / Other | Normal / Other | Clear | Daylight | Dry |
| 6 | 10/1/2016 | Jane Street btwn Teston Road & Kirby Road | Passenger Vehicle | Other (SMV) | P.D. Only | Normal / Improper Passing | Normal / Driving Properly | Rain | Dark | Wet |
| 7 | 7/2/2016 | Keele Street & Major Mackenzie Drive West | Passenger Vehicle | Angle | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Driving Properly | Clear | Daylight | Dry |
| 8 | 9/23/2016 | Keele Street & Major Mackenzie Drive West | Passenger Vehicle | Turning Movement | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Driving Properly | Clear | Daylight | Dry |
| 9 | 9/6/2018 | Keele Street & Major Mackenzie Drive West | Passenger Vehicle | Angle | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Driving Properly | Clear | Daylight | Dry |

| # | Date | Location | Vehicle Type | Impact Type | Classification of Collision | Driver Condition / Action | Cyclist Condition / Action | Environmental Condition | Light Condition | Surface Condition |
|----|------------|---|----------------------|---------------------|-----------------------------|--|--|----------------------------|----------------------|----------------------|
| 10 | 10/15/2015 | Keele Street & Teston Road | Dump Truck | Turning Movement | Non-Fatal | Normal / Improper Passing | Normal / Driving Properly | Clear | Daylight | Dry |
| 11 | 6/7/2018 | Keele Street & Teston Road | Passenger Vehicle | Sideswipe | P.D. Only | Normal / Driving Properly | Normal / Driving Properly | Clear | Daylight | Dry |
| 12 | 3/14/2019 | Major Mackenzie Dr. & Fortinos / Longos Entrance | Unknown | Angle | P.D. Only | / Improper Turn | / Improper Passing | Clear | Daylight | Dry |
| 13 | 6/30/2018 | Major Mackenzie Drive West & Avro Road/McNaughton Road | Passenger Vehicle | Angle | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Failed to Field Right- of-Way | Clear | Daylight | Dry |
| 14 | 6/28/2018 | Major Mackenzie Drive West & Exit 35 | Passenger Vehicle | Angle | P.D. Only | Normal / Failed to Field Right- of-Way | 01 - Normal / Driving Properly | Clear | Daylight | Dry |
| 15 | 8/9/2018 | Major Mackenzie Drive West & Exit 35 | Passenger Vehicle | Sideswipe | P.D. Only | Unknown / Improper Lane Change | Normal / Driving Properly | Clear | Daylight | Dry |
| 16 | 5/14/2019 | Major Mackenzie Drive West & Exit 35 | Passenger Vehicle | Angle | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Driving Properly | Clear | Daylight | Dry |
| 17 | 8/26/2019 | Major Mackenzie Drive West & Exit 35 | Passenger Vehicle | Sideswipe | P.D. Only | Normal / Failed to Field Right- of-Way | Normal / Driving Properly | Clear | Dusk | Wet |
| 18 | 6/25/2019 | Major Mackenzie Drive West & Jane Street | Passenger Vehicle | Angle | Non-Fatal | Inattentive / Failed to Field Right- of-Way | Normal / Driving Properly | Clear | Dusk | Dry |
| 19 | 11/19/2015 | Major Mackenzie Drive West & Melville Avenue | Passenger Vehicle | Turning Movement | Non-Fatal | Inattentive / Lost Control | Normal / Driving Properly | Clear | Dark (Artificial) | Dry |
| 20 | 9/28/2018 | Major Mackenzie Drive West btwn Exit 35/GO Carpool Lot - Hwy 400 & Major Mackenzie Drive West & Exit 35 | Pick-up Truck | Sideswipe | Non-Fatal | Normal / Driving Properly | Normal / Driving Properly | Clear | Daylight | Dry |

| # | Date | Location | Vehicle Type | Impact Type | Classification of Collision | Driver Condition / Action | Cyclist Condition / Action | Environmental Condition | Light Condition | Surface Condition |
|----|-----------|--|----------------------|---------------------|-----------------------------|---|----------------------------------|----------------------------|--------------------|----------------------|
| 21 | 5/31/2019 | Major Mackenzie Drive West btwn Grand Trunk Avenue & Dufferin Street | Passenger Vehicle | Angle | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Other | Clear | Daylight | Dry |
| 22 | 6/18/2016 | Major Mackenzie Drive West btwn Ontario Street & Entrance to Vaughan Municipal Offices | Passenger Vehicle | Angle | Non-Fatal | Normal / Driving Properly | Normal / Driving Properly | Clear | Daylight | Dry |
| 23 | 9/20/2016 | Teston Road & Exit 37 | Passenger Vehicle | Turning Movement | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Driving Properly | Clear | Daylight | Dry |

Table 2: Summary of Collisions in the Project Study Area involving Pedestrians

| # | Date | Location | Vehicle Type | Impact Type | Classification of Collision | Driver Condition / Action | Pedestrian Condition / Action | Environmental Condition | Light Condition | Surface Condition |
|----|------------|---|----------------------|----------------|-----------------------------|--|---|----------------------------|----------------------|----------------------|
| 1 | 11/23/2016 | Bathurst Street & Mill Street/Queen Filomena Avenue | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Failed to Field Right- of-Way | Normal / Crossing w/ Right-of-Way | Rain | Dark (Artificial) | Wet |
| 2 | 10/31/2018 | Bathurst Street & Woodland Acres Crescent | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Driving Properly | Inattentive / Crossing without Right- of-Way | Rain | Daylight | Wet |
| 3 | 4/18/2017 | Bathurst Street & Gamble Road | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 4 | 10/24/2018 | Bathurst Street btwn Regent Street/Lady Nadia Drive & Oxford Street/Lady Dolores Avenue | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Driving Properly | Inattentive / Running onto Roadway | Clear | Dark | Wet |
| 5 | 6/28/2018 | Jane Street & Ahmadiyya Avenue (979F083B) | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Driving Properly | Normal / Crossing without Right- of-Way | Clear | Daylight | Dry |
| 6 | 9/26/2017 | Jane Street & America Avenue/Brandon Gate Drive | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Dark (Artificial) | Dry |
| 7 | 10/11/2017 | Jane Street & America Avenue/Brandon Gate Drive | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Rain | Dawn | Wet |
| 8 | 5/9/2018 | Jane Street & America Avenue/Brandon Gate Drive | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Driving Properly | Normal / Crossing without Right- of-Way | Clear | Dark (Artificial) | Dry |
| 9 | 10/1/2018 | Jane Street & America Avenue/Brandon Gate Drive | Passenger Vehicle | Other (SMV) | Non-Fatal | Inattentive / Failed to Field Right- of-Way | Inattentive / Crossing with Right-of-Way | Rain | Dark | Wet |
| 10 | 12/26/2018 | Jane Street & America Avenue/Brandon Gate Drive | Passenger Vehicle | Other (SMV) | Non-Fatal | Inattentive / Disobeyed Traffic Control | Normal / Crossing with Right-of-Way | Clear | Dark | Dry |

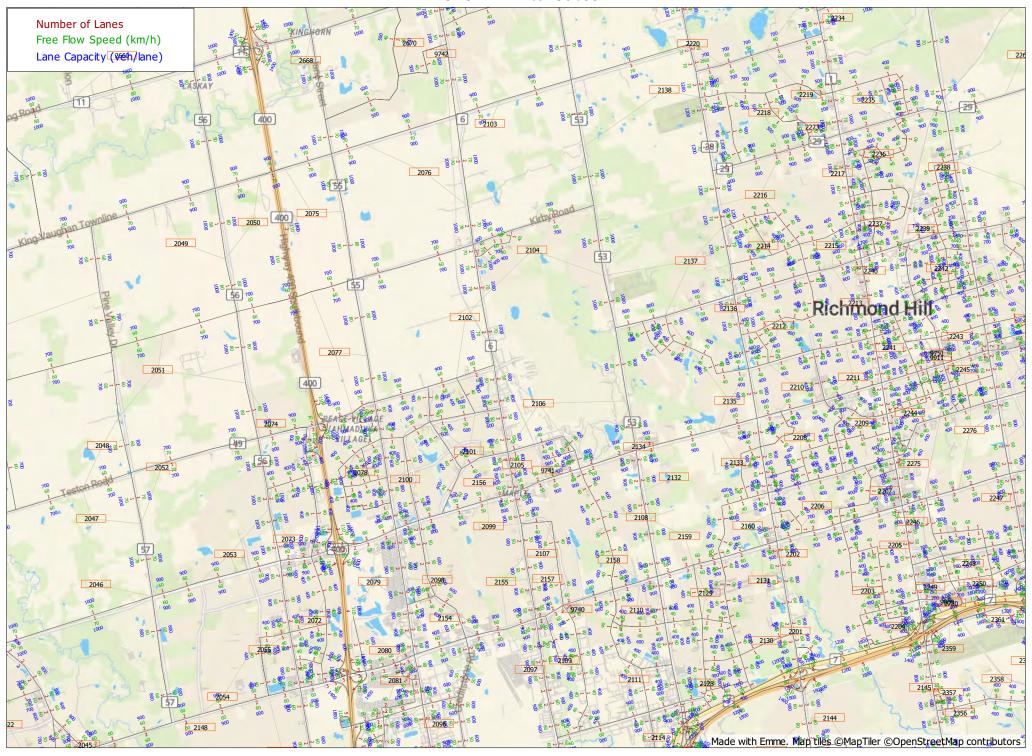
| # | Date | Location | Vehicle Type | Impact Type | Classification of Collision | Driver Condition / Action | Pedestrian Condition / Action | Environmental Condition | Light Condition | Surface Condition |
|----|------------|---|----------------------|----------------|-----------------------------|--|--|----------------------------|----------------------|----------------------|
| 11 | 12/13/2019 | Jane Street & America Avenue/Brandon Gate Drive | Passenger Vehicle | Other (SMV) | Non-Fatal | Inattentive / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 12 | 10/10/2015 | Jane Street & Roseheath Drive/Grand Valley Boulevard | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Improper Turn | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 13 | 9/3/2016 | Jane Street & Roseheath Drive/Grand Valley Boulevard | Pick-up Truck | Other (SMV) | Non-Fatal | Unknown / Improper Turn | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 14 | 2/16/2017 | Jane Street & Roseheath Drive/Grand Valley Boulevard | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 15 | 5/3/2015 | Keele Street & Major Mackenzie Drive West | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Driving Properly | Normal / Crossing without Right- of-Way | Clear | Daylight | Dry |
| 16 | 10/10/2017 | Keele Street & Major Mackenzie Drive West | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Driving Properly | Normal / Crossing without Right- of-Way | Clear | Dark (Artificial) | Dry |
| 17 | 2/10/2018 | Keele Street & Major Mackenzie Drive West | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Dark (Artificial) | Wet |
| 18 | 6/12/2019 | Keele Street & Major Mackenzie Drive West | School Bus | Other (SMV) | Non-Fatal | Unknown / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 19 | 1/3/2017 | Keele Street & Peak Point Boulevard | Passenger Vehicle | Other (SMV) | Non-Fatal | Inattentive / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Rain | Dark (Artificial) | Wet |
| 20 | 11/9/2015 | Keele Street & Railway Street/Killian Road | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 21 | 11/2/2018 | Major Mackenzie Drive West & Bathurst Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Rain | Dark | Wet |

| # | Date | Location | Vehicle Type | Impact Type | Classification of Collision | Driver Condition / Action | Pedestrian Condition / Action | Environmental Condition | Light Condition | Surface Condition |
|----|------------|--|----------------------|----------------|-----------------------------|--|---|----------------------------|----------------------|----------------------|
| 22 | 3/17/2019 | Major Mackenzie Drive West & Bathurst Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Inattentive / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 23 | 9/10/2016 | Major Mackenzie Drive West & Dufferin Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Improper Turn | Normal / Crossing with Right-of-Way | Clear | Dusk | Dry |
| 24 | 12/27/2016 | Major Mackenzie Drive West & Dufferin Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Inattentive / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Snow | Dark (Artificial) | Wet |
| 25 | 2/15/2019 | Major Mackenzie Drive West & Dufferin Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Other | Normal / Crossing with Right-of-Way | Clear | Daylight | Wet |
| 26 | 10/21/2015 | Major Mackenzie Drive West & Exit 35 | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 27 | 5/15/2016 | Major Mackenzie Drive West & Jane Street | Passenger Vehicle | Other (SMV) | P.D. Only | Fatigue / Improper Turn | Medical or Physical Disability / Crossing with Right-of-Way | Snow | Daylight | Wet |
| 28 | 9/21/2017 | Major Mackenzie Drive West & Jane Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Dark (Artificial) | Dry |
| 29 | 1/25/2018 | Major Mackenzie Drive West & Jane Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Inattentive / Improper Turn | Normal / Crossing with Right-of-Way | Fog, Mist, Smoke, Dust | Dark | Dry |
| 30 | 12/21/2018 | Major Mackenzie Drive West & Jane Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Rain | Dawn | Wet |
| 31 | 4/4/2016 | Major Mackenzie Drive West & Netherford Road/Killian Road | Passenger Vehicle | Other (SMV) | P.D. Only | Unknown / Driving Properly | Inattentive / Crossing without Right- of-Way | Clear | Daylight | Dry |
| 32 | 10/7/2018 | Major Mackenzie Drive West & Netherford Road/Killian Road | Passenger Van | Other (SMV) | Non-Fatal | Inattentive / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Daylight | Wet |

| # | Date | Location | Vehicle Type | Impact Type | Classification of Collision | Driver Condition / Action | Pedestrian Condition / Action | Environmental Condition | Light Condition | Surface Condition |
|----|-----------|---|----------------------|----------------|-----------------------------|--|--|----------------------------|--------------------|----------------------|
| 33 | 3/25/2015 | Major Mackenzie Drive West & Peter Rupert Avenue/McNaughton Road East | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Rain | Daylight | Wet |
| 34 | 5/22/2016 | Major Mackenzie Drive West & Peter Rupert Avenue/McNaughton Road East | Passenger Van | Other (SMV) | Non-Fatal | Normal / Driving Properly | Normal / Crossing without Right- of-Way | Clear | Daylight | Dry |
| 35 | 6/11/2018 | Major Mackenzie Drive West & Peter Rupert Avenue/McNaughton Road East | Passenger Van | Other (SMV) | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 36 | 11/6/2019 | Major Mackenzie Drive West & Peter Rupert Avenue/McNaughton Road East | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Failed to Field Right- of-Way | Normal / Crossing with Right-of-Way | Rain | Dark | Wet |
| 37 | 6/29/2016 | Major Mackenzie Drive West & Sir Benson Drive | Pick-up Truck | Other (SMV) | Non-Fatal | Normal / Other | Normal / Crossing with Right-of-Way | Clear | Daylight | Dry |
| 38 | 9/27/2019 | Major Mackenzie Drive West btwn Entrance to Vaughan Municipal Offices & Hill Street | Truck | Other (SMV) | Non-Fatal | Unknown / Improper Passing | Normal / Other | Clear | Daylight | Dry |
| 39 | 6/21/2018 | Major Mackenzie Drive West btwn Grand Trunk Avenue & Dufferin Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Normal / Driving Properly | Normal / Crossing without Right- of-Way | Clear | Daylight | Dry |
| 40 | 3/3/2016 | Major Mackenzie Drive West btwn Jackson Street & Keele Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Failed to Field Right- of-Way | Normal / On Sidewalk or Shoulder | Clear | Daylight | Dry |
| 41 | 3/1/2017 | Major Mackenzie Drive West btwn Jackson Street & Keele Street | Passenger Vehicle | Other (SMV) | Non-Fatal | Unknown / Driving Properly | Normal / Running onto Roadway | Rain | Dark | Wet |

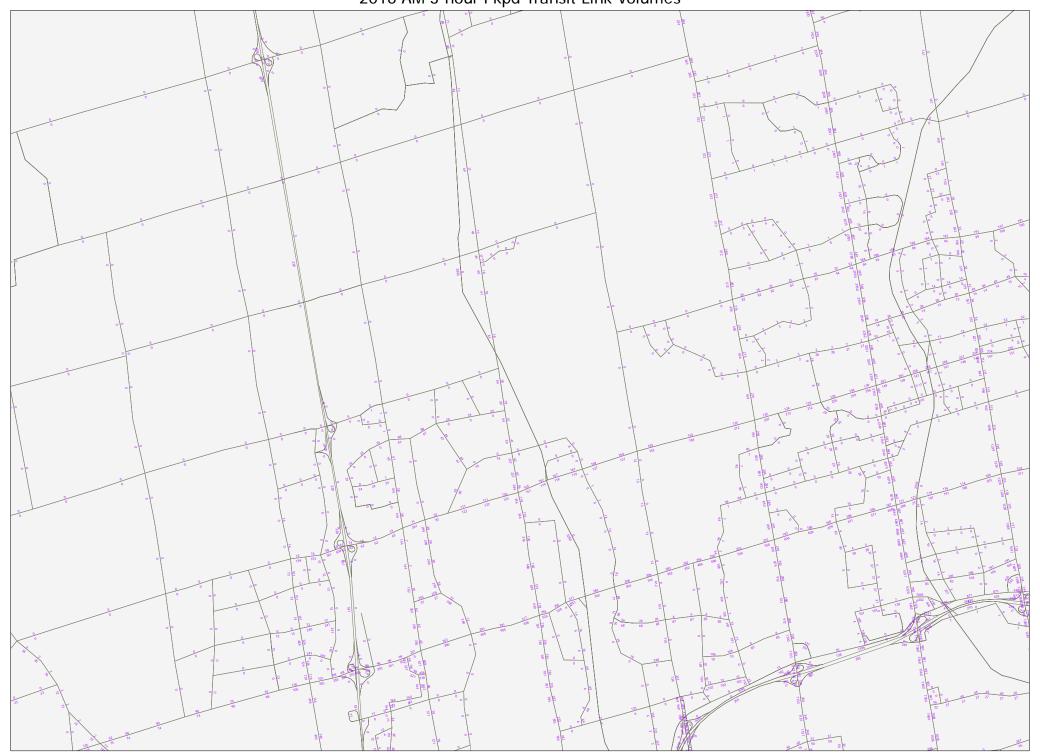
Appendix F: 2016 Snapshot of EMME Subarea Network

2016 Link Attributes



 $\label{limited} \begin{tabular}{lll} YRTDF Model-2016_March-2020 (I:/EMME/Emme_4_Modelling_in_2020_MASTER/Database/Model-2016_March-2020/emmebank) \\ Scenario 7121: 2016 MASTER Apr15-2020 \\ 2020-06-04 \end{tabular}$

2016 AM 3-hour Pkpd Transit Link Volumes



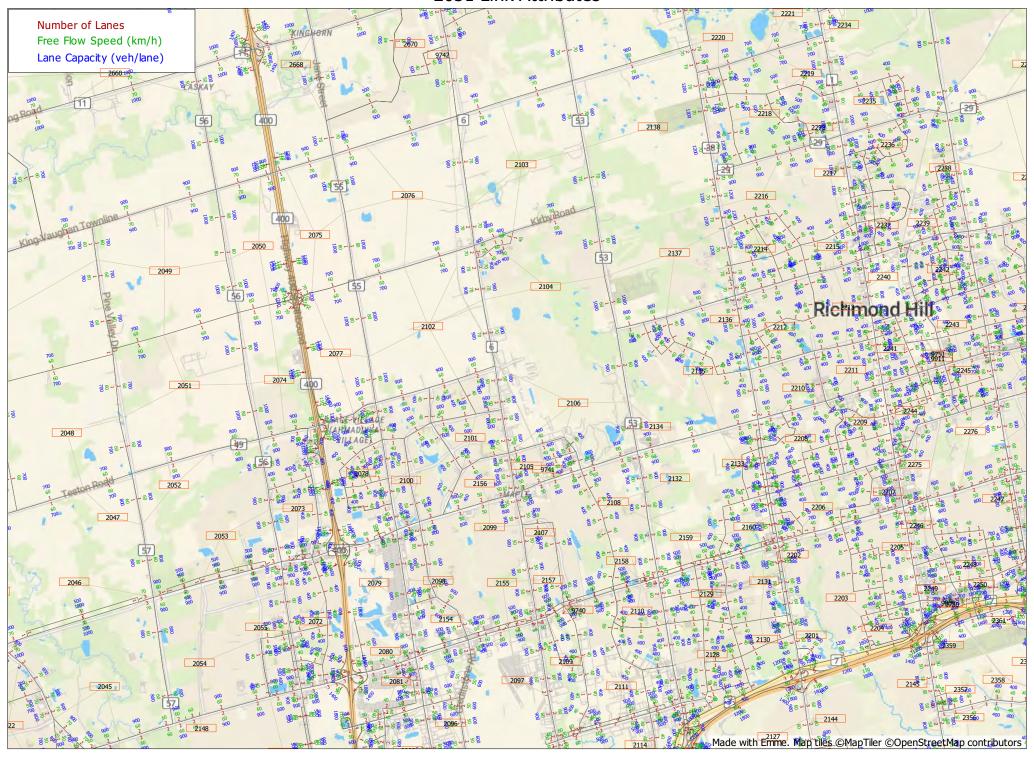


2016 Link Volume to Capacity Ratio

| Arterial Road | Travel Direction | Section | 2016 # of Lanes | 2016 Lane Capacity | Total Capacity | 2016 EMME Assigned Volumes | 2016 v/c |
|--------------------|--------------------|---|-----------------|--------------------|----------------|----------------------------|--------------|
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 648 | 0.36 |
| | F | Jane St to Keele St | 2 | 900 | 1,800 | 319 | 0.18 |
| | Eastbound | Keele St to Dufferin St | Missing link | Missing link | Missing link | Missing link | Missing link |
| | | Dufferin St to Bathurst St | 1 | 800 | 800 | 365 | 0.46 |
| Teston Road | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,513 | 0.84 |
| | | Jane St to Keele St | 2 | 900 | 1,800 | 1,175 | 0.65 |
| | Westbound | Keele St to Dufferin St | Missing link | Missing link | Missing link | Missing link | Missing link |
| | | Dufferin St to Bathurst St | 1 | 800 | 800 | 768 | 0.96 |
| | | Hwy 400 to Jane St | 1 | 700 | 700 | 65 | 0.09 |
| | | Jane St to Keele St | 1 | 700 | 700 | 97 | 0.14 |
| | Eastbound | Keele St to Dufferin St | 1 | 700 | 700 | 188 | 0.27 |
| W. b. D I | | Dufferin St to Bathurst St | Missing link | Missing link | Missing link | Missing link | Missing link |
| Kirby Road | | Hwy 400 to Jane St | 1 | 700 | 700 | 298 | 0.43 |
| | Mr. ale a sal | Jane St to Keele St | 1 | 700 | 700 | 504 | 0.72 |
| | Westbound | Keele St to Dufferin St | 1 | 700 | 700 | 619 | 0.88 |
| | | Dufferin St to Bathurst St | Missing link | Missing link | Missing link | Missing link | Missing link |
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,369 | 0.76 |
| | Eastbound | Jane St to Keele St | 2 | 800 | 1,600 | 1,073 | 0.67 |
| | Eastbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,065 | 0.59 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 906 | 0.50 |
| Major Mackenzie Dr | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,890 | 1.05 |
| | Markhau a | Jane St to Keele St | 2 | 800 | 1,600 | 1,362 | 0.85 |
| | Westbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,651 | 0.92 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,780 | 0.99 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 179 | 0.10 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 232 | 0.13 |
| | Northbound | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 176 | 0.18 |
| | | Kirby Rd to King Vaughan Rd | 1 | 1,000 | 1,000 | 197 | 0.20 |
| Jane Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2,046 | 1.14 |
| | Contract | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 939 | 0.52 |
| | Southbound | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 986 | 0.99 |
| | | Kirby Rd to King Vaughan Rd | 1 | 1,000 | 1,000 | 833 | 0.83 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 276 | 0.15 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 205 | 0.13 |
| | Northbound | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 160 | 0.08 |
| Vaala Chaash | | Kirby Rd to King Vaughan Rd | 2 | 1,000 | 2,000 | 161 | 0.08 |
| Keele Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 1,862 | 1.03 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 1,051 | 0.66 |
| | Southbound | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 1,548 | 0.77 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,000 | 2,000 | 1,530 | 0.77 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 730 | 0.41 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 1 | 900 | 900 | 333 | 0.37 |
| | Northbound | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 428 | 0.43 |
| D. Harin Charact | | Kirby Rd to King Vaughan Rd | 1 | 1,000 | 1,000 | 193 | 0.19 |
| Dufferin Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 1,523 | 0.85 |
| | Couthbour | Major Mackenzie Dr IC to Teston Rd IC | 1 | 900 | 900 | 1,018 | 1.13 |
| | Southbound | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 598 | 0.60 |
| | | Kirby Rd to King Vaughan Rd | 1 | 1,000 | 1,000 | 794 | 0.79 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 862 | 0.48 |
| | N a stable a con 1 | Major Mackenzie Dr IC to Teston Rd IC | 2 | 1,000 | 2,000 | 745 | 0.37 |
| | Northbound | Teston Rd to Kirby Rd | 2 | 1,200 | 2,400 | 790 | 0.33 |
| Dath Church | | Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 | 840 | 0.35 |
| Bathurst Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 1,942 | 1.08 |
| | 6. 111 | Major Mackenzie Dr IC to Teston Rd IC | 2 | 1,000 | 2,000 | 1,903 | 0.95 |
| | Southbound | Teston Rd to Kirby Rd | 2 | 1,200 | 2,400 | 1,931 | 0.80 |
| | | | | | | | |

Appendix G: 2031 Snapshot of EMME Subarea Network

2031 Link Attributes



YRTDF Model-2031_March-2020 (I:/EMME/Emme_4_Modelling_in_2020_MASTER/Database/Model-2031_March-2020/emmebank) Scenario 3007: 2031 MASTER Apr 15-2020 2020-06-04

2031 AM 3-hour Pkpd Transit Link Volumes



YRTDF Model-2031_March-2020 (I:/EMME/Emme_4_Modelling_in_2020_MASTER/Database/Model-2031_March-2020/emmebank) Scenario 3009: 2031 MASTER Jun29-2020 2020-08-24



2031 Link Volume to Capacity Ratio

| Arterial Road | Travel Direction | Section | 2031 # of Lanes | 2031 Lane Capacity | Total Capacity | 2031 EMME Counts | 2031 v/c |
|--------------------|------------------|---|-----------------|--------------------|----------------|------------------|--------------|
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,076 | 0.60 |
| | Eastbound | Jane St to Keele St | 2 | 900 | 1,800 | 918 | 0.51 |
| | Lastbourid | Keele St to Dufferin St | Missing link | Missing link | Missing link | Missing link | Missing link |
| Teston Road | | Dufferin St to Bathurst St | 1 | 800 | 800 | 503 | 0.63 |
| restorritoad | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,519 | 0.84 |
| | Westbound | Jane St to Keele St | 2 | 900 | 1,800 | 1,321 | 0.73 |
| | TTOOLDOUTIU | Keele St to Dufferin St | Missing link | Missing link | Missing link | Missing link | Missing link |
| | | Dufferin St to Bathurst St | 1 | 800 | 800 | 1,026 | 1.28 |
| | | Hwy 400 to Jane St | 1 | 700 | 700 | 385 | 0.55 |
| | Eastbound | Jane St to Keele St | 1 | 700 | 700 | 163 | 0.23 |
| | | Keele St to Dufferin St | 1 | 700 | 700 | 426 | 0.61 |
| Kirby Road | | Dufferin St to Bathurst St | Missing link | Missing link | Missing link | Missing link | Missing link |
| | | Hwy 400 to Jane St | 1 | 700 | 700 | 736 | 1.05 |
| | Westbound | Jane St to Keele St | 1 | 700 | 700 | 521 | 0.74 |
| | | Keele St to Dufferin St | 1 | 700 | 700 | 646 | 0.92 |
| | | Dufferin St to Bathurst St | Missing link | Missing link | Missing link | Missing link | Missing link |
| | | Hwy 400 to Jane St | 3 | 900 | 2,700 | 2,040 | 0.76 |
| | Eastbound | Jane St to Keele St | 2 | 800 | 1,600 | 1,178 | 0.74 |
| | | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,198 | 0.67 |
| Major Mackenzie Dr | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,197 | 0.67 |
| ., | | Hwy 400 to Jane St | 3 | 900 | 2,700 | 2,411 | 0.89 |
| | Westbound | Jane St to Keele St | 2 | 800 | 1,600 | 1,439 | 0.90 |
| | | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,801 | 1.00 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,699 | 0.94 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 269 | 0.15 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 240 | 0.13 |
| | | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 216 | 0.22 |
| Jane Street | | Kirby Rd to King Vaughan Rd | 1 | 1,000 | 1,000 | 399 | 0.40 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2342 | 1.30 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 1507 | 0.84 |
| | | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 912 | 0.91 |
| | | Kirby Rd to King Vaughan Rd | 1 | 1,000 | 1,000 | 1019 | 1.02 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 718 | 0.40 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 658 | 0.41 |
| | | Teston Rd to Kirby Rd | 2 | 900 | 1,800 | 514 | 0.29 |
| Keele Street | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 398 | 0.22 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2309 | 1.28 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 1510 | 0.94 |
| | | Teston Rd to Kirby Rd | 2 | 900 | 1,800 | 1710 | 0.95 |
| | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 1819 | 1.01 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 975 | 0.54 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 714 | 0.40 |
| | | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 627 | 0.63 |
| Dufferin Street | | Kirby Rd to King Vaughan Rd | 1 | 900 | 900 | 242 | 0.27 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 1899 | 1.06 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 1816 | 1.01 |
| | | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 1032 | 1.03 |
| | | Kirby Rd to King Vaughan Rd | 1 | 900 | 900 | 867 | 0.96 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 3 | 900 | 2,700 | 1129 | 0.42 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 1,000 | 2,000 | 915 | 0.46 |
| | | Teston Rd to Kirby Rd | 2 | 1,200 | 2,400 | 1063 | 0.44 |
| Bathurst Street | | Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 | 1187 | 0.49 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 3 | 900 | 2,700 | 2740 | 1.01 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 1,000 | 2,000 | 2142 | 1.07 |
| | | Teston Rd to Kirby Rd | 2 | 1,200 | 2,400 | 2422 | 1.01 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 | 2392 | 1.00 |

Appendix H: 2031 Snapshot of EMME Subarea Network with 2041 Demand



2041 Link Volume to Capacity Ratio with 2031 Road Improvements

| Arterial Road | Travel Direction | Section | 2031 # of Lanes | 2031 Lane Capacity | Total Capacity | 2031 EMME Counts | 2031 v/c |
|--------------------|---|--|-----------------|--------------------|----------------|------------------|--------------|
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,280 | 0.71 |
| | | Jane St to Keele St | 2 | 900 | 1,800 | 982 | 0.55 |
| | Eastbound | Keele St to Dufferin St | Missing link | Missing link | Missing link | Missing link | Missing link |
| Teston Road | | Dufferin St to Bathurst St | 1 | 800 | 800 | 678 | 0.85 |
| reston Road | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,735 | 0.96 |
| | Westbound | Jane St to Keele St | 2 | 900 | 1,800 | 1,381 | 0.77 |
| | Westbound | Keele St to Dufferin St | Missing link | Missing link | Missing link | Missing link | Missing link |
| | | Dufferin St to Bathurst St | 1 | 800 | 800 | 1,135 | 1.42 |
| | | Hwy 400 to Jane St | 1 | 700 | 700 | 529 | 0.76 |
| | Eastbound | Jane St to Keele St | 1 | 700 | 700 | 483 | 0.69 |
| | Lastbourid | Keele St to Dufferin St | 1 | 700 | 700 | 590 | 0.84 |
| Kirby Road | | Dufferin St to Bathurst St | Missing link | Missing link | Missing link | Missing link | Missing link |
| Kirby Nodu | | Hwy 400 to Jane St | 1 | 700 | 700 | 805 | 1.15 |
| | Westbound | Jane St to Keele St | 1 | 700 | 700 | 659 | 0.94 |
| | Westboaria | Keele St to Dufferin St | 1 | 700 | 700 | 773 | 1.10 |
| | | Dufferin St to Bathurst St | Missing link | Missing link | Missing link | Missing link | Missing link |
| | | Hwy 400 to Jane St | 3 | 900 | 2,700 | 2,294 | 0.85 |
| | Eastbound | Jane St to Keele St | 2 | 800 | 1,600 | 1,342 | 0.84 |
| | Lastocana | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,404 | 0.78 |
| Major Mackenzie Dr | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,366 | 0.76 |
| , | | Hwy 400 to Jane St | 3 | 900 | 2,700 | 2,597 | 0.96 |
| | Westbound | Jane St to Keele St | 2 | 800 | 1,600 | 1,590 | 0.99 |
| | *************************************** | Keele St to Dufferin St | 2 | 900 | 1,800 | 2,006 | 1.11 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,882 | 1.05 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 727 | 0.40 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 547 | 0.30 |
| | | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 551 | 0.55 |
| Jane Street | | Kirby Rd to King Vaughan Rd | 1 | 1,000 | 1,000 | 775 | 0.78 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2624 | 1.46 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 1994 | 1.11 |
| | | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 1362 | 1.36 |
| | | Kirby Rd to King Vaughan Rd | 1 | 1,000 | 1,000 | 1371 | 1.37 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 928 | 0.52 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 910 | 0.57 |
| | | Teston Rd to Kirby Rd | 2 | 900 | 1,800 | 939 | 0.52 |
| Keele Street | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 944 | 0.52 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2620 | 1.46 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 1948 | 1.22 |
| | | Teston Rd to Kirby Rd | 2 | 900 | 1,800 | 1993 | 1.11 |
| | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 2183 | 1.21 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 1109 | 0.62 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 1012 | 0.56 |
| | | Teston Rd to Kirby Rd | 1 | 1,000 | 1,000 | 827 | 0.83 |
| Dufferin Street | | Kirby Rd to King Vaughan Rd | 1 | 900 | 900 | 361 | 0.40 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2098 | 1.17 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 2150 | 1.19 |
| | | Teston Rd to Kirby Rd | 1 1 | 1,000 | 1,000 | 1293 1010 | 1.29 |
| | | Kirby Rd to King Vaughan Rd | | 900 | 900 | 1010 | 1.12 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC Major Mackenzie Dr IC to Teston Rd IC | 3 2 | 900 | 2,700 | 995 | 0.48 0.50 |
| | Northbound | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 2,400 | 1319 | 0.50 |
| | | Kirby Rd to Kirby Kd Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 | 1519 | 0.55 |
| Bathurst Street | | Rutherford Rd IC to Major Mackenzie Dr IC | | 1,200 900 | 2,400 | 3031 | 1.12 |
| | | · · · · · · · · · · · · · · · · · · · | 3 | | | | |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 1,000 | 2,000 | 2451 | 1.23 |
| | Teston Rd to Kirby Rd | | 2 2 | 1,200 | 2,400 | 2905 2881 | 1.21 1.20 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 | 2881 | 1.20 |

Appendix I: 2041 Snapshot of EMME Subarea Network <u>without</u> GTA West

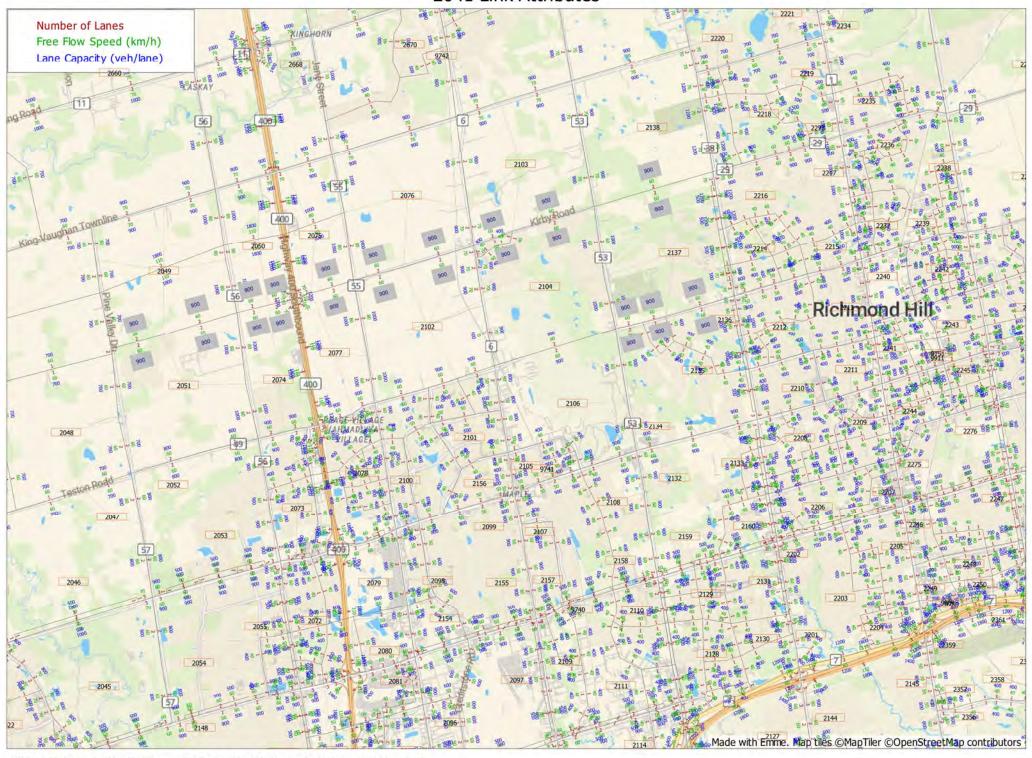


2041 Link Volume to Capacity Ratio without GTA West Corridor

| Arterial Road | Travel Direction | Section | 2041# of Lanes | 2041 Lane Capacity | Total Capacity | 2041 EMME Assigned Volumes | 2041 v/c |
|--------------------|------------------|--|----------------|--------------------|----------------|----------------------------|--------------|
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,131 | 0.63 |
| | Eastbound | Jane St to Keele St | 2 | 900 | 1,800 | 1,376 | 0.76 |
| | Lastbourid | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,171 | 0.65 |
| Teston Road | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,326 | 0.74 |
| rooton rtoda | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,632 | 0.91 |
| | | Jane St to Keele St | 2 | 900 | 1,800 | 1,500 | 0.83 |
| | Westbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,518 | 0.84 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,555 | 0.86 |
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,243 | 0.69 |
| | | Jane St to Keele St | 2 | 900 | 1,800 | 852 | 0.47 |
| | Eastbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,262 | 0.70 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,196 | 0.66 |
| Kirby Road | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,535 | 0.85 |
| | Westbound | Jane St to Keele St | 2 | 900 | 1,800 | 1,237 | 0.69 |
| | westbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,411 | 0.78 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,369 | 0.76 |
| | | Hwy 400 to Jane St | 3 | 900 | 2,700 | 1,579 | 0.58 |
| | | Jane St to Keele St | 2 | 800 | 1,600 | 1,074 | 0.67 |
| | Eastbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 874 | 0.49 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,127 | 0.63 |
| Major Mackenzie Dr | | Hwy 400 to Jane St | 3 | 900 | 2,700 | 1,943 | 0.72 |
| | | Jane St to Keele St | 2 | 800 | 1,600 | 1,385 | 0.72 |
| | Westbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,628 | 0.90 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,610 | 0.89 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 405 | 0.03 |
| | | • | 2 | 900 | 1,800 | | 0.23 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | | 2.000 | 575 | 0.32 |
| | | Teston Rd to Kirby Rd | 2 | 1,000 1,000 | 2,000 | 470 1161 | 0.24 |
| Jane Street | | Kirby Rd to King Vaughan Rd Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2527 | 1.40 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 2376 | 1.32 |
| | Southbound | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 1988 | 0.99 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,000 | 2,000 | 2086 | 1.04 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 408 | 0.23 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 407 | 0.25 |
| | Northbound | Teston Rd to Kirby Rd | 2 | 900 | 1,800 | 723 | 0.40 |
| | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 722 | 0.40 |
| Keele Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2573 | 1.43 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 1806 | 1.13 |
| | Southbound | Teston Rd to Kirby Rd | 2 | 900 | 1,800 | 1798 | 1.00 |
| | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 2077 | 1.15 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 1045 | 0.58 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 814 | 0.45 |
| | Northboand | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 485 | 0.24 |
| Dufferin Street | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 328 | 0.18 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2078 | 1.15 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 2183 | 1.21 |
| | | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 1792 | 0.90 |
| | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 1611 | 0.90 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 3 | 900 | 2,700 | 1380 | 0.51 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 3 | 1,000 | 3,000 | 1390 | 0.46 |
| | | Teston Rd to Kirby Rd | 3 | 1,200 | 3,600 | 1570 | 0.44 |
| Bathurst Street | | Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 2,700 | 1093 2940 | 0.46 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC Major Mackenzie Dr IC to Teston Rd IC | 3 | 900 1,000 | 3,000 | 2940 2747 | 1.09 0.92 |
| | Southbound | Teston Rd to Kirby Rd | 3 | 1,200 | 3,000 | 2747 | 0.92 |
| | | | | | | | |

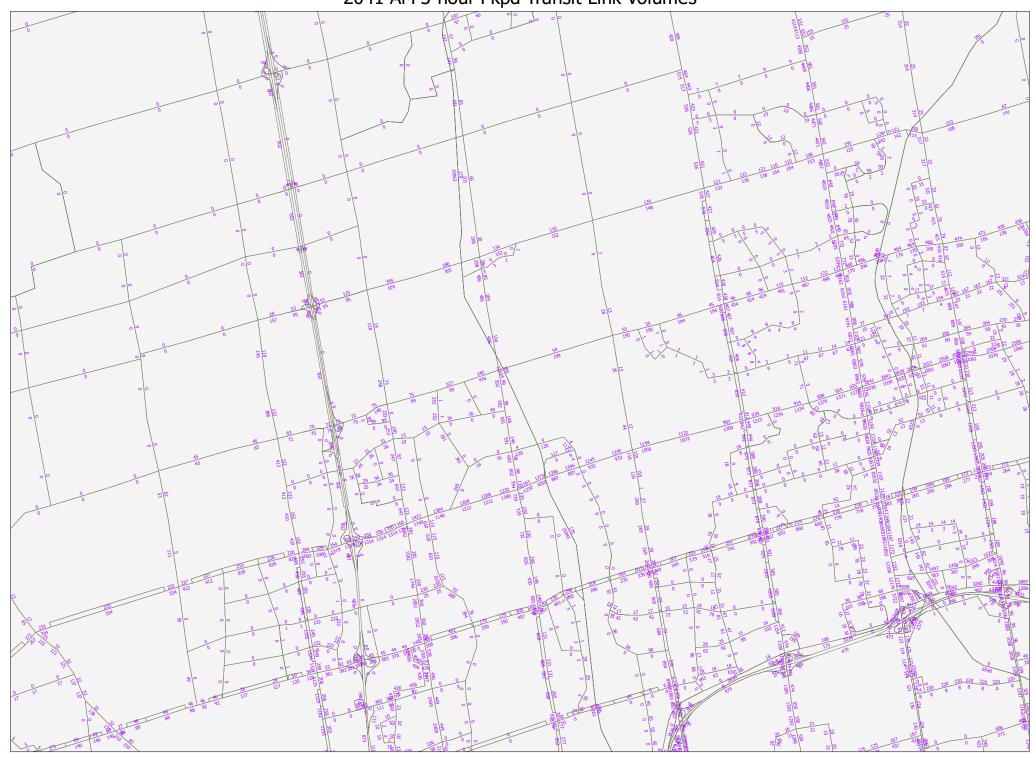
Appendix J: 2041 Snapshot of EMME Subarea Network <u>with</u> GTA West

2041 Link Attributes



YRTDF Model-2041_March-2020 (I:/EMME/Emme_4_Modelling_in_2020_MASTER/Database/Model-2041_March-2020/emmebank) Scenario 9422: 2041 MASTER Apr15-2020 2020-06-04

2041 AM 3-hour Pkpd Transit Link Volumes



YRTDF Model-2041_March-2020 (I:/EMME/Emme_4_Modelling_in_2020_MASTER/Database/Model-2041_March-2020/emmebank) Scenario 9424: 2041 MASTER Jun29-2020 2020-08-24

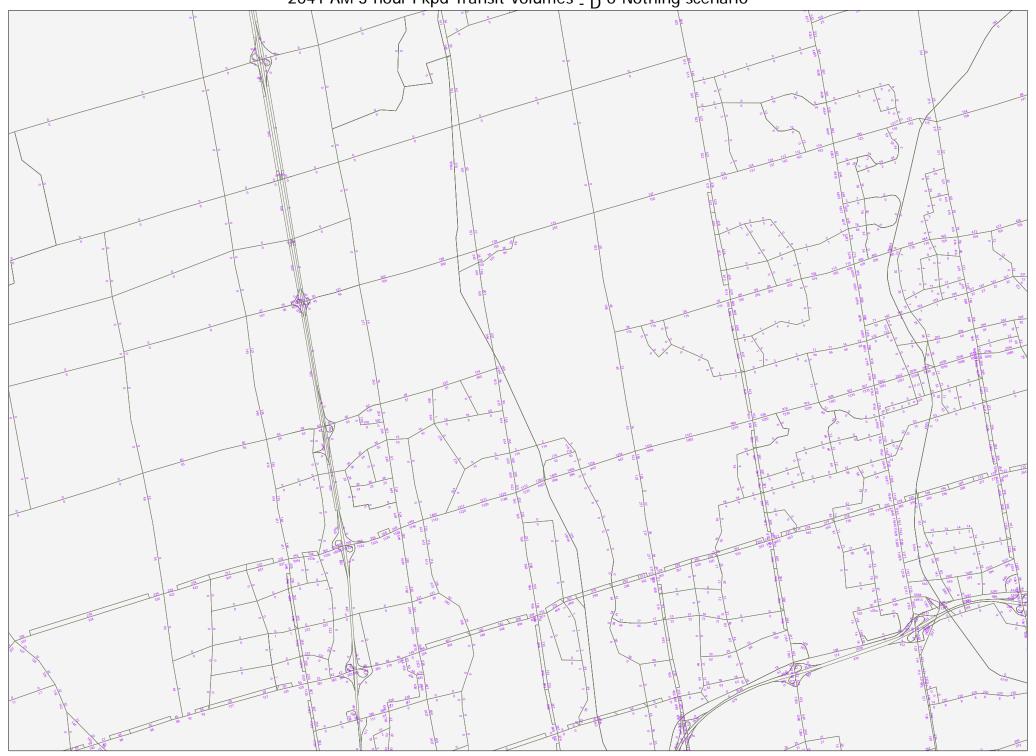


2041 Link Volume to Capacity Ratio with GTA West Corridor

| Arterial Road | Travel Direction | Section | 2041# of Lanes | 2041 Lane Capacity | Total Capacity | 2041 EMME Assigned Volumes | 2041 v/c |
|--------------------|------------------|---|----------------|--------------------|----------------|----------------------------|--------------|
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,160 | 0.64 |
| | Eastbound | Jane St to Keele St | 2 | 900 | 1,800 | 1,340 | 0.74 |
| | Lastbourid | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,142 | 0.63 |
| Teston Road | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,320 | 0.73 |
| 1 CStOII 1 Codd | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,480 | 0.82 |
| | | Jane St to Keele St | 2 | 900 | 1,800 | 1,522 | 0.85 |
| | Westbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,637 | 0.909 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,611 | 0.90 |
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 618 | 0.34 |
| | | Jane St to Keele St | 2 | 900 | 1,800 | 839 | 0.47 |
| | Eastbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,270 | 0.71 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,184 | 0.66 |
| Kirby Road | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,235 | 0.69 |
| | | Jane St to Keele St | 2 | 900 | 1,800 | 1,503 | 0.84 |
| | Westbound | | | | | · · | |
| | | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,585 | 0.88 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,518 | 0.84 |
| | | Hwy 400 to Jane St | 3 | 900 | 2,700 | 1,552 | 0.57 |
| | Eastbound | Jane St to Keele St | 2 | 800 | 1,600 | 1,093 | 0.68 |
| | | Keele St to Dufferin St | 2 | 900 | 1,800 | 879 | 0.49 |
| Major Mackenzie Dr | | Dufferin St to Bathurst St | 3 | 900 900 | 1,800 | 1,164 1,826 | 0.65 |
| ., | | Hwy 400 to Jane St Jane St to Keele St | 2 | 800 | 2,700 1,600 | 1,826 | 0.68 |
| | Westbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,568 | 0.83 |
| | | | 2 | 900 | | , | _ |
| | | Dufferin St to Bathurst St | _ | | 1,800 | 1,616 | 0.90 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 391 | 0.22 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 377 | 0.21 |
| | | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 503 | 0.25 |
| Jane Street | | Kirby Rd to King Vaughan Rd | 2 | 1,000 | 2,000 | 648 | 0.32 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2487 | 1.38 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 2224 | 1.24 |
| | | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 1805 | 0.90 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,000 | 2,000 | 1959 | 0.98 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 439 | 0.24 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 391 | 0.24 |
| | | Teston Rd to Kirby Rd | 2 | 900 | 1,800 | 805 | 0.45 |
| Keele Street | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 685 | 0.38 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2504 | 1.39 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 2 | 800 | 1,600 | 1675 | 1.05 |
| | | Teston Rd to Kirby Rd | | 900 | 1,800 | 1723 | 0.96 |
| | | Kirby Rd to King Vaughan Rd Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 900 | 1,800 1,800 | 2049 1002 | 1.14 0.56 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 780 | 0.36 |
| | Northbound | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 369 | 0.43 |
| | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 246 | 0.16 |
| Dufferin Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 1998 | 1.11 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 2132 | 1.11 |
| | Southbound | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 1747 | 0.87 |
| | | Kirby Rd to Kirby Kd Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 1606 | 0.89 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 3 | 900 | 2,700 | 1327 | 0.49 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 3 | 1,000 | 3,000 | 1397 | 0.47 |
| | Northbound | Teston Rd to Kirby Rd | 3 | 1,200 | 3,600 | 1599 | 0.44 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 | 1127 | 0.44 |
| Bathurst Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 3 | 900 | 2,700 | 2871 | 1.06 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 3 | 1,000 | 3,000 | 2698 | 0.90 |
| | Southbound | Teston Rd to Kirby Rd | 3 | 1,200 | 3,600 | 2840 | 0.79 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 | 2329 | 0.73 |

Appendix K: 2041 Snapshot of EMME Subarea Network for Do-Nothing Option

2041 AM 3-hour Pkpd Transit Volumes $_{\text{- }D}$ o-Nothing scenario





2041 Link Volume to Capacity Ratio with GTA West Corridor for Do-Nothing Option

| Arterial Road | Travel Direction | Section | 2041# of Lanes | 2041 Lane Capacity | Total Capacity | 2041 EMME Assigned Volumes | 2041 v/c |
|--------------------|------------------|---|----------------|--------------------|----------------|----------------------------|----------|
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 923 | 0.51 |
| | Eastbound | Jane St to Keele St | 2 | 900 | 1,800 | 861 | 0.48 |
| | Lustbourid | Keele St to Dufferin St | 2 | 900 | 1,800 | Missing Link | |
| Teston Road | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,035 | 0.58 |
| rooton roud | | Hwy 400 to Jane St | 2 | 900 | 1.800 | 1,370 | 0.76 |
| | | Jane St to Keele St | 2 | 900 | 1,800 | 1,217 | 0.68 |
| | Westbound | Keele St to Dufferin St | 2 | 900 | 1,800 | Missing Link | |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,406 | 0.78 |
| | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 762 | 0.42 |
| | F | Jane St to Keele St | 2 | 900 | 1,800 | 896 | 0.50 |
| | Eastbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,694 | 0.94 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,345 | 0.75 |
| Kirby Road | | Hwy 400 to Jane St | 2 | 900 | 1,800 | 1,353 | 0.75 |
| | | Jane St to Keele St | 2 | 900 | 1,800 | 1,497 | 0.83 |
| | Westbound | Keele St to Dufferin St | 2 | 900 | 1.800 | 2,114 | 1.17 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,489 | 0.83 |
| | | Hwy 400 to Jane St | 3 | 900 | 2,700 | 1,560 | 0.58 |
| | | Jane St to Keele St | 2 | 800 | 1,600 | 1,282 | 0.80 |
| | Eastbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 1,284 | 0.71 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,169 | 0.65 |
| Major Mackenzie Dr | | Hwy 400 to Jane St | 3 | 900 | 2,700 | 1,773 | 0.66 |
| | | Jane St to Keele St | 2 | 800 | 1,600 | 1,439 | 0.90 |
| | Westbound | Keele St to Dufferin St | 2 | 900 | 1,800 | 2,039 | 1.13 |
| | | Dufferin St to Bathurst St | 2 | 900 | 1,800 | 1,823 | 1.01 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 357 | 0.20 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 299 | 0.17 |
| | Northbound | Teston Rd to Kirby Rd | 2 | 1,000 | 2.000 | 550 | 0.28 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,000 | 2,000 | 644 | 0.32 |
| Jane Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2479 | 1.38 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 2112 | 1.17 |
| | Southbound | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 1901 | 0.95 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,000 | 2,000 | 1995 | 1.00 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 460 | 0.26 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 836 | 0.52 |
| | Northbound | Teston Rd to Kirby Rd | 2 | 900 | 1,800 | 672 | 0.37 |
| Keele Street | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 696 | 0.39 |
| Reele Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2499 | 1.39 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 800 | 1,600 | 1728 | 1.08 |
| | SouthBound | Teston Rd to Kirby Rd | 2 | 900 | 1,800 | 1748 | 0.97 |
| | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 2081 | 1.16 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 1005 | 0.56 |
| | Northbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 819 | 0.46 |
| | | Teston Rd to Kirby Rd | 2 | 1,000 | 2,000 | 1159 | 0.58 |
| Dufferin Street | | Kirby Rd to King Vaughan Rd | 2 | 900 | 1,800 | 477 | 0.27 |
| | | Rutherford Rd IC to Major Mackenzie Dr IC | 2 | 900 | 1,800 | 2025 | 1.13 |
| | Southbound | Major Mackenzie Dr IC to Teston Rd IC | 2 | 900 | 1,800 | 2139 | 1.19 |
| | | Teston Rd to Kirby Rd | 2 | 1,000 900 | 2,000 1,800 | 1914 1509 | 0.96 |
| | | Kirby Rd to King Vaughan Rd Rutherford Rd IC to Major Mackenzie Dr IC | 3 | 900 | 2,700 | 1509 | 0.84 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 3 | 1,000 | 3,000 | 1206 | 0.40 |
| | Northbound | Teston Rd to Kirby Rd | 3 | 1,200 | 3,600 | 1460 | 0.40 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 | 1036 | 0.43 |
| Bathurst Street | | Rutherford Rd IC to Major Mackenzie Dr IC | 3 | 900 | 2,700 | 2859 | 1.06 |
| | | Major Mackenzie Dr IC to Teston Rd IC | 3 | 1,000 | 3,000 | 2657 | 0.89 |
| | Southbound | Teston Rd to Kirby Rd | 3 | 1,200 | 3,600 | 2942 | 0.82 |
| | | Kirby Rd to King Vaughan Rd | 2 | 1,200 | 2,400 | 2293 | 0.96 |

Appendix L: Synchro Results for Do-Nothing Conditions (2041)

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|-----------------------------------|-------|----------|--------|-------|--------------|------------|---------|----------|-------|------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | × | ^ | 7 | * | 1 | | 44 | | 7 | | 4 | |
| Traffic Volume (vph) | 0 | 880 | 528 | 944 | 854 | 4 | 30 | 0 | 183 | 0 | 3 | 1 |
| Future Volume (vph) | 0 | 880 | 528 | 944 | 854 | 4 | 30 | 0 | 183 | 0 | 3 | 1 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | 1.0 | 5.0 | | 5.0 | | 5.0 | | 1.0 | |
| Lane Util. Factor | | 0.95 | 1.00 | 1.00 | 0.95 | | 0.97 | | 1.00 | | 1.00 | |
| Frpb, ped/bikes | | 1.00 | 0.99 | 1.00 | 1.00 | | 1.00 | | 1.00 | | 1.00 | |
| Flpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | | 1.00 | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | | 0.85 | | 0.97 | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | | 1.00 | |
| Satd. Flow (prot) | | 3318 | 1464 | 1630 | 3258 | | 2603 | | 1420 | | 1856 | |
| FIt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | | 1.00 | |
| Satd. Flow (perm) | | 3318 | 1464 | 1630 | 3258 | | 2603 | | 1420 | | 1856 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 0 | 907 | 544 | 944 | 880 | 4 | 31 | 0 | 189 | 0 | 3 | 1 |
| RTOR Reduction (vph) | 0 | 0 | 328 | 0 | 0 | 0 | 0 | 0 | 171 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 0 | 907 | 216 | 944 | 884 | 0 | 31 | 0 | 18 | 0 | 3 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | | | | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Heavy Vehicles (%) | 0% | 10% | 10% | 12% | 12% | 0% | 36% | 0% | 15% | 0% | 0% | 0% |
| | Perm | NA | Perm | Prot | NA | | Prot | | Perm | | NA | |
| Protected Phases | | 6 | . 0 | 5 | 2 | | 8 | | . 0 | | 7 | |
| Permitted Phases | 6 | | 6 | | - | | | | 8 | 7 | • | |
| Actuated Green, G (s) | | 33.1 | 33.1 | 56.2 | 93.3 | | 10.8 | | 10.8 | • | 1.3 | |
| Effective Green, g (s) | | 35.1 | 35.1 | 59.2 | 95.3 | | 11.8 | | 11.8 | | 5.3 | |
| Actuated g/C Ratio | | 0.28 | 0.28 | 0.48 | 0.77 | | 0.10 | | 0.10 | | 0.04 | |
| Clearance Time (s) | | 7.0 | 7.0 | 4.0 | 7.0 | | 6.0 | | 6.0 | | 5.0 | |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 943 | 416 | 781 | 2516 | | 248 | | 135 | | 79 | |
| v/s Ratio Prot | | c0.27 | 710 | c0.58 | 0.27 | | 0.01 | | 100 | | c0.00 | |
| v/s Ratio Perm | | 00.21 | 0.15 | 00.00 | 0.21 | | 0.01 | | c0.01 | | 00.00 | |
| v/c Ratio | | 0.96 | 0.52 | 1.21 | 0.35 | | 0.12 | | 0.13 | | 0.04 | |
| Uniform Delay, d1 | | 43.5 | 37.1 | 32.1 | 4.4 | | 51.1 | | 51.1 | | 56.6 | |
| Progression Factor | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 21.4 | 4.6 | 105.8 | 0.4 | | 0.2 | | 0.5 | | 0.2 | |
| Delay (s) | | 64.9 | 41.7 | 137.9 | 4.8 | | 51.3 | | 51.6 | | 56.8 | |
| Level of Service | | E | D | F | A | | D | | D | | E | |
| Approach Delay (s) | | 56.2 | | • | 73.5 | | | 51.5 | | | 56.8 | |
| Approach LOS | | E | | | E | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 64.9 | H | CM 2000 | Level of S | Service | | Е | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.94 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 123.4 | Sı | um of lost | time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | | | 101.8% | | | of Service | | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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| | - | * | 1 | ← | 1 | - | | |
|-----------------------------------|------------|------|-------|----------|------------|------------------|---|--|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | | |
| Lane Configurations | † † | 7 | | ^ | 774 | 7 | | |
| Traffic Volume (vph) | 402 | 130 | 0 | 1467 | 262 | 1158 | | |
| Future Volume (vph) | 402 | 130 | 0 | 1467 | 262 | 1158 | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | |
| Total Lost time (s) | 5.0 | 4.0 | | 5.0 | 5.0 | 5.0 | | |
| Lane Util. Factor | 0.95 | 1.00 | | 0.95 | 0.97 | 0.91 | | |
| Frt | 1.00 | 0.85 | | 1.00 | 0.90 | 0.85 | | |
| Flt Protected | 1.00 | 1.00 | | 1.00 | 0.98 | 1.00 | | |
| Satd. Flow (prot) | 3411 | 1526 | | 3411 | 3075 | 1389 | | |
| Flt Permitted | 1.00 | 1.00 | | 1.00 | 0.98 | 1.00 | | |
| Satd. Flow (perm) | 3411 | 1526 | | 3411 | 3075 | 1389 | | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | | |
| Adj. Flow (vph) | 414 | 134 | 0 | 1512 | 270 | 1194 | | |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 277 | 277 | | |
| Lane Group Flow (vph) | 414 | 134 | 0 | 1512 | 590 | 320 | | |
| Heavy Vehicles (%) | 7% | 7% | 0% | 7% | 7% | 7% | | |
| Turn Type | NA | Free | | NA | Prot | Perm | | |
| Protected Phases | 2 | | | 6 | 8 | | | |
| Permitted Phases | | Free | | | | 8 | | |
| Actuated Green, G (s) | 47.3 | 86.4 | | 47.3 | 24.1 | 24.1 | | |
| Effective Green, g (s) | 49.8 | 86.4 | | 49.8 | 26.6 | 26.6 | | |
| Actuated g/C Ratio | 0.58 | 1.00 | | 0.58 | 0.31 | 0.31 | | |
| Clearance Time (s) | 7.5 | | | 7.5 | 7.5 | 7.5 | | |
| Vehicle Extension (s) | 4.0 | | | 4.0 | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 1966 | 1526 | | 1966 | 946 | 427 | | |
| v/s Ratio Prot | 0.12 | | | c0.44 | 0.19 | | | |
| v/s Ratio Perm | | 0.09 | | | | c0.23 | | |
| v/c Ratio | 0.21 | 0.09 | | 0.77 | 0.62 | 0.75 | | |
| Uniform Delay, d1 | 8.8 | 0.0 | | 13.9 | 25.6 | 26.9 | | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 0.2 | 0.1 | | 3.0 | 1.3 | 7.1 | | |
| Delay (s) | 9.1 | 0.1 | | 16.9 | 26.9 | 34.0 | | |
| Level of Service | Α | Α | | В | С | С | | |
| Approach Delay (s) | 6.9 | | | 16.9 | 29.8 | | | |
| Approach LOS | Α | | | В | С | | | |
| Intersection Summary | | | | | | | | |
| HCM 2000 Control Delay | | | 20.7 | HO | CM 2000 | Level of Service | e | |
| HCM 2000 Volume to Capaci | ity ratio | | 0.76 | | | | | |
| Actuated Cycle Length (s) | | | 86.4 | Sı | ım of lost | time (s) | | |
| Intersection Capacity Utilization | on | | 72.8% | IC | U Level c | of Service | | |
| Analysis Period (min) | | | 15 | | | | | |
| c Critical Lane Group | | | | | | | | |

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| | ٠ | → | * | • | ← | • | 1 | 1 | ~ | - | ↓ | 4 |
|-------------------------------|------------|----------|--------|-------|-----------|------------|---------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | * | ^ | 7 | * | ^ | 7 | * | ^ | 7 |
| Traffic Volume (vph) | 84 | 629 | 210 | 321 | 1266 | 14 | 147 | 78 | 74 | 220 | 1430 | 671 |
| Future Volume (vph) | 84 | 629 | 210 | 321 | 1266 | 14 | 147 | 78 | 74 | 220 | 1430 | 671 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1772 | 3544 | 1547 | 1807 | 3510 | 1126 | 1825 | 3288 | 1555 | 1772 | 3614 | 1597 |
| Flt Permitted | 0.10 | 1.00 | 1.00 | 0.21 | 1.00 | 1.00 | 0.07 | 1.00 | 1.00 | 0.70 | 1.00 | 1.00 |
| Satd. Flow (perm) | 182 | 3544 | 1547 | 399 | 3510 | 1126 | 125 | 3288 | 1555 | 1310 | 3614 | 1597 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 87 | 648 | 216 | 331 | 1266 | 14 | 152 | 80 | 76 | 227 | 1474 | 692 |
| RTOR Reduction (vph) | 0 | 0 | 94 | 0 | 0 | 9 | 0 | 0 | 39 | 0 | 0 | 89 |
| Lane Group Flow (vph) | 87 | 648 | 122 | 331 | 1266 | 5 | 152 | 80 | 37 | 227 | 1474 | 603 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | | | | | | |
| Confl. Bikes (#/hr) | | | | | | | | | | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 4% | 1% | 4% | 45% | 0% | 11% | 5% | 3% | 1% | 1% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | 1 | 6 | | | 2 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 6 | | 6 | 2 | | 2 |
| Actuated Green, G (s) | 44.9 | 37.9 | 37.9 | 60.5 | 49.5 | 49.5 | 68.5 | 68.5 | 68.5 | 57.5 | 57.5 | 57.5 |
| Effective Green, g (s) | 50.9 | 41.4 | 41.4 | 63.5 | 53.0 | 53.0 | 71.5 | 71.0 | 71.0 | 60.0 | 60.0 | 60.0 |
| Actuated g/C Ratio | 0.35 | 0.29 | 0.29 | 0.44 | 0.37 | 0.37 | 0.49 | 0.49 | 0.49 | 0.41 | 0.41 | 0.41 |
| Clearance Time (s) | 4.0 | 8.5 | 8.5 | 4.0 | 8.5 | 8.5 | 4.0 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 173 | 1011 | 441 | 384 | 1282 | 411 | 178 | 1609 | 761 | 542 | 1495 | 660 |
| v/s Ratio Prot | 0.03 | 0.18 | | c0.13 | c0.36 | | c0.06 | 0.02 | | | c0.41 | |
| v/s Ratio Perm | 0.14 | | 0.08 | 0.25 | | 0.00 | 0.36 | | 0.02 | 0.17 | | 0.38 |
| v/c Ratio | 0.50 | 0.64 | 0.28 | 0.86 | 0.99 | 0.01 | 0.85 | 0.05 | 0.05 | 0.42 | 0.99 | 0.91 |
| Uniform Delay, d1 | 37.0 | 45.3 | 40.2 | 30.5 | 45.7 | 29.3 | 38.8 | 19.4 | 19.3 | 30.1 | 42.1 | 40.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.3 | 1.4 | 0.3 | 17.7 | 21.9 | 0.0 | 30.6 | 0.1 | 0.1 | 2.4 | 20.2 | 19.3 |
| Delay (s) | 39.3 | 46.7 | 40.5 | 48.2 | 67.6 | 29.3 | 69.4 | 19.4 | 19.5 | 32.5 | 62.2 | 59.3 |
| Level of Service | D | D | D | D | Е | С | Ε | В | В | С | Е | Е |
| Approach Delay (s) | | 44.6 | | | 63.3 | | | 44.1 | | | 58.6 | |
| Approach LOS | | D | | | Е | | | D | | | Е | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 56.6 | Н | ICM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.95 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 145.0 | | um of los | | | | 12.0 | | | |
| Intersection Capacity Utiliza | ation | | 115.0% | IC | CU Level | of Service | 9 | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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| | - | * | 1 | • | 1 | ~ | | |
|--------------------------------|-----------|------|-------|----------|------------|------------------|----|--|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | | |
| Lane Configurations | ^ | 7 | * | ^ | * | 7 | | |
| Traffic Volume (vph) | 594 | 56 | 63 | 1576 | 138 | 55 | | |
| Future Volume (vph) | 594 | 56 | 63 | 1576 | 138 | 55 | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | |
| Total Lost time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | |
| Frt | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 | | |
| Flt Protected | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 3444 | 1541 | 1772 | 3510 | 1807 | 1526 | | |
| Flt Permitted | 1.00 | 1.00 | 0.42 | 1.00 | 0.95 | 1.00 | | |
| Satd. Flow (perm) | 3444 | 1541 | 779 | 3510 | 1807 | 1526 | | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | | |
| Adj. Flow (vph) | 612 | 58 | 65 | 1625 | 142 | 57 | | |
| RTOR Reduction (vph) | 0 | 15 | 0 | 0 | 0 | 48 | | |
| Lane Group Flow (vph) | 612 | 43 | 65 | 1625 | 142 | 9 | | |
| Heavy Vehicles (%) | 6% | 6% | 3% | 4% | 1% | 7% | | |
| Turn Type | NA | Perm | Perm | NA | Prot | Perm | | |
| Protected Phases | 6 | | | 2 | 8 | | | |
| Permitted Phases | | 6 | 2 | | | 8 | | |
| Actuated Green, G (s) | 66.0 | 66.0 | 66.0 | 66.0 | 12.8 | 12.8 | | |
| Effective Green, g (s) | 68.5 | 68.5 | 68.5 | 68.5 | 14.8 | 14.8 | | |
| Actuated g/C Ratio | 0.73 | 0.73 | 0.73 | 0.73 | 0.16 | 0.16 | | |
| Clearance Time (s) | 7.5 | 7.5 | 7.5 | 7.5 | 7.0 | 7.0 | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 2528 | 1131 | 571 | 2577 | 286 | 242 | | |
| v/s Ratio Prot | 0.18 | | | c0.46 | c0.08 | | | |
| v/s Ratio Perm | | 0.03 | 0.08 | | | 0.01 | | |
| v/c Ratio | 0.24 | 0.04 | 0.11 | 0.63 | 0.50 | 0.04 | | |
| Uniform Delay, d1 | 4.0 | 3.4 | 3.6 | 6.1 | 35.8 | 33.2 | | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 0.2 | 0.1 | 0.4 | 1.2 | 1.4 | 0.1 | | |
| Delay (s) | 4.2 | 3.5 | 4.0 | 7.3 | 37.2 | 33.3 | | |
| Level of Service | Α | Α | Α | Α | D | С | | |
| Approach Delay (s) | 4.2 | | | 7.2 | 36.1 | | | |
| Approach LOS | Α | | | Α | D | | | |
| Intersection Summary | | | | | | | | |
| HCM 2000 Control Delay | | | 8.6 | H | CM 2000 | Level of Service | ce | |
| HCM 2000 Volume to Capac | ity ratio | | 0.61 | | | | | |
| Actuated Cycle Length (s) | | | 93.3 | Sı | um of lost | time (s) | | |
| Intersection Capacity Utilizat | ion | | 69.0% | IC | U Level o | of Service | | |
| Analysis Period (min) | | | 15 | | | | | |
| c Critical Lane Group | | | | | | | | |

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|-------------------------------|------------|----------|-------|-------|------------|------------|---------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ↑ | 7 | 7 | 7 | | * | 1 | | 7 | ^ | 7 |
| Traffic Volume (vph) | 238 | 107 | 517 | 47 | 34 | 5 | 318 | 401 | 118 | 35 | 1154 | 782 |
| Future Volume (vph) | 238 | 107 | 517 | 47 | 34 | 5 | 318 | 401 | 118 | 35 | 1154 | 782 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | | 1.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1738 | 1731 | 1533 | 1207 | 1560 | | 1601 | 3050 | | 1765 | 3544 | 1601 |
| Flt Permitted | 0.71 | 1.00 | 1.00 | 0.69 | 1.00 | | 0.10 | 1.00 | | 0.45 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1298 | 1731 | 1533 | 872 | 1560 | | 169 | 3050 | | 842 | 3544 | 1601 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 245 | 110 | 533 | 48 | 35 | 5 | 318 | 413 | 122 | 36 | 1190 | 806 |
| RTOR Reduction (vph) | 0 | 0 | 276 | 0 | 4 | 0 | 0 | 25 | 0 | 0 | 0 | 478 |
| Lane Group Flow (vph) | 245 | 110 | 257 | 48 | 36 | 0 | 318 | 510 | 0 | 36 | 1190 | 328 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | | | 4 | 4 | | |
| Heavy Vehicles (%) | 5% | 11% | 5% | 51% | 21% | 20% | 14% | 8% | 38% | 3% | 3% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | | pm+pt | NA | | Perm | NA | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | 1 | 6 | | | 2 | |
| Permitted Phases | 4 | | 4 | 8 | | | 6 | | | 2 | | 2 |
| Actuated Green, G (s) | 39.1 | 31.5 | 31.5 | 35.7 | 29.8 | | 54.4 | 54.4 | | 35.8 | 35.8 | 35.8 |
| Effective Green, g (s) | 44.4 | 34.0 | 34.0 | 41.7 | 32.3 | | 57.4 | 56.9 | | 38.3 | 38.3 | 38.3 |
| Actuated g/C Ratio | 0.40 | 0.31 | 0.31 | 0.38 | 0.29 | | 0.52 | 0.51 | | 0.35 | 0.35 | 0.35 |
| Clearance Time (s) | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | | 4.0 | 7.5 | | 7.5 | 7.5 | 7.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 562 | 531 | 470 | 355 | 454 | | 315 | 1566 | | 291 | 1225 | 553 |
| v/s Ratio Prot | c0.04 | 0.06 | | 0.01 | 0.02 | | c0.16 | 0.17 | | | c0.34 | |
| v/s Ratio Perm | 0.13 | | c0.17 | 0.04 | | | 0.36 | | | 0.04 | | 0.21 |
| v/c Ratio | 0.44 | 0.21 | 0.55 | 0.14 | 0.08 | | 1.01 | 0.33 | | 0.12 | 0.97 | 0.59 |
| Uniform Delay, d1 | 23.2 | 28.4 | 32.0 | 22.4 | 28.5 | | 34.1 | 15.7 | | 24.8 | 35.7 | 29.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.5 | 0.9 | 4.5 | 0.2 | 0.3 | | 53.1 | 0.6 | | 0.9 | 19.7 | 4.6 |
| Delay (s) | 23.7 | 29.3 | 36.5 | 22.6 | 28.8 | | 87.2 | 16.3 | | 25.7 | 55.4 | 34.5 |
| Level of Service | С | C | D | С | С | | F | В | | С | Е | С |
| Approach Delay (s) | | 32.1 | | | 25.4 | | | 42.7 | | | 46.6 | |
| Approach LOS | | С | | | С | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 41.9 | H | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.77 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.8 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliza | ation | | 86.7% | IC | U Level c | of Service |) | | Е | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|------------------------------|-------------|----------|--------|-------|------------|----------|---------|----------|-------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | 1 | | 44 | ↑ | | 7 | ^ | 7 | 7 | 1 | |
| Traffic Volume (vph) | 1 | 2 | 14 | 1004 | 13 | 313 | 7 | 445 | 367 | 508 | 1563 | 6 |
| Future Volume (vph) | 1 | 2 | 14 | 1004 | 13 | 313 | 7 | 445 | 367 | 508 | 1563 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | | 1.0 | 5.0 | | 5.0 | 5.0 | 1.0 | 1.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 0.97 | 1.00 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.87 | | 1.00 | 0.86 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1825 | 1669 | | 3404 | 1461 | | 1825 | 3259 | 1449 | 1659 | 3348 | |
| Flt Permitted | 0.56 | 1.00 | | 0.95 | 1.00 | | 0.12 | 1.00 | 1.00 | 0.31 | 1.00 | |
| Satd. Flow (perm) | 1073 | 1669 | | 3404 | 1461 | | 222 | 3259 | 1449 | 535 | 3348 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 1.00 | 0.97 |
| Adj. Flow (vph) | 1 | 2 | 14 | 1004 | 13 | 323 | 7 | 459 | 378 | 508 | 1563 | 6 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 177 | 0 | 0 | 0 | 185 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 1 | 9 | 0 | 1004 | 159 | 0 | 7 | 459 | 193 | 508 | 1569 | 0 |
| Confl. Bikes (#/hr) | | | | | | | | | 1 | | | 1 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 4% | 0% | 13% | 0% | 12% | 12% | 10% | 9% | 0% |
| Turn Type | pm+pt | NA | | Prot | NA | | Perm | NA | pm+ov | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | | 6 | 3 | 5 | 2 | |
| Permitted Phases | 4 | | | | | | 6 | | 6 | 2 | | |
| Actuated Green, G (s) | 30.6 | 29.2 | | 37.0 | 64.8 | | 32.6 | 32.6 | 69.6 | 64.0 | 64.0 | |
| Effective Green, g (s) | 36.6 | 31.2 | | 40.0 | 66.8 | | 34.6 | 34.6 | 75.6 | 67.0 | 66.0 | |
| Actuated g/C Ratio | 0.25 | 0.21 | | 0.27 | 0.45 | | 0.23 | 0.23 | 0.51 | 0.45 | 0.45 | |
| Clearance Time (s) | 4.0 | 7.0 | | 4.0 | 7.0 | | 7.0 | 7.0 | 4.0 | 4.0 | 7.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 6.0 | 6.0 | 3.0 | 6.0 | 3.0 | |
| Lane Grp Cap (vph) | 287 | 351 | | 918 | 658 | | 51 | 760 | 739 | 472 | 1491 | |
| v/s Ratio Prot | 0.00 | 0.01 | | c0.29 | c0.11 | | | 0.14 | 0.07 | c0.22 | c0.47 | |
| v/s Ratio Perm | 0.00 | | | | | | 0.03 | | 0.06 | 0.27 | | |
| v/c Ratio | 0.00 | 0.03 | | 1.09 | 0.24 | | 0.14 | 0.60 | 0.26 | 1.08 | 1.05 | |
| Uniform Delay, d1 | 42.0 | 46.4 | | 54.1 | 25.1 | | 45.0 | 50.7 | 20.5 | 33.5 | 41.1 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 0.1 | | 58.6 | 0.9 | | 5.5 | 3.5 | 0.2 | 63.4 | 38.4 | |
| Delay (s) | 42.0 | 46.6 | | 112.7 | 25.9 | | 50.5 | 54.2 | 20.7 | 97.0 | 79.5 | |
| Level of Service | D | D | | F | С | | D | D | С | F | Е | |
| Approach Delay (s) | | 46.3 | | | 91.0 | | | 39.2 | | | 83.8 | |
| Approach LOS | | D | | | F | | | D | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 77.1 | Н | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Cap | acity ratio | | 0.88 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 148.2 | S | um of lost | time (s) | | | 12.0 | | | |
| Intersection Capacity Utiliz | | | 116.2% | | CU Level | . , | | | H | | | |
| Analysis Period (min) | | | 15 | | ,,,,,, | | | | | | | |
| 0.''' 11 0 | | | | | | | | | | | | |

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| | - | * | 1 | • | 1 | - | | |
|------------------------------|-------------|---------|---------|----------|------------|------------------|---|------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | | |
| Lane Configurations | ^ | 7 | * | ^ | ሻ | 7 | | |
| Traffic Volume (vph) | 739 | 179 | 81 | 1021 | 93 | 93 | | |
| Future Volume (vph) | 739 | 179 | 81 | 1021 | 93 | 93 | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | |
| Total Lost time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | |
| Frpb, ped/bikes | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 0.99 | | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Frt | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 | | |
| Flt Protected | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 3444 | 1480 | 1789 | 3579 | 1738 | 1581 | | |
| Flt Permitted | 1.00 | 1.00 | 0.36 | 1.00 | 0.95 | 1.00 | | |
| Satd. Flow (perm) | 3444 | 1480 | 674 | 3579 | 1738 | 1581 | | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | | |
| Adj. Flow (vph) | 762 | 185 | 84 | 1053 | 96 | 96 | | |
| RTOR Reduction (vph) | 0 | 65 | 0 | 0 | 0 | 80 | | |
| Lane Group Flow (vph) | 762 | 120 | 84 | 1053 | 96 | 16 | | |
| Confl. Peds. (#/hr) | 102 | 1 | 1 | . 500 | 1 | 1 | | |
| Heavy Vehicles (%) | 6% | 8% | 2% | 2% | 5% | 2% | | |
| Turn Type | NA | Perm | Perm | NA | Prot | Perm | | |
| Protected Phases | 6 | 1 01111 | i Oiiii | 2 | 8 | 1 01111 | | |
| Permitted Phases | | 6 | 2 | | | 8 | | |
| Actuated Green, G (s) | 33.1 | 33.1 | 33.1 | 33.1 | 8.1 | 8.1 | | |
| Effective Green, g (s) | 35.6 | 35.6 | 35.6 | 35.6 | 9.1 | 9.1 | | |
| Actuated g/C Ratio | 0.65 | 0.65 | 0.65 | 0.65 | 0.17 | 0.17 | | |
| Clearance Time (s) | 7.5 | 7.5 | 7.5 | 7.5 | 6.0 | 6.0 | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 2241 | 963 | 438 | 2329 | 289 | 263 | | |
| v/s Ratio Prot | 0.22 | 300 | 100 | c0.29 | c0.06 | | | |
| v/s Ratio Perm | V | 0.08 | 0.12 | 00.20 | 33.00 | 0.01 | | |
| v/c Ratio | 0.34 | 0.13 | 0.12 | 0.45 | 0.33 | 0.06 | | |
| Uniform Delay, d1 | 4.3 | 3.6 | 3.8 | 4.7 | 20.1 | 19.2 | | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 0.4 | 0.3 | 1.0 | 0.6 | 0.7 | 0.1 | | |
| Delay (s) | 4.7 | 3.9 | 4.8 | 5.4 | 20.8 | 19.3 | | |
| Level of Service | A | A | A | A | C | В | | |
| Approach Delay (s) | 4.5 | | | 5.3 | 20.0 | | | |
| Approach LOS | A | | | A | C | | | |
| Intersection Summary | | | | | | | | |
| HCM 2000 Control Delay | | | 6.2 | Н | CM 2000 | Level of Service |) | Α |
| HCM 2000 Volume to Cap | acity ratio | | 0.43 | - " | 2111 2000 | | | |
| Actuated Cycle Length (s) | | | 54.7 | S | um of lost | time (s) | | 10.0 |
| Intersection Capacity Utiliz | | | 71.2% | | | of Service | | C |
| Analysis Period (min) | | | 15 | | | | | |
| o Critical Lana Croup | | | | | | | | |

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|-------------------------------|------------|----------|--------|-------|------------|------------|---------|----------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | * | ↑ | 7 | 7 | ^ | 7 | * | ^ | 7 |
| Traffic Volume (vph) | 206 | 471 | 41 | 265 | 527 | 77 | 39 | 816 | 146 | 265 | 1973 | 416 |
| Future Volume (vph) | 206 | 471 | 41 | 265 | 527 | 77 | 39 | 816 | 146 | 265 | 1973 | 416 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1738 | 3544 | 1331 | 1772 | 1847 | 1387 | 1644 | 3476 | 1522 | 1771 | 3579 | 1586 |
| Flt Permitted | 0.10 | 1.00 | 1.00 | 0.32 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.23 | 1.00 | 1.00 |
| Satd. Flow (perm) | 191 | 3544 | 1331 | 604 | 1847 | 1387 | 107 | 3476 | 1522 | 431 | 3579 | 1586 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 1.00 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 |
| Adj. Flow (vph) | 212 | 486 | 42 | 265 | 527 | 79 | 40 | 841 | 151 | 273 | 1973 | 429 |
| RTOR Reduction (vph) | 0 | 0 | 30 | 0 | 0 | 57 | 0 | 0 | 81 | 0 | 0 | 123 |
| Lane Group Flow (vph) | 212 | 486 | 12 | 265 | 527 | 22 | 40 | 841 | 70 | 273 | 1973 | 306 |
| Confl. Peds. (#/hr) | 16 | | 1 | 1 | | 16 | 5 | | 14 | 14 | | 5 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 2 |
| Heavy Vehicles (%) | 5% | 3% | 21% | 3% | 4% | 14% | 11% | 5% | 4% | 3% | 2% | 1% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 6 | | 6 | 2 | | 2 |
| Actuated Green, G (s) | 45.0 | 35.4 | 35.4 | 46.2 | 36.0 | 36.0 | 61.9 | 61.9 | 61.9 | 74.4 | 74.4 | 74.4 |
| Effective Green, g (s) | 51.0 | 38.4 | 38.4 | 52.2 | 39.0 | 39.0 | 64.9 | 64.9 | 64.9 | 77.4 | 77.4 | 77.4 |
| Actuated g/C Ratio | 0.36 | 0.27 | 0.27 | 0.37 | 0.28 | 0.28 | 0.46 | 0.46 | 0.46 | 0.55 | 0.55 | 0.55 |
| Clearance Time (s) | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 208 | 972 | 365 | 335 | 514 | 386 | 49 | 1611 | 705 | 348 | 1978 | 876 |
| v/s Ratio Prot | c0.09 | 0.14 | | c0.07 | c0.29 | | | 0.24 | | 0.06 | c0.55 | |
| v/s Ratio Perm | 0.28 | | 0.01 | 0.22 | | 0.02 | 0.37 | | 0.05 | 0.37 | | 0.19 |
| v/c Ratio | 1.02 | 0.50 | 0.03 | 0.79 | 1.03 | 0.06 | 0.82 | 0.52 | 0.10 | 0.78 | 1.00 | 0.35 |
| Uniform Delay, d1 | 39.2 | 42.7 | 37.2 | 34.9 | 50.5 | 37.0 | 32.4 | 26.6 | 21.1 | 19.2 | 31.2 | 17.4 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 67.5 | 0.4 | 0.0 | 12.0 | 46.3 | 0.2 | 82.0 | 1.2 | 0.3 | 11.0 | 19.6 | 1.1 |
| Delay (s) | 106.7 | 43.1 | 37.2 | 46.9 | 96.8 | 37.2 | 114.4 | 27.8 | 21.4 | 30.2 | 50.9 | 18.5 |
| Level of Service | F | D | D | D | F | D | F | С | С | С | D | В |
| Approach Delay (s) | | 61.0 | | | 76.2 | | | 30.2 | | | 43.6 | |
| Approach LOS | | Е | | | Е | | | С | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 48.7 | Н | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Capa | city ratio | | 1.01 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 140.0 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliza | ition | | 135.1% | IC | CU Level | of Service | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|------------|----------|-------|-------|------------|------------|---------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | * | | 7 | ^ | 7 | 7 | | 7 | 7 | 4 | 7 |
| Traffic Volume (vph) | 0 | 1983 | 8 | 14 | 1670 | 0 | 6 | 0 | 13 | 856 | 54 | 347 |
| Future Volume (vph) | 0 | 1983 | 8 | 14 | 1670 | 0 | 6 | 0 | 13 | 856 | 54 | 347 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | | 1.0 | 5.0 | | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 0.91 | | 1.00 | 0.95 | | 1.00 | | 1.00 | 0.95 | 0.91 | 0.95 |
| Frpb, ped/bikes | | 1.00 | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | | 1.00 | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | | 1.00 | 1.00 | | 1.00 | | 0.85 | 1.00 | 0.99 | 0.85 |
| Flt Protected | | 1.00 | | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | 0.96 | 1.00 |
| Satd. Flow (prot) | | 4852 | | 1372 | 3349 | | 1371 | | 1247 | 1651 | 1522 | 1085 |
| Flt Permitted | | 1.00 | | 0.06 | 1.00 | | 0.47 | | 1.00 | 0.95 | 0.96 | 1.00 |
| Satd. Flow (perm) | | 4852 | | 82 | 3349 | | 679 | | 1247 | 1651 | 1522 | 1085 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 0 | 2044 | 8 | 14 | 1722 | 0 | 6 | 0 | 13 | 882 | 56 | 358 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 1 | 81 |
| Lane Group Flow (vph) | 0 | 2052 | 0 | 14 | 1722 | 0 | 6 | 0 | 1 | 494 | 475 | 245 |
| Confl. Peds. (#/hr) | | | 4 | 4 | | | 1 | | | | | 1 |
| Heavy Vehicles (%) | 0% | 8% | 10% | 33% | 9% | 0% | 33% | 0% | 31% | 5% | 20% | 41% |
| Turn Type | | NA | | pm+pt | NA | Perm | Perm | | Perm | Perm | NA | Perm |
| Protected Phases | | 2 | | 1 | 6 | | | | | | 4 | |
| Permitted Phases | | | | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | | 66.7 | | 73.5 | 73.5 | | 6.0 | | 6.0 | 49.0 | 49.0 | 49.0 |
| Effective Green, g (s) | | 68.7 | | 76.5 | 75.5 | | 8.5 | | 8.5 | 51.0 | 51.0 | 51.0 |
| Actuated g/C Ratio | | 0.46 | | 0.51 | 0.50 | | 0.06 | | 0.06 | 0.34 | 0.34 | 0.34 |
| Clearance Time (s) | | 7.0 | | 4.0 | 7.0 | | 7.5 | | 7.5 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2222 | | 91 | 1685 | | 38 | | 70 | 561 | 517 | 368 |
| v/s Ratio Prot | | 0.42 | | 0.01 | c0.51 | | | | | | | |
| v/s Ratio Perm | | | | 0.07 | | | c0.01 | | 0.00 | 0.30 | 0.31 | 0.23 |
| v/c Ratio | | 0.92 | | 0.15 | 1.02 | | 0.16 | | 0.01 | 0.88 | 0.92 | 0.67 |
| Uniform Delay, d1 | | 38.2 | | 28.4 | 37.2 | | 67.3 | | 66.8 | 46.6 | 47.5 | 42.2 |
| Progression Factor | | 1.00 | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 7.9 | | 0.8 | 27.6 | | 1.9 | | 0.1 | 15.0 | 21.2 | 4.5 |
| Delay (s) | | 46.1 | | 29.2 | 64.9 | | 69.3 | | 66.8 | 61.6 | 68.7 | 46.7 |
| Level of Service | | D | | С | Е | | Е | | Е | Е | Е | D |
| Approach Delay (s) | | 46.1 | | | 64.6 | | | 67.6 | | | 60.5 | |
| Approach LOS | | D | | | E | | | Е | | | Е | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 56.1 | Н | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.95 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 150.0 | S | um of lost | t time (s) | | | 18.5 | | | |
| Intersection Capacity Utiliza | ition | | 89.8% | | CU Level o | | | | Е | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| 0.111 0 | | | | | | | | | | | | |

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|-----------------------------------|-------|----------|-------|------|-------------|------------|---------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ^ | 7 | | ^ | 7 | 44 | | 77 | | | |
| Traffic Volume (vph) | 0 | 1026 | 0 | 0 | 1668 | 0 | 483 | 0 | 560 | 0 | 0 | 0 |
| Future Volume (vph) | 0 | 1026 | 0 | 0 | 1668 | 0 | 483 | 0 | 560 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | | | 5.0 | | 5.0 | | 5.0 | | | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 0.97 | | 0.88 | | | |
| Frt | | 1.00 | | | 1.00 | | 1.00 | | 0.85 | | | |
| Flt Protected | | 1.00 | | | 1.00 | | 0.95 | | 1.00 | | | |
| Satd. Flow (prot) | | 3411 | | | 3444 | | 3190 | | 2566 | | | |
| FIt Permitted | | 1.00 | | | 1.00 | | 0.95 | | 1.00 | | | |
| Satd. Flow (perm) | | 3411 | | | 3444 | | 3190 | | 2566 | | | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 0 | 1058 | 0 | 0 | 1720 | 0 | 498 | 0 | 577 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 181 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1058 | 0 | 0 | 1720 | 0 | 498 | 0 | 396 | 0 | 0 | 0 |
| Heavy Vehicles (%) | 0% | 7% | 0% | 0% | 6% | 0% | 11% | 0% | 12% | 0% | 0% | 0% |
| Turn Type | | NA | Perm | | NA | Perm | Perm | | Perm | | | |
| Protected Phases | | 2 | | | 6 | | | | | | | |
| Permitted Phases | | | 2 | | | 6 | 8 | | 8 | | | |
| Actuated Green, G (s) | | 114.3 | | | 114.3 | | 31.7 | | 31.7 | | | |
| Effective Green, g (s) | | 116.8 | | | 116.8 | | 33.2 | | 33.2 | | | |
| Actuated g/C Ratio | | 0.73 | | | 0.73 | | 0.21 | | 0.21 | | | |
| Clearance Time (s) | | 7.5 | | | 7.5 | | 6.5 | | 6.5 | | | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | 3.0 | | 3.0 | | | |
| Lane Grp Cap (vph) | | 2490 | | | 2514 | | 661 | | 532 | | | |
| v/s Ratio Prot | | 0.31 | | | c0.50 | | | | | | | |
| v/s Ratio Perm | | | | | | | c0.16 | | 0.15 | | | |
| v/c Ratio | | 0.42 | | | 0.68 | | 0.75 | | 0.74 | | | |
| Uniform Delay, d1 | | 8.5 | | | 11.7 | | 59.6 | | 59.4 | | | |
| Progression Factor | | 1.00 | | | 0.70 | | 1.00 | | 1.00 | | | |
| Incremental Delay, d2 | | 0.5 | | | 0.1 | | 4.9 | | 5.6 | | | |
| Delay (s) | | 9.0 | | | 8.2 | | 64.4 | | 65.0 | | | |
| Level of Service | | A | | | A | | E | C4.7 | E | | 0.0 | |
| Approach Delay (s) | | 9.0 | | | 8.2 | | | 64.7 | | | 0.0 | |
| Approach LOS | | Α | | | Α | | | E | | | Α | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 24.2 | H | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.71 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 160.0 | | um of lost | | | | 11.5 | | | |
| Intersection Capacity Utilization | 1 | | 67.4% | IC | CU Level of | of Service | | | С | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|------------|----------|--------|-------|-----------|------------|---------|----------|------|-------|----------|-------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 14.14 | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 133 | 1188 | 238 | 225 | 1470 | 26 | 98 | 196 | 64 | 135 | 1620 | 908 |
| Future Volume (vph) | 133 | 1188 | 238 | 225 | 1470 | 26 | 98 | 196 | 64 | 135 | 1620 | 908 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 0.97 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3404 | 3476 | 1564 | 1755 | 3579 | 1305 | 1722 | 3380 | 1427 | 1676 | 3579 | 1578 |
| FIt Permitted | 0.95 | 1.00 | 1.00 | 0.07 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.62 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3404 | 3476 | 1564 | 130 | 3579 | 1305 | 107 | 3380 | 1427 | 1090 | 3579 | 1578 |
| Peak-hour factor, PHF | 0.97 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 1.00 |
| Adj. Flow (vph) | 137 | 1188 | 245 | 225 | 1470 | 27 | 101 | 202 | 66 | 139 | 1620 | 908 |
| RTOR Reduction (vph) | 0 | 0 | 70 | 0 | 0 | 0 | 0 | 0 | 38 | 0 | 0 | 83 |
| Lane Group Flow (vph) | 137 | 1188 | 175 | 225 | 1470 | 27 | 101 | 202 | 28 | 139 | 1620 | 825 |
| Confl. Peds. (#/hr) | 4 | | 1 | 1 | | 4 | 2 | | 14 | 14 | | 2 |
| Heavy Vehicles (%) | 4% | 5% | 3% | 4% | 2% | 23% | 6% | 8% | 11% | 8% | 2% | 2% |
| Turn Type | Prot | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 7.0 | 53.0 | 53.0 | 67.0 | 56.0 | 56.0 | 72.0 | 65.0 | 65.0 | 72.0 | 65.0 | 65.0 |
| Effective Green, g (s) | 11.0 | 56.0 | 56.0 | 71.0 | 59.0 | 59.0 | 78.0 | 68.0 | 68.0 | 78.0 | 68.0 | 68.0 |
| Actuated g/C Ratio | 0.07 | 0.35 | 0.35 | 0.44 | 0.37 | 0.37 | 0.49 | 0.42 | 0.42 | 0.49 | 0.42 | 0.42 |
| Clearance Time (s) | 5.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 234 | 1216 | 547 | 199 | 1319 | 481 | 153 | 1436 | 606 | 568 | 1521 | 670 |
| v/s Ratio Prot | 0.04 | 0.34 | | c0.10 | c0.41 | | c0.04 | 0.06 | | 0.02 | 0.45 | |
| v/s Ratio Perm | | | 0.11 | 0.40 | | 0.02 | 0.28 | | 0.02 | 0.10 | | c0.52 |
| v/c Ratio | 0.59 | 0.98 | 0.32 | 1.13 | 1.11 | 0.06 | 0.66 | 0.14 | 0.05 | 0.24 | 1.07 | 1.23 |
| Uniform Delay, d1 | 72.3 | 51.4 | 38.1 | 50.0 | 50.5 | 32.6 | 35.9 | 28.1 | 27.0 | 22.9 | 46.0 | 46.0 |
| Progression Factor | 1.06 | 0.93 | 0.94 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.3 | 19.2 | 1.3 | 103.3 | 62.5 | 0.2 | 10.2 | 0.0 | 0.0 | 0.2 | 42.6 | 117.0 |
| Delay (s) | 80.2 | 67.1 | 37.2 | 153.4 | 113.0 | 32.8 | 46.1 | 28.2 | 27.0 | 23.1 | 88.6 | 163.0 |
| Level of Service | F | Е | D | F | F | С | D | С | С | С | F | F |
| Approach Delay (s) | | 63.6 | | | 117.0 | | | 32.9 | | | 110.5 | |
| Approach LOS | | Е | | | F | | | С | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 96.1 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capa | city ratio | | 1.14 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 160.0 | S | um of los | t time (s) | | | 12.0 | | | |
| Intersection Capacity Utiliza | ation | | 114.6% | | CU Level | |) | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| 0.111 | | | | | | | | | | | | |

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|------------------------------|-------------|-------------|--------|-------|------------|------------|---------|----------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | * 1> | | * | ↑ ↑ | | * | * | | * | 1 | |
| Traffic Volume (vph) | 55 | 1098 | 129 | 151 | 1712 | 47 | 96 | 256 | 106 | 348 | 1679 | 169 |
| Future Volume (vph) | 55 | 1098 | 129 | 151 | 1712 | 47 | 96 | 256 | 106 | 348 | 1679 | 169 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | | 1.0 | 5.0 | | 1.0 | 5.0 | | 1.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 1.00 | | 1.00 | 0.96 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1738 | 3510 | | 1789 | 3563 | | 1738 | 3299 | | 1800 | 3505 | |
| Flt Permitted | 0.06 | 1.00 | | 0.06 | 1.00 | | 0.08 | 1.00 | | 0.43 | 1.00 | |
| Satd. Flow (perm) | 115 | 3510 | | 116 | 3563 | | 146 | 3299 | | 814 | 3505 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 |
| Adj. Flow (vph) | 57 | 1132 | 133 | 156 | 1712 | 48 | 99 | 264 | 109 | 359 | 1679 | 174 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 1 | 0 | 0 | 28 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 57 | 1260 | 0 | 156 | 1759 | 0 | 99 | 345 | 0 | 359 | 1848 | 0 |
| Confl. Peds. (#/hr) | 15 | | 7 | 7 | | 15 | 20 | | 13 | 13 | | 20 |
| Heavy Vehicles (%) | 5% | 2% | 3% | 2% | 2% | 0% | 5% | 6% | 2% | 1% | 2% | 5% |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 66.4 | 60.8 | | 71.2 | 63.2 | | 54.0 | 47.0 | | 74.0 | 63.0 | |
| Effective Green, g (s) | 72.4 | 62.8 | | 75.8 | 65.2 | | 60.0 | 49.0 | | 77.0 | 65.0 | |
| Actuated g/C Ratio | 0.45 | 0.39 | | 0.47 | 0.41 | | 0.37 | 0.30 | | 0.48 | 0.40 | |
| Clearance Time (s) | 4.0 | 7.0 | | 4.0 | 7.0 | | 4.0 | 7.0 | | 4.0 | 7.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 138 | 1370 | | 169 | 1444 | | 153 | 1005 | | 549 | 1416 | |
| v/s Ratio Prot | 0.02 | 0.36 | | c0.06 | c0.49 | | 0.04 | 0.10 | | c0.11 | c0.53 | |
| v/s Ratio Perm | 0.16 | | | 0.37 | | | 0.20 | | | 0.21 | | |
| v/c Ratio | 0.41 | 0.92 | | 0.92 | 1.22 | | 0.65 | 0.34 | | 0.65 | 1.31 | |
| Uniform Delay, d1 | 36.6 | 46.6 | | 45.6 | 47.8 | | 40.5 | 43.4 | | 27.7 | 47.9 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.0 | 11.4 | | 47.2 | 104.6 | | 9.1 | 0.9 | | 2.8 | 142.6 | |
| Delay (s) | 38.6 | 58.0 | | 92.8 | 152.4 | | 49.5 | 44.3 | | 30.5 | 190.5 | |
| Level of Service | D | Е | | F | F | | D | D | | С | F | |
| Approach Delay (s) | | 57.2 | | | 147.6 | | | 45.4 | | | 164.5 | |
| Approach LOS | | Е | | | F | | | D | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 125.6 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capa | acity ratio | | 1.20 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 160.8 | S | um of lost | time (s) | | | 12.0 | | | |
| Intersection Capacity Utiliz | ation | | 127.5% | IC | U Level o | of Service |) | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|------------|----------|--------|-------|------------|------------|---------|----------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | * | ^ | 7 | T | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 154 | 921 | 209 | 259 | 1548 | 21 | 253 | 559 | 190 | 41 | 1458 | 556 |
| Future Volume (vph) | 154 | 921 | 209 | 259 | 1548 | 21 | 253 | 559 | 190 | 41 | 1458 | 556 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| FIt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1755 | 3579 | 1544 | 1807 | 3579 | 1518 | 1807 | 3510 | 1542 | 1771 | 3614 | 1574 |
| FIt Permitted | 0.08 | 1.00 | 1.00 | 0.12 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.34 | 1.00 | 1.00 |
| Satd. Flow (perm) | 146 | 3579 | 1544 | 230 | 3579 | 1518 | 143 | 3510 | 1542 | 635 | 3614 | 1574 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 | 1.00 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 |
| Adj. Flow (vph) | 159 | 949 | 215 | 267 | 1548 | 22 | 253 | 576 | 196 | 42 | 1458 | 573 |
| RTOR Reduction (vph) | 0 | 0 | 91 | 0 | 0 | 13 | 0 | 0 | 122 | 0 | 0 | 82 |
| Lane Group Flow (vph) | 159 | 949 | 124 | 267 | 1548 | 9 | 253 | 576 | 74 | 42 | 1458 | 491 |
| Confl. Peds. (#/hr) | 4 | | 4 | 4 | | 4 | 4 | | 5 | 5 | | 4 |
| Heavy Vehicles (%) | 4% | 2% | 4% | 1% | 2% | 6% | 1% | 4% | 4% | 3% | 1% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 54.5 | 47.5 | 47.5 | 65.5 | 54.5 | 54.5 | 57.7 | 50.7 | 50.7 | 54.9 | 49.3 | 49.3 |
| Effective Green, g (s) | 60.5 | 50.0 | 50.0 | 68.5 | 57.0 | 57.0 | 63.3 | 53.2 | 53.2 | 60.9 | 51.8 | 51.8 |
| Actuated g/C Ratio | 0.43 | 0.36 | 0.36 | 0.49 | 0.40 | 0.40 | 0.45 | 0.38 | 0.38 | 0.43 | 0.37 | 0.37 |
| Clearance Time (s) | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 177 | 1270 | 548 | 302 | 1448 | 614 | 182 | 1326 | 582 | 344 | 1329 | 579 |
| v/s Ratio Prot | c0.06 | 0.27 | | c0.11 | c0.43 | | c0.10 | 0.16 | | 0.01 | c0.40 | |
| v/s Ratio Perm | 0.32 | | 0.08 | 0.32 | | 0.01 | 0.53 | | 0.05 | 0.05 | | 0.31 |
| v/c Ratio | 0.90 | 0.75 | 0.23 | 0.88 | 1.07 | 0.01 | 1.39 | 0.43 | 0.13 | 0.12 | 1.10 | 0.85 |
| Uniform Delay, d1 | 36.1 | 39.9 | 31.8 | 32.3 | 41.9 | 25.1 | 40.3 | 32.6 | 28.6 | 23.7 | 44.5 | 40.9 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 39.7 | 4.0 | 1.0 | 24.9 | 44.5 | 0.0 | 205.6 | 0.2 | 0.1 | 0.2 | 55.7 | 11.2 |
| Delay (s) | 75.8 | 43.9 | 32.8 | 57.2 | 86.4 | 25.1 | 245.9 | 32.8 | 28.7 | 23.9 | 100.2 | 52.1 |
| Level of Service | Е | D | С | Е | F | С | F | С | С | С | F | D |
| Approach Delay (s) | | 45.9 | | | 81.4 | | | 84.6 | | | 85.3 | |
| Approach LOS | | D | | | F | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 75.7 | Н | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capa | city ratio | | 1.08 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 140.8 | S | um of lost | t time (s) | | | 12.0 | | | |
| Intersection Capacity Utiliza | ation | | 120.6% | | U Level | | Э | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Synchro 10 Report Page 13 Baseline

| | ٠ | → | * | • | ← | • | 1 | 1 | ~ | / | ↓ | 4 |
|---------------------------------|--------------|--------------|--------------|--------------|-----------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | × | ^ | 7 | 7 | ^ | 7 | Y | ^ | 7 | * | ^ | 7 |
| Traffic Volume (vph) | 163 | 928 | 88 | 178 | 1018 | 92 | 114 | 703 | 301 | 314 | 1703 | 497 |
| Future Volume (vph) | 163 | 928 | 88 | 178 | 1018 | 92 | 114 | 703 | 301 | 314 | 1703 | 497 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 4.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 1.00 | 0.85 1.00 | 1.00 0.95 | 1.00 | 0.85 1.00 | 1.00 | 1.00 | 0.85 1.00 | 1.00 0.95 | 1.00 1.00 | 0.85 |
| Flt Protected Satd. Flow (prot) | 0.95 1722 | 3476 | 1585 | 1807 | 3544 | 1565 | 0.95 1807 | 1.00 3510 | 1551 | 1824 | 3614 | 1.00 1600 |
| Flt Permitted | 0.10 | 1.00 | 1.00 | 0.10 | 1.00 | 1.00 | 0.07 | 1.00 | 1.00 | 0.26 | 1.00 | 1.00 |
| Satd. Flow (perm) | 173 | 3476 | 1585 | 181 | 3544 | 1565 | 131 | 3510 | 1551 | 499 | 3614 | 1600 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 |
| Adj. Flow (vph) | 168 | 957 | 91 | 184 | 1018 | 95 | 118 | 725 | 310 | 324 | 1703 | 512 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 67 | 0 | 0 | 113 | 0 | 0 | 95 |
| Lane Group Flow (vph) | 168 | 957 | 91 | 184 | 1018 | 28 | 118 | 725 | 197 | 324 | 1703 | 417 |
| Confl. Peds. (#/hr) | 1 | 007 | 01 | 101 | 1010 | 1 | 7 | 720 | 8 | 8 | 1700 | 7 |
| Heavy Vehicles (%) | 6% | 5% | 3% | 1% | 3% | 3% | 1% | 4% | 3% | 0% | 1% | 0% |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | . • | 3 | 8 | | 7 | 4 | . • |
| Permitted Phases | 2 | | Free | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 46.0 | 39.0 | 140.0 | 46.0 | 39.0 | 39.0 | 62.1 | 55.1 | 55.1 | 76.0 | 65.0 | 65.0 |
| Effective Green, g (s) | 52.0 | 41.0 | 140.0 | 52.0 | 41.0 | 41.0 | 68.1 | 57.1 | 57.1 | 79.0 | 67.0 | 67.0 |
| Actuated g/C Ratio | 0.37 | 0.29 | 1.00 | 0.37 | 0.29 | 0.29 | 0.49 | 0.41 | 0.41 | 0.56 | 0.48 | 0.48 |
| Clearance Time (s) | 4.0 | 7.0 | | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 174 | 1017 | 1585 | 183 | 1037 | 458 | 183 | 1431 | 632 | 469 | 1729 | 765 |
| v/s Ratio Prot | 0.07 | 0.28 | | c0.07 | c0.29 | | 0.05 | 0.21 | | c0.10 | c0.47 | |
| v/s Ratio Perm | 0.29 | | 0.06 | 0.30 | | 0.02 | 0.27 | | 0.13 | 0.29 | | 0.26 |
| v/c Ratio | 0.97 | 0.94 | 0.06 | 1.01 | 0.98 | 0.06 | 0.64 | 0.51 | 0.31 | 0.69 | 0.98 | 0.55 |
| Uniform Delay, d1 | 36.2 | 48.3 | 0.0 | 36.1 | 49.1 | 35.6 | 30.9 | 30.9 | 28.1 | 18.3 | 36.0 | 25.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 57.6 | 17.2 | 0.1 | 68.0 | 23.9 | 0.3 | 7.6 | 0.3 | 0.3 | 4.4 | 18.0 | 0.8 |
| Delay (s) | 93.7 | 65.5 | 0.1 | 104.1 | 73.0 | 35.9 | 38.5 | 31.2 | 28.4 | 22.7 | 54.0 | 26.5 |
| Level of Service | F | E 64.5 | Α | F | E 74.7 | D | D | C | С | С | D | С |
| Approach LOS | | 64.5 E | | | 74.7 E | | | 31.2 C | | | 44.5 | |
| Approach LOS | | | | | | | | C | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 52.2 | Н | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Cap | acity ratio | | 0.94 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 140.0 | | um of los | | | | 12.0 | | | |
| Intersection Capacity Utiliz | ation | | 105.6% | IC | CU Level | of Service | 9 | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|-------------|----------|--------|-------|------------|------------|---------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 239 | 409 | 113 | 823 | 823 | 56 | 16 | 407 | 126 | 31 | 1779 | 184 |
| Future Volume (vph) | 239 | 409 | 113 | 823 | 823 | 56 | 16 | 407 | 126 | 31 | 1779 | 184 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1615 | 3579 | 1541 | 1738 | 3614 | 1484 | 1460 | 3318 | 1471 | 1825 | 3544 | 1585 |
| Flt Permitted | 0.32 | 1.00 | 1.00 | 0.29 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.49 | 1.00 | 1.00 |
| Satd. Flow (perm) | 551 | 3579 | 1541 | 523 | 3614 | 1484 | 129 | 3318 | 1471 | 942 | 3544 | 1585 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 239 | 409 | 113 | 823 | 823 | 56 | 16 | 407 | 126 | 31 | 1779 | 184 |
| RTOR Reduction (vph) | 0 | 0 | 100 | 0 | 0 | 40 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 239 | 409 | 13 | 823 | 823 | 16 | 16 | 407 | 126 | 31 | 1779 | 184 |
| Heavy Vehicles (%) | 13% | 2% | 6% | 5% | 1% | 10% | 25% | 10% | 11% | 0% | 3% | 3% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 20.0 | 10.0 | 10.0 | 41.0 | 27.0 | 27.0 | 44.0 | 44.0 | 44.0 | 44.0 | 44.0 | 44.0 |
| Effective Green, g (s) | 26.0 | 11.5 | 11.5 | 44.0 | 28.5 | 28.5 | 47.5 | 47.5 | 47.5 | 47.5 | 47.5 | 47.5 |
| Actuated g/C Ratio | 0.26 | 0.12 | 0.12 | 0.44 | 0.28 | 0.28 | 0.48 | 0.48 | 0.48 | 0.48 | 0.48 | 0.48 |
| Clearance Time (s) | 4.0 | 6.5 | 6.5 | 4.0 | 6.5 | 6.5 | 8.5 | 8.5 | 8.5 | 8.5 | 8.5 | 8.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 281 | 411 | 177 | 594 | 1029 | 422 | 61 | 1576 | 698 | 447 | 1683 | 752 |
| v/s Ratio Prot | 0.11 | c0.11 | | c0.42 | 0.23 | | | 0.12 | | | c0.50 | |
| v/s Ratio Perm | 0.11 | | 0.01 | 0.19 | | 0.01 | 0.12 | | 0.09 | 0.03 | | 0.12 |
| v/c Ratio | 0.85 | 1.00 | 0.07 | 1.39 | 0.80 | 0.04 | 0.26 | 0.26 | 0.18 | 0.07 | 1.06 | 0.24 |
| Uniform Delay, d1 | 32.1 | 44.2 | 39.5 | 25.9 | 33.1 | 25.8 | 15.7 | 15.7 | 15.1 | 14.3 | 26.2 | 15.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 21.1 | 42.8 | 0.2 | 183.8 | 4.4 | 0.0 | 2.3 | 0.1 | 0.1 | 0.1 | 38.8 | 0.2 |
| Delay (s) | 53.2 | 87.1 | 39.7 | 209.6 | 37.5 | 25.9 | 18.0 | 15.8 | 15.2 | 14.3 | 65.0 | 15.8 |
| Level of Service | D | F | D | F | D | С | В | В | В | В | Е | В |
| Approach Delay (s) | | 69.4 | | | 120.4 | | | 15.7 | | | 59.7 | |
| Approach LOS | | Е | | | F | | | В | | | Е | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 77.0 | Н | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capa | acity ratio | | 1.14 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | um of lost | | | | 11.0 | | | |
| Intersection Capacity Utiliza | ation | | 117.7% | IC | CU Level | of Service | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|------------|----------|--------|-------|------------|------------|----------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 180 | 468 | 247 | 1014 | 663 | 193 | 61 | 503 | 109 | 23 | 1931 | 127 |
| Future Volume (vph) | 180 | 468 | 247 | 1014 | 663 | 193 | 61 | 503 | 109 | 23 | 1931 | 127 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1705 | 3579 | 1445 | 1789 | 3579 | 1519 | 1508 | 3380 | 1477 | 1382 | 3579 | 1500 |
| Flt Permitted | 0.40 | 1.00 | 1.00 | 0.28 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.41 | 1.00 | 1.00 |
| Satd. Flow (perm) | 717 | 3579 | 1445 | 522 | 3579 | 1519 | 96 | 3380 | 1477 | 591 | 3579 | 1500 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 180 | 468 | 247 | 1014 | 663 | 193 | 61 | 503 | 109 | 23 | 1931 | 127 |
| RTOR Reduction (vph) | 0 | 0 | 50 | 0 | 0 | 101 | 0 | 0 | 59 | 0 | 0 | 33 |
| Lane Group Flow (vph) | 180 | 468 | 197 | 1014 | 663 | 92 | 61 | 503 | 50 | 23 | 1931 | 94 |
| Confl. Peds. (#/hr) | 1 | | | | | 1 | 3 | | 1 | 1 | | 3 |
| Confl. Bikes (#/hr) | | | | | | 1 | | | 1 | | | |
| Heavy Vehicles (%) | 7% | 2% | 13% | 2% | 2% | 6% | 21% | 8% | 9% | 32% | 2% | 7% |
| Turn Type | Perm | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 29.0 | 29.0 | 29.0 | 67.0 | 67.0 | 67.0 | 63.5 | 63.5 | 63.5 | 63.5 | 63.5 | 63.5 |
| Effective Green, g (s) | 31.0 | 31.0 | 31.0 | 70.0 | 69.0 | 69.0 | 66.0 | 66.0 | 66.0 | 66.0 | 66.0 | 66.0 |
| Actuated g/C Ratio | 0.21 | 0.21 | 0.21 | 0.48 | 0.48 | 0.48 | 0.46 | 0.46 | 0.46 | 0.46 | 0.46 | 0.46 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 153 | 765 | 308 | 575 | 1703 | 722 | 43 | 1538 | 672 | 269 | 1629 | 682 |
| v/s Ratio Prot | | 0.13 | | c0.45 | 0.19 | | | 0.15 | | | 0.54 | |
| v/s Ratio Perm | c0.25 | | 0.14 | 0.40 | | 0.06 | c0.63 | | 0.03 | 0.04 | | 0.06 |
| v/c Ratio | 1.18 | 0.61 | 0.64 | 1.76 | 0.39 | 0.13 | 1.42 | 0.33 | 0.07 | 0.09 | 1.19 | 0.14 |
| Uniform Delay, d1 | 57.0 | 51.6 | 51.9 | 32.7 | 24.4 | 21.2 | 39.5 | 25.3 | 22.3 | 22.4 | 39.5 | 23.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 128.1 | 1.5 | 4.3 | 350.6 | 0.1 | 0.1 | 282.8 | 0.1 | 0.0 | 0.1 | 90.0 | 0.1 |
| Delay (s) | 185.1 | 53.0 | 56.2 | 383.4 | 24.6 | 21.3 | 322.3 | 25.4 | 22.3 | 22.5 | 129.5 | 23.1 |
| Level of Service | F | D | Е | F | С | С | F | С | С | С | F | С |
| Approach Delay (s) | | 80.4 | | | 218.8 | | | 51.8 | | | 121.8 | |
| Approach LOS | | F | | | F | | | D | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 139.4 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capac | citv ratio | | 1.43 | | | | | | | | | |
| Actuated Cycle Length (s) | , | | 145.0 | S | um of lost | t time (s) | | | 11.0 | | | |
| Intersection Capacity Utiliza | tion | | 136.5% | | | of Service | <u> </u> | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|-------------|----------|--------|------|------------|------------|---------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | * | ^ | 7 | 1 | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 143 | 1217 | 358 | 34 | 1405 | 106 | 506 | 580 | 43 | 100 | 969 | 441 |
| Future Volume (vph) | 143 | 1217 | 358 | 34 | 1405 | 106 | 506 | 580 | 43 | 100 | 969 | 441 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 6.5 | 5.0 | 6.5 | 1.0 | 5.0 | 8.0 | 8.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1789 | 3650 | 1601 | 1825 | 3650 | 1633 | 1789 | 3579 | 1633 | 1825 | 3579 | 1601 |
| Flt Permitted | 0.08 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 | 0.43 | 1.00 | 1.00 |
| Satd. Flow (perm) | 155 | 3650 | 1601 | 174 | 3650 | 1633 | 209 | 3579 | 1633 | 818 | 3579 | 1601 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 | 1.00 | 0.97 | 0.97 | 0.97 | 1.00 | 0.97 |
| Adj. Flow (vph) | 147 | 1255 | 369 | 35 | 1405 | 109 | 506 | 598 | 44 | 103 | 969 | 455 |
| RTOR Reduction (vph) | 0 | 0 | 117 | 0 | 0 | 72 | 0 | 0 | 24 | 0 | 0 | 91 |
| Lane Group Flow (vph) | 147 | 1255 | 252 | 35 | 1405 | 37 | 506 | 598 | 20 | 103 | 969 | 364 |
| Heavy Vehicles (%) | 2% | 0% | 2% | 0% | 0% | 0% | 2% | 2% | 0% | 0% | 2% | 2% |
| Turn Type | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |
| Protected Phases | 7 | 4 | | | 8 | | 5 | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 55.5 | 55.5 | 55.5 | 44.5 | 44.5 | 44.5 | 60.0 | 60.0 | 60.0 | 32.0 | 32.0 | 32.0 |
| Effective Green, g (s) | 58.5 | 57.0 | 57.0 | 44.5 | 46.0 | 44.5 | 63.0 | 63.0 | 60.0 | 32.0 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.45 | 0.44 | 0.44 | 0.34 | 0.35 | 0.34 | 0.48 | 0.48 | 0.46 | 0.25 | 0.27 | 0.27 |
| Clearance Time (s) | 4.0 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 4.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 195 | 1600 | 701 | 59 | 1291 | 558 | 429 | 1734 | 753 | 201 | 963 | 431 |
| v/s Ratio Prot | 0.06 | c0.34 | | | c0.38 | | c0.24 | 0.17 | | | c0.27 | |
| v/s Ratio Perm | 0.28 | | 0.16 | 0.20 | | 0.02 | 0.33 | | 0.01 | 0.13 | | 0.23 |
| v/c Ratio | 0.75 | 0.78 | 0.36 | 0.59 | 1.09 | 0.07 | 1.18 | 0.34 | 0.03 | 0.51 | 1.01 | 0.84 |
| Uniform Delay, d1 | 29.7 | 31.2 | 24.3 | 35.3 | 42.0 | 28.8 | 40.3 | 20.7 | 19.1 | 42.3 | 47.5 | 44.9 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 15.2 | 2.6 | 0.3 | 15.0 | 52.7 | 0.1 | 102.5 | 0.5 | 0.1 | 9.0 | 30.5 | 18.0 |
| Delay (s) | 44.9 | 33.8 | 24.6 | 50.3 | 94.7 | 28.8 | 142.8 | 21.3 | 19.1 | 51.3 | 78.0 | 62.9 |
| Level of Service | D | С | С | D | F | С | F | С | В | D | Е | Е |
| Approach Delay (s) | | 32.8 | | | 89.1 | | | 74.8 | | | 71.7 | |
| Approach LOS | | С | | | F | | | Е | | | Е | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 65.3 | Н | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capa | acity ratio | | 1.03 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | um of lost | | | | 12.0 | | | |
| Intersection Capacity Utiliza | ation | | 116.6% | IC | CU Level | of Service | 9 | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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| | ۶ | → | * | • | + | • | 1 | 1 | ~ | / | Ţ | 4 |
|-----------------------------------|------|----------|--------|---------------------------|----------|------|-------|----------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | ^ | 7 | ٦ | ^ | 7 | * | ^ | 7 | * | ^ | 7 |
| Traffic Volume (vph) | 24 | 921 | 431 | 413 | 1081 | 41 | 477 | 865 | 231 | 215 | 2116 | 24 |
| Future Volume (vph) | 24 | 921 | 431 | 413 | 1081 | 41 | 477 | 865 | 231 | 215 | 2116 | 24 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1825 | 3650 | 1633 | 1789 | 3650 | 1601 | 1825 | 3579 | 1601 | 1789 | 3579 | 1633 |
| Flt Permitted | 0.12 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.24 | 1.00 | 1.00 |
| Satd. Flow (perm) | 233 | 3650 | 1633 | 215 | 3650 | 1601 | 116 | 3579 | 1601 | 446 | 3579 | 1633 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 24 | 921 | 431 | 413 | 1081 | 41 | 477 | 865 | 231 | 215 | 2116 | 24 |
| RTOR Reduction (vph) | 0 | 0 | 119 | 0 | 0 | 27 | 0 | 0 | 121 | 0 | 0 | 13 |
| Lane Group Flow (vph) | 24 | 921 | 312 | 413 | 1081 | 14 | 477 | 865 | 110 | 215 | 2116 | 11 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 2% | 0% | 2% | 0% | 2% | 2% | 2% | 2% | 0% |
| Turn Type | Perm | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 31.0 | 31.0 | 31.0 | 46.0 | 46.0 | 46.0 | 77.2 | 64.2 | 64.2 | 73.8 | 62.5 | 62.5 |
| Effective Green, g (s) | 33.0 | 33.0 | 33.0 | 49.0 | 48.0 | 48.0 | 82.5 | 66.7 | 66.7 | 79.8 | 65.0 | 65.0 |
| Actuated g/C Ratio | 0.24 | 0.24 | 0.24 | 0.35 | 0.34 | 0.34 | 0.59 | 0.48 | 0.48 | 0.57 | 0.46 | 0.46 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 54 | 860 | 384 | 232 | 1251 | 548 | 263 | 1705 | 762 | 391 | 1661 | 758 |
| v/s Ratio Prot | | c0.25 | | c0.18 | 0.30 | | c0.21 | 0.24 | | 0.06 | c0.59 | |
| v/s Ratio Perm | 0.10 | | 0.19 | 0.44 | | 0.01 | 0.86 | | 0.07 | 0.26 | | 0.01 |
| v/c Ratio | 0.44 | 1.07 | 0.81 | 1.78 | 0.86 | 0.03 | 1.81 | 0.51 | 0.14 | 0.55 | 1.27 | 0.01 |
| Uniform Delay, d1 | 45.7 | 53.5 | 50.6 | 39.8 | 43.0 | 30.5 | 47.9 | 25.3 | 20.6 | 16.5 | 37.5 | 20.2 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 5.7 | 51.5 | 12.3 | 368.0 | 6.4 | 0.0 | 380.8 | 1.1 | 0.4 | 1.6 | 128.1 | 0.0 |
| Delay (s) | 51.4 | 105.0 | 62.9 | 407.8 | 49.4 | 30.5 | 428.7 | 26.4 | 21.0 | 18.1 | 165.6 | 20.3 |
| Level of Service | D | F | Е | F | D | С | F | С | С | В | F | С |
| Approach Delay (s) | | 90.9 | | | 145.3 | | | 147.6 | | | 150.7 | |
| Approach LOS | | F | | | F | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay 136.7 | | | | HCM 2000 Level of Service | | | | | F | | | |
| HCM 2000 Volume to Capacity ratio | | | 1.30 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 140.0 | · / | | | | | 12.0 | | | |
| Intersection Capacity Utilization | | | 148.3% | ICU Level of Service | | | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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